Phase I Bond Release Application

J19, J19 West (J19W), and N9 Coal Resource Areas, Kayenta Mine

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PUBLIC NOTICE

Peabody Western Coal Company (PWCC) has filed an application with the Office of Surface Mining Reclamation and Enforcement (OSMRE) for bond release on a portion of the lands in the J19, J19W, and N9 Coal Resource Areas (CRAs) within the Kayenta Mine Permit AZ-0001F. PWCC is seeking a release of Phase I bond liability for a portion of the J19, J19W, and N9 areas currently under bond with Zurich American Insurance Company, Continental Casualty Company, National Fire Insurance Company of Hartford, Federal Insurance Company, Liberty Mutual Insurance Company, Indemnity National Insurance Company, and Travelers Casualty and Surety Company of America. PWCC is seeking a reduction in bond of \$20,299,758 under the Phase I application from the total J19, J19W, and N9 bond amount of \$79,830,381. The total combined bond for Kayenta Mine is \$178,569,992.

The Phase I bond release application consists of information currently contained in the AZ-0001F permit application package (PAP) approved October 3, 2017. The PAP outlines PWCC's reclamation operations on Permanent Program Lands. The total areas in J19, J19W, and N9 requested for Phase I release is 929 acres. Reclamation was completed between 1999 and 2019. Reclamation activities were completed in accordance with the approved PAP and included backfilling, grading, and replacement of suitable soil or plant growth media. Other reclamation activities included mitigation of unsuitable material and drainage control construction. The Kayenta Mine permit for the release areas is under Navajo Tribal Coal Lease 14-20-0603-9910, Navajo Tribal Coal Lease 14-20-0603-8580, and Hopi Tribal Coal Lease 14-20-0450-5743 and operates pursuant to Code of Federal Regulations (CFR), Title 30; Subchapter E, Part 750; Subchapter G, Parts 773 and 774; and Subchapter K, Parts 810 and 816. This notice is hereby given that:

1. The name and business address of the applicant is:

Peabody Western Coal Company Kayenta Mine P.O. Box 650 Kayenta, AZ 86033

2. The mine permit area is located approximately 18 miles south southwest of Kayenta, Arizona. The permit area for the Phase I bond release areas is located in USGS 7.5 minute quadrangle maps "Yucca Hill" and "Long House Valley" within the following lands of Navajo County, Arizona that are described relative to the Gila and Salt River Base Meridian as:

A total of 267 acres of land located within the J19 CRA. The computer-generated centroid location is Latitude $36^\circ~26'~45.4''$ N and Longitude $110^\circ~17'$

54.9" W. A total of 251 acres of land located within the J19W CRA. The computer-generated centroid location is Latitude $36^{\circ} 26' 57.0"$ N and Longitude $110^{\circ} 19' 41.7"$ W. A total of 411 acres of land located within the N9 CRA. The computer-generated centroid location is Latitude $36^{\circ} 33' 43.5"$ N and Longitude $110^{\circ} 24' 59.2"$ W.

3. Locations of where copies of the application and permit are available for public review and/or inspection are:

Navajo Nation Minerals Department	Forest Lake Chapter House
Office of Surface Mining	Navajo Route 41
Window Rock Boulevard	20 Miles North of Pinon
Window Rock, AZ 86515	Pinon, AZ 86510

Office of Surface Mining	Hopi Tribe
Reclamation and Enforcement	Office of Mining and Mineral
Western Region Office	Resources, Highway 264
P. O. Box 25065	1 Mile East of Kykotsmovi
Denver, CO 80225-0065	Kykotsmovi, AZ 86039

4. The name and address of the OSMRE-WRO representative where written comments, objections, requests for a public hearing, or requests for an informal conference may be submitted on or before 5:00 p.m., (Date To Be Determined), thirty (30) days after the last publication date are:

Mr. Jeremy Spangler Western Region Office Office of Surface Mining Reclamation & Enforcement P. O. Box 25065 Denver, CO 80225-0065 WR Permitting Information Line, 1-866-847-7362

- Interested persons may obtain more information concerning the bond release by contacting Marie Shepherd, Senior Manager Environmental for PWCC at 928.677.5130.
- 6. The application has been filed with OSMRE and will be acted upon pursuant to the Permanent Regulatory Program (30 CFR Parts 750 and 774) approved by the Secretary of the Interior under Title V of the Surface mining Control and Reclamation Act of 1977.



June 17, 2020

Bureau of Indian Affairs Navajo Area Office Ms. Sharon A. Pinto, Area Director P.O. Box 1060 301 West Hill Street Gallup, New Mexico 87305-1060

RE: Notice of Application for Phase I Bond Release; J19, J19W, and N9 Coal Resource Areas; Kayenta Mine

Dear Ms. Pinto:

Peabody Western Coal Company (PWCC) has filed an application with the Office of Surface Mining Reclamation and Enforcement (OSMRE) for Phase I bond release on portions of the J19, J19W, and N9 Coal Resource Areas. The release areas are in the northwestern and southeastern portion of the PWCC lease area. PWCC is seeking release from Phase I bond liability for those surety bonds currently held with Zurich American Insurance Company, Continental Casualty Company, National Fire Insurance Company of Hartford, Liberty Mutual Insurance Company, Federal Insurance Company, Indemnity National Insurance Company, and Travelers Casualty and Surety Company of America. The total combined bond for Kayenta Mine is \$178,569,992.

The Phase I bond release areas are located within the Kayenta Mine Permanent Program permit area (AZ-0001F PAP) in the northwestern and southeastern portions of the PWCC lease area. PWCC is seeking a reduction of the total J19, J19W, and N9 bond amount of \$20,299,758 at this time by gaining regulatory approval for release of lands described in the application from Phase I bond liability. The total area sought for release includes 929 acres of disturbed land. Approval of Phase I will allow for Phase II and III bond release to proceed on these areas once all requirements for this phase are met. Phase III is the final bond release step and once approved will allow for the planned return of these lands to the Navajo Nation in the future. Until that time, PWCC will continue to control and manage reclaimed lands in the release areas described.

Reclamation of the Phase I release areas which includes; backfilling and grading, drainage control, mitigation of unsuitable material, and topsoil replacement was completed between 1999 and 2019. All reclamation activities were conducted in accordance with the Surface Mining Control and Reclamation Act (SMCRA) and the requirements of the OSMRE Permit AZ-0001F PAP approved October 3, 2017. Reclamation activities are documented in annual reports submitted previously to OSMRE.

Navajo Nation Minerals Dept.	Forest Lake Chapter House
Office of Surface Mining	Navajo Route 41
Window Rock Boulevard	14 miles North of Pinon
Window Rock, AZ 86515	Pinon, AZ 86510

Ms. Sharon A. Pinto June 17, 2020 Page 2 of 2

> Office of Surface Mining Reclamation and Enforcement Western Region Office 1999 Broadway, Suite 3320 Denver, CO 80202-3050

Hopi Tribe Office of Mining and Mineral Resources, Highway 264 1 Mile East of Kykotsmovi Kykotsmovi, AZ 86039

If you have questions, comments, or wish to request a hearing or informal conference regarding this bond release application, please contact:

Mr. Jeremy Spangler Western Region Office Office of Surface Mining Reclamation & Enforcement 1999 Broadway, Suite 3320 Denver, CO 80202-3050 303.293.5022

Please direct your questions about this application to me at 928.677.5130 or email them to me at mshepherd2@peabodyenergy.com.

Respectfully,

Marie Shepherd Senior Manager Environmental Kayenta Mine



June 17, 2020

Bureau of Land Management Arizona State Office Mr. Stewart Boyd Native American Minerals Lead One North Central Ave., Suite 800 Phoenix, Arizona 85004

RE: Notice of Application for Phase I Bond Release; J19, J19W, and N9 Coal Resource Areas; Kayenta Mine

Dear Mr. Boyd:

Peabody Western Coal Company (PWCC) has filed an application with the Office of Surface Mining Reclamation and Enforcement (OSMRE) for Phase I bond release on portions of the J19, J19W, and N9 Coal Resource Areas. The release areas are in the northwestern and southeastern portion of the PWCC lease area. PWCC is seeking release from Phase I bond liability for those surety bonds currently held with Zurich American Insurance Company, Continental Casualty Company, National Fire Insurance Company of Hartford, Liberty Mutual Insurance Company, Federal Insurance Company, Indemnity National Insurance Company, and Travelers Casualty and Surety Company of America. The total combined bond for Kayenta Mine is \$178,569,992.

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Navajo Nation Minerals Dept.	Forest Lake Chapter House
Office of Surface Mining	Navajo Route 41
Window Rock Boulevard	14 miles North of Pinon
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Mr. Stewart Boyd June 17, 2020 Page 2 of 2

> Office of Surface Mining Reclamation and Enforcement Western Region Office 1999 Broadway, Suite 3320 Denver, CO 80202-3050

Hopi Tribe Office of Mining and Mineral Resources, Highway 264 1 Mile East of Kykotsmovi Kykotsmovi, AZ 86039

If you have questions, comments, or wish to request a hearing or informal conference regarding this bond release application, please contact:

Mr. Jeremy Spangler Western Region Office Office of Surface Mining Reclamation & Enforcement 1999 Broadway, Suite 3320 Denver, CO 80202-3050 303.293.5022

Please direct your questions about this application to me at 928.677.5130 or email them to me at mshepherd2@peabodyenergy.com.

Respectfully,

Marie Shepherd Senior Manager Environmental Kayenta Mine



PEABODY WESTERN COAL COMPANY Kayenta Mine Highway 160, Navajo Route 41 P.O. Box 650 Kayenta, Arizona 86033 928.677.5177

June 17, 2020

Chilchinbeto Chapter Mr. Thomas Bradley, President P.O. Box 1681 Kayenta, Arizona 86033

RE: Notice of Application for Phase I Bond Release; J19, J19W, and N9 Coal Resource Areas; Kayenta Mine

Dear Mr. Bradley:

Peabody Western Coal Company (PWCC) has filed an application with the Office of Surface Mining Reclamation and Enforcement (OSMRE) for Phase I bond release on portions of the J19, J19W, and N9 Coal Resource Areas. The release areas are in the northwestern and southeastern portion of the PWCC lease area. PWCC is seeking release from Phase I bond liability for those surety bonds currently held with Zurich American Insurance Company, Continental Casualty Company, National Fire Insurance Company of Hartford, Liberty Mutual Insurance Company, Federal Insurance Company, Indemnity National Insurance Company, and Travelers Casualty and Surety Company of America. The total combined bond for Kayenta Mine is \$178,569,992.

The Phase I bond release areas are located within the Kayenta Mine Permanent Program permit area (AZ-0001F PAP) in the northwestern and southeastern portions of the PWCC lease area. PWCC is seeking a reduction of the total J19, J19W, and N9 bond amount of \$20,299,758 at this time by gaining regulatory approval for release of lands described in the application from Phase I bond liability. The total area sought for release includes 929 acres of disturbed land. Approval of Phase I will allow for Phase II and III bond release to proceed on these areas once all requirements for this phase are met. Phase III is the final bond release step and once approved will allow for the planned return of these lands to the Navajo Nation in the future. Until that time, PWCC will continue to control and manage reclaimed lands in the release areas described.

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Navajo Nation Minerals Dept.	Forest Lake Chapter House
Office of Surface Mining	Navajo Route 41
Window Rock Boulevard	14 miles North of Pinon
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Mr. Thomas Bradley June 17, 2020 Page 2 of 2

> Office of Surface Mining Reclamation and Enforcement Western Region Office 1999 Broadway, Suite 3320 Denver, CO 80202-3050

Hopi Tribe Office of Mining and Mineral Resources, Highway 264 1 Mile East of Kykotsmovi Kykotsmovi, AZ 86039

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Mr. Jeremy Spangler Western Region Office Office of Surface Mining Reclamation & Enforcement 1999 Broadway, Suite 3320 Denver, CO 80202-3050 303.293.5022

Please direct your questions about this application to me at 928.677.5130 or email them to me at mshepherd2@peabodyenergy.com.

Respectfully,

Marie Shepherd Senior Manager Environmental Kayenta Mine



PEABODY WESTERN COAL COMPANY Kayenta Mine Highway 160, Navajo Route 41 P.O. Box 650 Kayenta, Arizona 86033 928.677.5177

June 17, 2020

Forest Lake Chapter Ms. Fern Benally, President P.O. Box 441 Pinon, Arizona 86510

RE: Notice of Application for Phase I Bond Release; J19, J19W, and N9 Coal Resource Areas; Kayenta Mine

Dear Ms. Benally:

Peabody Western Coal Company (PWCC) has filed an application with the Office of Surface Mining Reclamation and Enforcement (OSMRE) for Phase I bond release on portions of the J19, J19W, and N9 Coal Resource Areas. The release areas are in the northwestern and southeastern portion of the PWCC lease area. PWCC is seeking release from Phase I bond liability for those surety bonds currently held with Zurich American Insurance Company, Continental Casualty Company, National Fire Insurance Company of Hartford, Liberty Mutual Insurance Company, Federal Insurance Company, Indemnity National Insurance Company, and Travelers Casualty and Surety Company of America. The total combined bond for Kayenta Mine is \$178,569,992.

The Phase I bond release areas are located within the Kayenta Mine Permanent Program permit area (AZ-0001F PAP) in the northwestern and southeastern portions of the PWCC lease area. PWCC is seeking a reduction of the total J19, J19W, and N9 bond amount of \$20,299,758 at this time by gaining regulatory approval for release of lands described in the application from Phase I bond liability. The total area sought for release includes 929 acres of disturbed land. Approval of Phase I will allow for Phase II and III bond release to proceed on these areas once all requirements for this phase are met. Phase III is the final bond release step and once approved will allow for the planned return of these lands to the Navajo Nation in the future. Until that time, PWCC will continue to control and manage reclaimed lands in the release areas described.

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Navajo Nation Minerals Dept.	Forest Lake Chapter House
Office of Surface Mining	Navajo Route 41
Window Rock Boulevard	14 miles North of Pinon
Window Rock, AZ 86515	Pinon, AZ 86510

Ms. Fern Benally June 17, 2020 Page 2 of 2

> Office of Surface Mining Reclamation and Enforcement Western Region Office 1999 Broadway, Suite 3320 Denver, CO 80202-3050

Hopi Tribe Office of Mining and Mineral Resources, Highway 264 1 Mile East of Kykotsmovi Kykotsmovi, AZ 86039

If you have questions, comments, or wish to request a hearing or informal conference regarding this bond release application, please contact:

Mr. Jeremy Spangler Western Region Office Office of Surface Mining Reclamation & Enforcement 1999 Broadway, Suite 3320 Denver, CO 80202-3050 303.293.5022

Please direct your questions about this application to me at 928.677.5130 or email them to me at mshepherd2@peabodyenergy.com.

Respectfully,

Marie Shepherd Senior Manager Environmental Kayenta Mine



PEABODY WESTERN COAL COMPANY Kayenta Mine Highway 160, Navajo Route 41 P.O. Box 650 Kayenta, Arizona 86033 928.677.5177

June 17, 2020

Navajo Nation Minerals Department Mr. Akhtar Zaman P.O. Box 1910 Window Rock, AZ 86515

RE: Notice of Application for Phase I Bond Release; J19, J19W, and N9 Coal Resource Areas; Kayenta Mine

Dear Mr. Zaman:

Peabody Western Coal Company (PWCC) has filed an application with the Office of Surface Mining Reclamation and Enforcement (OSMRE) for Phase I bond release on portions of the J19, J19W, and N9 Coal Resource Areas. The release areas are in the northwestern and southeastern portion of the PWCC lease area. PWCC is seeking release from Phase I bond liability for those surety bonds currently held with Zurich American Insurance Company, Continental Casualty Company, National Fire Insurance Company of Hartford, Liberty Mutual Insurance Company, Federal Insurance Company, Indemnity National Insurance Company, and Travelers Casualty and Surety Company of America. The total combined bond for Kayenta Mine is \$178,569,992.

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Navajo Nation Minerals Dept.	Forest Lake Chapter House
Office of Surface Mining	Navajo Route 41
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Mr. Akhtar Zaman June 17, 2020 Page 2 of 2

> Office of Surface Mining Reclamation and Enforcement Western Region Office 1999 Broadway, Suite 3320 Denver, CO 80202-3050

Hopi Tribe Office of Mining and Mineral Resources, Highway 264 1 Mile East of Kykotsmovi Kykotsmovi, AZ 86039

If you have questions, comments, or wish to request a hearing or informal conference regarding this bond release application, please contact:

Mr. Jeremy Spangler Western Region Office Office of Surface Mining Reclamation & Enforcement 1999 Broadway, Suite 3320 Denver, CO 80202-3050 303.293.5022

Please direct your questions about this application to me at 928.677.5130 or email them to me at mshepherd2@peabodyenergy.com.

Respectfully,

Marie Shepherd Senior Manager Environmental Kayenta Mine



PEABODY WESTERN COAL COMPANY Kayenta Mine Highway 160, Navajo Route 41 P.O. Box 650 Kayenta, Arizona 86033 928.677.5177

June 17, 2020

The Hopi Tribe Office of Mining and Minerals Attn: Norman Honie Jr. P.O. Box 123 Kykotsmovi, AZ 86039

RE: Notice of Application for Phase I Bond Release; J19, J19W, and N9 Coal Resource Areas; Kayenta Mine

Dear Mr. Honie:

Peabody Western Coal Company (PWCC) has filed an application with the Office of Surface Mining Reclamation and Enforcement (OSMRE) for Phase I bond release on portions of the J19, J19W, and N9 Coal Resource Areas. The release areas are in the northwestern and southeastern portion of the PWCC lease area. PWCC is seeking release from Phase I bond liability for those surety bonds currently held with Zurich American Insurance Company, Continental Casualty Company, National Fire Insurance Company of Hartford, Liberty Mutual Insurance Company, Federal Insurance Company, Indemnity National Insurance Company, and Travelers Casualty and Surety Company of America. The total combined bond for Kayenta Mine is \$178,569,992.

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Navajo Nation Minerals Dept.	Forest Lake Chapter House
Office of Surface Mining	Navajo Route 41
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Mr. Norman Honie, Jr. June 17, 2020 Page 2 of 2

> Office of Surface Mining Reclamation and Enforcement Western Region Office 1999 Broadway, Suite 3320 Denver, CO 80202-3050

Hopi Tribe Office of Mining and Mineral Resources, Highway 264 1 Mile East of Kykotsmovi Kykotsmovi, AZ 86039

If you have questions, comments, or wish to request a hearing or informal conference regarding this bond release application, please contact:

Mr. Jeremy Spangler Western Region Office Office of Surface Mining Reclamation & Enforcement 1999 Broadway, Suite 3320 Denver, CO 80202-3050 303.293.5022

Please direct your questions about this application to me at 928.677.5130 or email them to me at mshepherd2@peabodyenergy.com.

Respectfully,

Marie Shepherd Senior Manager Environmental Kayenta Mine



PEABODY WESTERN COAL COMPANY Kayenta Mine Highway 160, Navajo Route 41 P.O. Box 650 Kayenta, Arizona 86033 928.677.5177

June 17, 2020

Navajo Tribal Utility Authority Mr. Walter W. Haase, P.E., General Manager P.O. Box 170 Fort Defiance, Arizona 86504-0170

RE: Notice of Application for Phase I Bond Release; J19, J19W, and N9 Coal Resource Areas; Kayenta Mine

Dear Mr. Haase:

Peabody Western Coal Company (PWCC) has filed an application with the Office of Surface Mining Reclamation and Enforcement (OSMRE) for Phase I bond release on portions of the J19, J19W, and N9 Coal Resource Areas. The release areas are in the northwestern and southeastern portion of the PWCC lease area. PWCC is seeking release from Phase I bond liability for those surety bonds currently held with Zurich American Insurance Company, Continental Casualty Company, National Fire Insurance Company of Hartford, Liberty Mutual Insurance Company, Federal Insurance Company, Indemnity National Insurance Company, and Travelers Casualty and Surety Company of America. The total combined bond for Kayenta Mine is \$178,569,992.

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Navajo Nation Minerals Dept.	Forest Lake Chapter House
Office of Surface Mining	Navajo Route 41
Window Rock Boulevard	14 miles North of Pinon
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Mr. Walter W. Haase June 17, 2020 Page 2 of 2

> Office of Surface Mining Reclamation and Enforcement Western Region Office 1999 Broadway, Suite 3320 Denver, CO 80202-3050

Hopi Tribe Office of Mining and Mineral Resources, Highway 264 1 Mile East of Kykotsmovi Kykotsmovi, AZ 86039

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Mr. Jeremy Spangler Western Region Office Office of Surface Mining Reclamation & Enforcement 1999 Broadway, Suite 3320 Denver, CO 80202-3050 303.293.5022

Please direct your questions about this application to me at 928.677.5130 or email them to me at mshepherd2@peabodyenergy.com.

Respectfully,

Marie Shepherd Senior Manager Environmental Kayenta Mine



PEABODY WESTERN COAL COMPANY Kayenta Mine Highway 160, Navajo Route 41 P.O. Box 650 Kayenta, Arizona 86033 928.677.5177

June 17, 2020

Shonto Chapter Ms. Elizabeth Whitethorne-Benally P. O. Box 7800 Shonto, AZ 86054

RE: Notice of Application for Phase I Bond Release; J19, J19W, and N9 Coal Resource Areas; Kayenta Mine

Dear Ms. Whitethorne-Benally:

Peabody Western Coal Company (PWCC) has filed an application with the Office of Surface Mining Reclamation and Enforcement (OSMRE) for Phase I bond release on portions of the J19, J19W, and N9 Coal Resource Areas. The release areas are in the northwestern and southeastern portion of the PWCC lease area. PWCC is seeking release from Phase I bond liability for those surety bonds currently held with Zurich American Insurance Company, Continental Casualty Company, National Fire Insurance Company of Hartford, Liberty Mutual Insurance Company, Federal Insurance Company, Indemnity National Insurance Company, and Travelers Casualty and Surety Company of America. The total combined bond for Kayenta Mine is \$178,569,992.

The Phase I bond release areas are located within the Kayenta Mine Permanent Program permit area (AZ-0001F PAP) in the northwestern and southeastern portions of the PWCC lease area. PWCC is seeking a reduction of the total J19, J19W, and N9 bond amount of \$20,299,758 at this time by gaining regulatory approval for release of lands described in the application from Phase I bond liability. The total area sought for release includes 929 acres of disturbed land. Approval of Phase I will allow for Phase II and III bond release to proceed on these areas once all requirements for this phase are met. Phase III is the final bond release step and once approved will allow for the planned return of these lands to the Navajo Nation in the future. Until that time, PWCC will continue to control and manage reclaimed lands in the release areas described.

Reclamation of the Phase I release areas which includes; backfilling and grading, drainage control, mitigation of unsuitable material, and topsoil replacement was completed between 1999 and 2019. All reclamation activities were conducted in accordance with the Surface Mining Control and Reclamation Act (SMCRA) and the requirements of the OSMRE Permit AZ-0001F PAP approved October 3, 2017. Reclamation activities are documented in annual reports submitted previously to OSMRE.

Navajo Nation Minerals Dept.	Forest Lake Chapter House
Office of Surface Mining	Navajo Route 41
Window Rock Boulevard	14 miles North of Pinon
Window Rock, AZ 86515	Pinon, AZ 86510

Ms. Elizabeth Whitethorne-Benally June 17, 2020 Page 2 of 2

> Office of Surface Mining Reclamation and Enforcement Western Region Office 1999 Broadway, Suite 3320 Denver, CO 80202-3050

Hopi Tribe Office of Mining and Mineral Resources, Highway 264 1 Mile East of Kykotsmovi Kykotsmovi, AZ 86039

If you have questions, comments, or wish to request a hearing or informal conference regarding this bond release application, please contact:

Mr. Jeremy Spangler Western Region Office Office of Surface Mining Reclamation & Enforcement 1999 Broadway, Suite 3320 Denver, CO 80202-3050 303.293.5022

Please direct your questions about this application to me at 928.677.5130 or email them to me at mshepherd2@peabodyenergy.com.

Respectfully,

Marie Shepherd Senior Manager Environmental Kayenta Mine

PUBLIC NOTICE

Peabody Western Coal Company (PWCC) has filed an application with the Office of Surface Mining Reclamation and Enforcement (OSMRE) for bond release on a portion of the lands in the J19, J19W, and N9 Coal Resource Areas (CRAs) within the Kayenta Mine Permit AZ-0001F. PWCC is seeking a release of Phase I bond liability for a portion of the J19, J19W, and N9 areas currently under bond with Zurich American Insurance Company, Continental Casualty Company, National Fire Insurance Company of Hartford, Federal Insurance Company, Liberty Mutual Insurance Company, Indemnity National Insurance Company, and Travelers Casualty and Surety Company of America. PWCC is seeking a reduction in bond of \$20,299,758 under the Phase I application from the total J19, J19W, and N9 bond amount of \$79,830,381. The total combined bond for Kayenta Mine is \$178,569,992.

The Phase I bond release application consists of information currently contained in the AZ-0001F permit application package (PAP) approved October 3, 2017. The PAP outlines PWCC's reclamation operations on Permanent Program Lands. The total areas in J19, J19W, and N9 requested for Phase I release is 929 acres. Reclamation was completed between 1999 and 2019. Reclamation activities were completed in accordance with the approved PAP and included backfilling, grading, and replacement of suitable soil or plant growth media. Other reclamation activities included mitigation of unsuitable material and drainage control construction. The Kayenta Mine permit for the release areas is under Navajo Tribal Coal Lease 14-20-0603-9910, Navajo Tribal Coal Lease 14-20-0603-8580, and Hopi Tribal Coal Lease 14-20-0450-5743 and operates pursuant to Code of Federal Regulations (CFR), Title 30; Subchapter E, Part 750; Subchapter G, Parts 773 and 774; and Subchapter K, Parts 810 and 816. This notice is hereby given that:

1. The name and business address of the applicant is:

Peabody Western Coal Company Kayenta Mine P.O. Box 650 Kayenta, AZ 86033

2. The mine permit area is located approximately 18 miles south southwest of Kayenta, Arizona. The permit area for the Phase I bond release areas is located in USGS 7.5 minute quadrangle maps "Yucca Hill" and "Long House Valley" within the following lands of Navajo County, Arizona that are described relative to the Gila and Salt River Base Meridian as:

A total of 267 acres of land located within the J19 CRA. The computer-generated centroid location is Latitude $36^\circ~26'~45.4''$ N and Longitude $110^\circ~17'$

54.9" W. A total of 251 acres of land located within the J19W CRA. The computer-generated centroid location is Latitude $36^{\circ} 26' 57.0"$ N and Longitude $110^{\circ} 19' 41.7"$ W. A total of 411 acres of land located within the N9 CRA. The computer-generated centroid location is Latitude $36^{\circ} 33' 43.5"$ N and Longitude $110^{\circ} 24' 59.2"$ W.

3. Locations of where copies of the application and permit are available for public review and/or inspection are:

Navajo Nation Minerals Department	Forest Lake Chapter House
Office of Surface Mining	Navajo Route 41
Window Rock Boulevard	20 Miles North of Pinon
Window Rock, AZ 86515	Pinon, AZ 86510

Office of Surface Mining	Hopi Tribe
Reclamation and Enforcement	Office of Mining and Mineral
Western Region Office	Resources, Highway 264
1999 Broadway, Suite 3320	1 Mile East of Kykotsmovi
Denver, CO 80202-3050	Kykotsmovi, AZ 86039

4. The name and address of the OSMRE-WRO representative where written comments, objections, requests for a public hearing, or requests for an informal conference may be submitted on or before 5:00 p.m., (Date To Be Determined), thirty (30) days after the last publication date are:

Mr. Jeremy Spangler Western Region Office Office of Surface Mining Reclamation & Enforcement 1999 Broadway, Suite 3320 Denver, CO 80202-3050 303.293.5022

- Interested persons may obtain more information concerning the bond release by contacting Marie Shepherd, Senior Manager Environmental for PWCC at 928.677.5130.
- 6. The application has been filed with OSMRE and will be acted upon pursuant to the Permanent Regulatory Program (30 CFR Parts 750 and 774) approved by the Secretary of the Interior under Title V of the Surface mining Control and Reclamation Act of 1977.

SECTION 1

Phase I Bond Release Supporting Documentation

Introduction

Peabody Western Coal Company (PWCC) is requesting Phase I bond release on portions of lands within the J19, J19-West (J19W), and N9 areas of Kayenta Mine. The bond release application included in this submittal contains required documentation and information to support Phase I bond release for 929 acres of mined and reclaimed lands in the permanent program areas within the J19 (267 acres) Coal Resource Area (CRA), J19W (251 acres) CRA, and N9 (411 acres) CRA as shown on Maps 1.1.1 and 1.1.2. None of the proposed permanent ponds or a request for permanent roads is included in this release application. These features will be further evaluated in relation to the final land use and customary use areas over the entire release application areas. Information for the Phase I technical portions of the application are contained in Section 2 of this document. Information such as the public notice, affidavit of publication, and copies of letters to the Tribes, government agencies, and utilities are included in this section of the application.

Permit and Bond Release Summary Information

The J19 and J19W CRAs are located within the southeastern portion of PWCC's Kayenta Mine. The N9 CRA is located within the northwestern portion of PWCC's Kayenta Mine. The Kayenta Mine operates under Permit AZ-0001F issued by the Office of Surface Mining Reclamation and Enforcement (OSMRE) to PWCC Kayenta Mine on October 3, 2017. Permit AZ-0001F authorized continuation of ongoing Kayenta Mine surface coal mining and reclamation activities in CRAs N9, J19, J19W, and J21, as well as to perform reclamation activities in CRAs previously mined (i.e. N11) for the 5-year period July 2015 through July 2020. The 5-year renewal application for Permit AZ-0001F was submitted to OSMRE on February 27, 2020.

The Kayenta mine permit area is located approximately 18 miles south southwest of Kayenta, Arizona (USGS 7.5 minute quadrangle maps Longhouse Valley, Marsh Pass S.E., Owl Spring, Great Spring, Yucca Hill, and Cliff Rose Hill). The permit areas for the J19, J19W, and N9 Phase I bond release are located within the following lands of Navajo County, Arizona that are described relative to the Gila and Salt River Base Meridian as:

A total of 267 acres of mined and reclaimed land located within the J19 CRA. The computer-generated centroid location of this area is approximately Latitude 36° 26' 45.4" N and Longitude 110° 17' 54.9" W. A total of 251 acres of mined and reclaimed land located within the J19W CRA. The computer-generated centroid

1. 1

location of this area is approximately Latitude 36° 26′ 57.0″ N and Longitude 110° 19′ 41.7″ W. A total of 411 acres of mined and reclaimed land located within the N9 CRA. The computer-generated centroid location of this area is approximately Latitude 36° 33′ 43.5″ N and Longitude 110° 24′ 59.2″ W.

The type of bond and the amount of bond filed for Kayenta Mine Permit AZ-0001F are described in Table 1.1. The portion requested for release in the J19, J19W, and N9 CRAs includes \$20,299,758 for Phase I. Justification for the release dollars are explained in the following section.

Table 1.1. Bond Information for Kayenta Mine.		
Bond Surety	Bond Number	Bond Amount
Continental Casualty Company & National Fire		
Insurance Company of Hartford	9264222	\$28,304,188
Continental Casualty Company of Chicago & National		
Fire Insurance Company of Hartford	9264224	\$8,167,651
Indemnity National Insurance Company	N-7003484	\$7,250,000
Federal Insurance Company	82154865	\$10,797,629
Liberty Mutual Insurance Company	60S003887	\$29,012,760
Travelers Casualty and Surety Company of America	105243347	\$23,847,246
Travelers Casualty and Surety Company of America	105191031	\$28,000,000
Zurich American Insurance Company	8940860	\$43,190,518
TOTAL		\$178,569,992

Phase I Bond Reduction Cost

PWCC is seeking a reduction in bond for Phase I in the amount of \$20,299,758. This amount was determined using direct and indirect unit costs calculated for 267 acres in J19, 251 acres in J19W, and 411 acres in N9 as documented in Permit AZ-0001F, Chapter 24, Table 24-1-4. Reclamation cost estimates as of July 2017 ("worst case" or "highest liability" as approved in Permit AZ-0001F by OSMRE on October 3, 2017) were used and these rates were adjusted for inflation through June 2020. Reduction in bond at the J19W CRA was based upon 19,500 feet of the final pit being 100% backfilled (total bonded pit length is 32,100 feet - Table 24-2-1) and completion of Phase I reclamation activities including general grading on 251 acres and replacing four feet of suitable plant growth material including one foot of soil material on the surface of 247 acres of final graded lands per Chapter 22, Minesoil Reconstruction, Volume 11, Permit AZ-0001F. OSMRE released 2,400 feet of reduced highwall and backfilled pit from Phase I bond on January 4, 2017. OSMRE released 6,500 feet of highwall and backfilled pit from Phase I bond on July 25, 2018. Reduction in bond at J19 was based upon completion of Phase I reclamation activities including general grading on 267 acres and replacing four feet of suitable plant growth material including one foot of soil material on the surface of 163 acres of final graded lands per Chapter 22, Minesoil Reconstruction, Volume 11, Permit AZ-0001F. Reduction in bond at N9 was based upon completion of Phase I reclamation activities including general grading on 411 acres and replacing four feet of suitable plant growth material including one foot of soil material on the surface of 286 acres of final graded lands per Chapter 22, Minesoil Reconstruction, Volume 11, Permit AZ-0001F. Suitable plant growth material replacement areas are documented for the J19W, J19, and N9 CRAs on Maps 2.1.1, 2.1.2, 2.2.1, and 2.2.2 in Section 2 of this document.

The project categories and direct costs applicable to this Phase I bond release are listed in Table 1.2.1 for the J19W CRA, Table 1.2.2 for the J19 CRA, and Table 1.2.3 for the N9 CRA. PWCC is not requesting full release of the grading and ripping maintenance costs for the disturbed lands because these are considered by OSMRE to be Phase II reclamation activities. Similarly, no costs have been requested on the disturbed lands for the Phase III reclamation activities including surface stabilization, revegetation, and vegetation maintenance. The combined total bond reduction direct costs shown in Tables 1.2.1, 1.2.2, and 1.2.3 is \$16,571,234.

Table 1.2.1	
Bond Reduction of Direct Costs for Backfilling, Grading, Suitable Material Replacement,	
and Soil Material Replacement i	n the J19W CRA.
Project Category	Bond Reduction Amount
Cast/blast high wall (10,600 feet)	\$2,478,741
Doze high wall (10,600 feet)	\$1,505,783
Doze first two spoils (10,600 feet)	\$1,407,633
Doze back two spoils (10,600 feet)	\$ 331,968
Backfill and grade ramps (10,600 feet)	\$ 674,372
General grading (251 ac @ \$4,127.70/ac)	\$1,036,053
Suitable material replacement (247 ac @ \$0.98/yd)	\$ 937,256
Soil material replacement (247 ac @ \$1.32/yd)	\$ 841,618
Total Direct Cost Category I	\$9,213,424
Inflation July 2017 thru June 2020 (5.85%)	\$ 538,985
Total Direct Cost Category I (Inflated to 6-2020)	\$9,752,409

Table 1.2.2	
Bond Reduction of Direct Costs for Grading, Suitab	ble Material Replacement, and Soil
Material Replacement in th	e J19 CRA.
Project Category	Bond Reduction Amount
General grading (267 ac @ 4,127.70/ac)	\$1,102,096
Suitable material replacement (163 ac @ \$0.98/yd)	\$ 618,513
Soil material replacement (163 ac @ \$1.32/yd)	\$ 555,400
Total Direct Cost Category I	\$2,276,009
Inflation July 2017 thru June 2020 (5.85%)	\$ 133,147
Total Direct Cost Category I	\$2,409,156

Table 1.2.3	
Bond Reduction of Direct Costs for Grading, Suitable	Material Replacement, and Soil
Material Replacement in the	N9 CRA.
Project Category	Bond Reduction Amount
General grading (411 ac @\$4,127.68/ ac)	\$1,696,476
Suitable material replacement (286 ac @ \$1.11/yd)	\$1,229,205
Soil material replacement (286 ac @ \$1.68/yd)	\$1,240,279
Total Direct Cost Category I	\$4,165,960
Inflation July 2017 thru June 2020 (5.85%)	\$ 243,709
Total Direct Cost Category I (Inflated to 6-2020)	\$4,409,669

Tables 1.3.1, 1.3.2, and 1.3.3 show the indirect costs obtained from Permit AZ-0001F, Chapter 24 that are associated with the J19W, J19, and N9 Phase I direct cost, respectively as determined in July 2017. The total indirect cost reflects inflation through June 2020 (5.85%). The combined total bond reduction indirect costs shown in Tables 1.3.1, 1.3.2, and 1.3.3 is \$3,728,524.

Table 1.3.1 Bond Reduction of Indirect Costs for Backfilling, Grading, Suitable Material Replacement, and Soil Material Replacement in the J19W CRA.	
Project Category	Bond Reduction Amount
Mobilization/demobilization (1.5%)	\$ 146,286
Contingencies (2.0%)	\$ 195,048
Engineering redesign fee (2.0%)	\$ 195,048
Contractor profit and overhead (15.0%)	\$1,462,861

Reclamation management fee (2.0%)	\$ 195,048
Total Indirect Cost	\$2,194,291

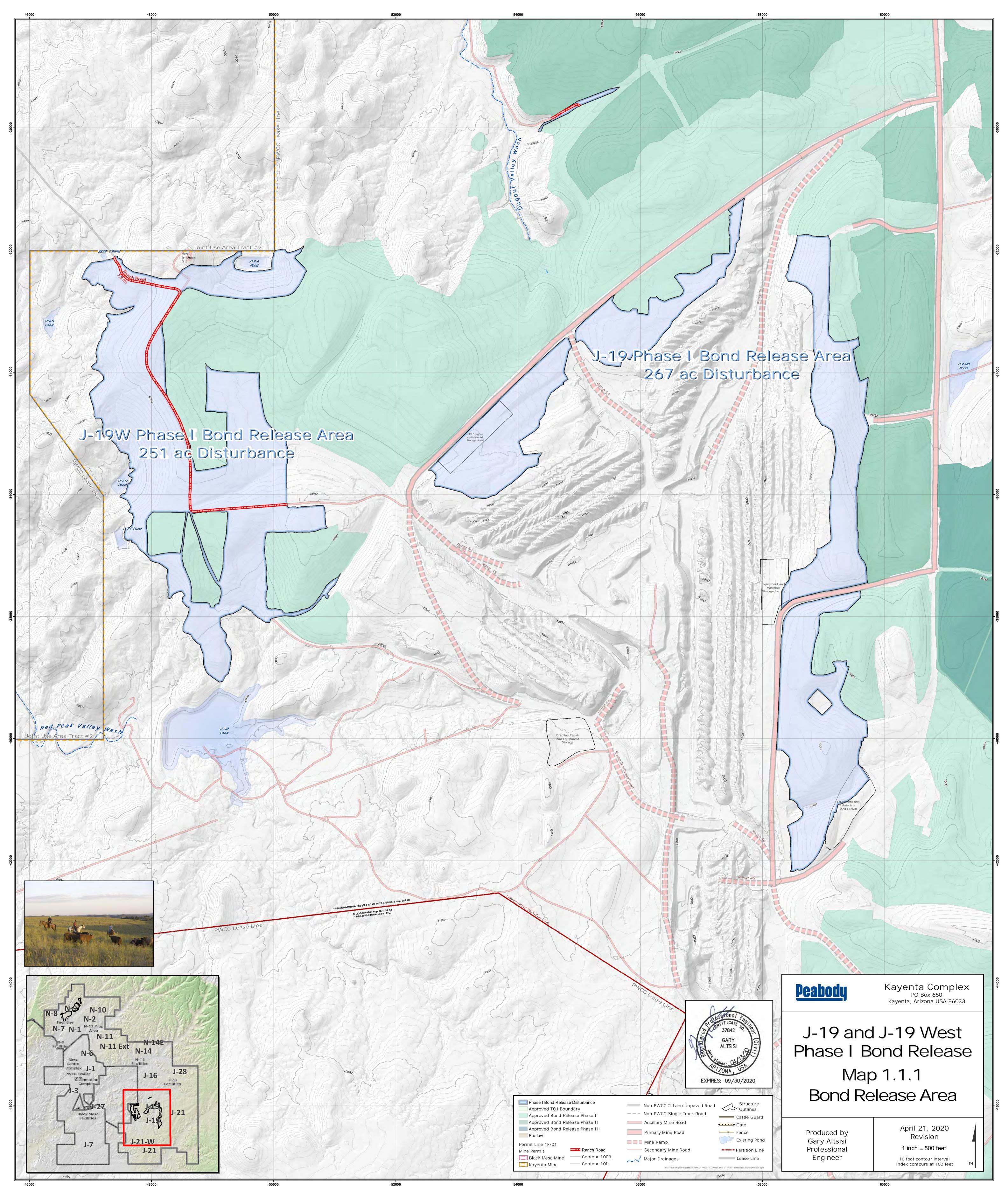
Table 1.3.2	
Bond Reduction of Indirect Costs for Gradi	ng, Suitable Material Replacement, and Soil
Material Replaceme	ent in the J19 CRA.
Project Category	Bond Reduction Amount
Mobilization/demobilization (1.5%)	\$ 36,137
Contingencies (2.0%)	\$ 48,183
Engineering redesign fee (2.0%)	\$ 48,183
Contractor profit and overhead (15.0%)	\$361,373
Reclamation management fee (2.0%)	\$ 48,183
Total Indirect Cost	\$542,059

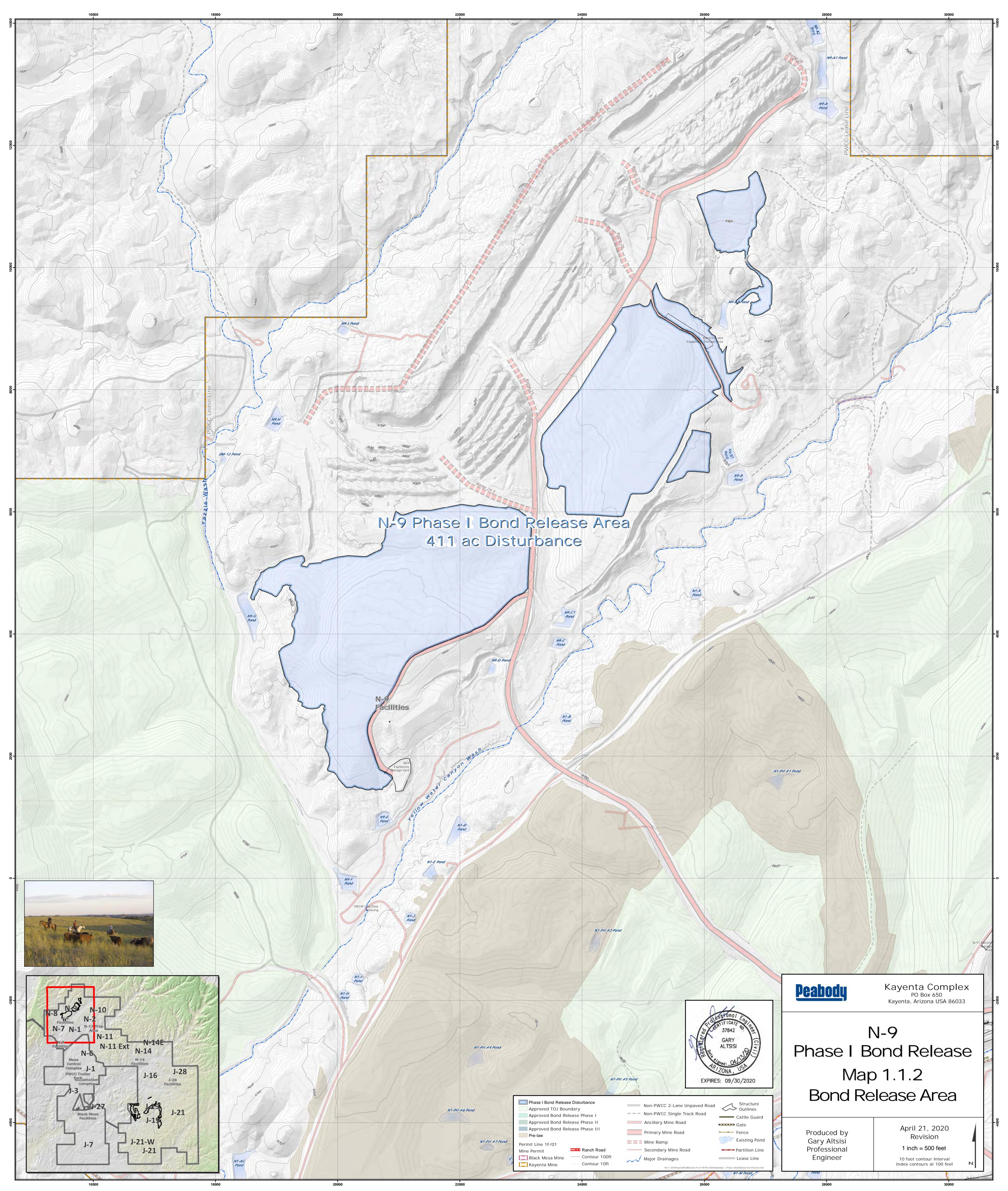
Table 1.3.3 Bond Reduction of Indirect Costs for Grading, Suitable Material Replacement, and Soil Material Replacement in the N9 CRA.	
Project Category	Bond Reduction Amount
Mobilization/demobilization (1.5%)	\$ 66,145
Contingencies (2.0%)	\$ 88,193
Engineering redesign fee (2.0%)	\$ 88,193
Contractor profit and overhead (15.0%)	\$661,450
Reclamation management fee (2.0%)	\$ 88,193
Total Indirect Cost	\$992,174

The total direct, indirect, tax, and 2017 - 2020 inflation costs for Phase I bond categories in the J19W, J19, and N9 CRAs are \$20,299,758.

Permanent Facilities

There are no requests included in this J19 and N9 Phase I bond release application for any facilities to be retained as permanent features. None of the sediment ponds (including those proposed as permanent), roads, or Kayenta Mine support facilities located within the J19 and N9 CRAs are included in this Phase I bond release application. The two-track ranch road shown within the J19W portion of the release area will continue to be used for access to monitor the J19-A, J19-D, and J19-E sediment ponds, for compliance-related inspections, for reclamation maintenance, other environmental monitoring, and local access by residents.





%cAcos	1,118 1,443 1,606
PYRS A-B TINHODOTN	
PVR A POT TN/1000TN	
A-B POT TN/1000TN	3.60 9.99 5.24
NEUT POT TN/100TN	11.2 14.4 16.1
ACID POT TV1000TN	7.57 4.45 10.8
ora s%	
%s syd	
SULFATE S%	
TOT S %	0.242 0.142 0.347
OLASS	o co CLC
V CLAY	42.5 40.0 40.0
א sורד גערי	30.0 28.8 22.5
% SAND	27.5 31.3 37.5
SAR	8,30 2.55 2.28
sodium Meq/L	47.0 15.6 15.4
MAGNESIUM	42.3 53.0 66.6
CALCIUM	21.9 22.0 24.9
% SAT	51.3 44.9 43.8
PH UNITS EC. MMHOIOM	6.31 4.66 5.04
STINU H	6.21 6.58 6.68
SAMPLE	0-1 1-2 2-3 2-3
IPLE DATE	11/15/99 11/15/99 11/15/99
ACCULARS # LOCATION SAM	58RG24 58RG24 58RG24
COLLABS #	PB-1861 PB-1862 PB-1863

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5,63 4,24
7,4 7,8
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9c sample_id 45 RG 26 46 RG 26
lab_id 0302504202 0302504203

%CACD3	0.495	1.386	0.644	0.594	0.248	1.287		
TN/1000TN	-9.36	0.18	-7.75	-7.62	-14.1	12.7		
TW1000TN	14.3	13.7	14.2	13.6	16.5	0.19		
TN/1000TN	-24.5	-18.5	-23.4	-23.8	-34.8	9.16		
NEUT POT TN/1000TN	4.95	13.9	6.44	5.94	2.48	12.9		
ACID POT TN/1000TN	29.4	32.4	29.8	29.8	37.3	3.71		
ORG S%								
PYR S %	0.458	0.438	0.454	0.434	0.529	0.006		
SULFATE S%								
TOT S %	0.942	1.036	0.955	0.953	1.194	0.119		
CLASS	,E,	-	CL	CL	۲		CL	
% CLAY	23.8	25.0	27.5	27.5	26,3		35.0	
% SILT	37.5	33.8	36.3	35.0	36.3		31.3	
% SAND	38.8	41.3	36.3	37.5	37.5		33.8	
SAR	15.9	18.0	11.8	12.4	13.1		7.94	
SODIUM	88.3	91,8	66.1	74.4	93.1		30.6	
MAGNESIUM	39.5	29.4	40.3	46.2	75.6		11.1	
MEGIL	22.2	22.7	22.2	25.3	24.7		18.6	
% SAT	42.5	42.7	42.6	41.7	41.8		52.8	
EC MMHO/CM	10,6	9.71	8,80	9.12	11.6		4.53	
PH UNITS	6.22	6.66	6,37	6.33	5,34		7.00	
DEPTH	0-1.	1-3'	0-1.	0-1.	1-3			
SAMPLE DATE	5/15/2003	5/15/2003	5/15/2003	5/15/2003	5/15/2003			
LOCATION	100			46RG35				
GAL#							2C-23	SC1-001

%CACO3	1.251	0.741	1.251		
PYRS A-B TN/1000TN		5.75	12.5		
TW/1000TN		1.66	00.00		
A-B POT TN/1000TN	7.25	-0.78	9.08		
NEUT POT TN/1000TN	12.5	7.41	12.5		
ACID POT TN/1000TN	5.26	8.19	3.43		
ORG 8%					
PYR S %		0.053	0.000		
SULFATE S% PYR S %					
TOT S % S	0.168	0.262	0.110		
CLASS	ы	ы		C	
% DLAY	36.25	33.75		35.00	
% SILT	28.75	25.00		30.00	
W SAND	35.00	41.25		35.00	
SAR	25.5	17,5		8.52	
SODIUM MEQ/L	53.5	63.1		29.9	
MAGNESIUM MEQIL	3.75	11.7		8.72	
MEQU	5.04	14.3		15.9	
% SAT	41.6	40.4		49.4	
EC MMHO/CM	5.81	7.50		4.43	
PH UNITS	8.09	6.87		7.20	
SAMPLE	0-1	1-3			
SAMPLE DATE					
LOCATION	43RG13	43RG13			
GAL #	S-4264	S-4265	QC-18	QC-25	SQC-346

%CACO3	1.044	0.841	0.236	0.438	1.448	1.650	3.299	3.703	3.501	1.448	1.549	2.054	1.347	2,458	2,559	0.942			
PYRS A-B TN/1000TN		6.35	-8.33	-1.65	5.57	8.31				8.20	6.39		6.47			8.86			
TN/1000TN		2.06	10.7	6.03	8.90	8.18				6.28	60.6		2.00			0.56			
A-B POT P TN/1000TN T	2.95	-4.33	-20.2	-14.3	-0.80	0.64	28.8	29.4	24.9	-6.13	-6.10	5.66	-5.18	2.87	0.71	5.67			
NEUT POT TN/1000TN TI	10.4	8.42	2.36	4.38	14.5	16.5	33.0	37.0	35.0	14.5	15.5	20.5	13.5	24.6	25.6	9.42			
AGID POT N TN/1000TN TI	7.49	12.7	22.6	18.7	15,3	15.9	4.18	7.63	10.1	20.6	21.6	14.9	18.6	21.7	24.9	3.76			
ORG 5%																			
PVR S %		0.066	0.342	0.193	0.285	0.262				0.201	0.291		0.224			0.018			
sulfate s% P																			
TOT S % SUL	0.240	0.408	0.723	0.599	0.489	0.507	0.134	0.244	0.324	0.660	0.691	0.476	0.597	0.695	0.796	0.120			
CLASS TO	CL		CL						Č,								CL		
% CLAY OI			36.25														35.00		
% SILT %			40.00 36								23.75 26				30.00 31		26.25 35		
% SAND			7 23.75														38.75		
A SAR	8.7(15.7				ļ			Î	Ì		j	Ì	1		8.51		
A SODIUM	37.6	41.8	63.1	58.7	38.4	38.3	17.8	26.9	69.69	40.4	54.8	47.4	62.2	57.4	63.1		29.1		
MAGNESIUM	17.2	18.6	15.5	17.4	9.13	9.38	27.0	12.3	19.1	22.1	20.2	13.4	23.1	11.5	12.8		8.23		
CALCIUM	20.1	19.2	17.0	18.2	12.9	13.3	18.7	17.1	17.2	18.1	21.2	17.4	17.4	18.1	18,8		15.2		
% SAT	48.3	49.0	47.6	48.5	50.3	52.4	38.9	44.1	40.5	43.2	40.5	44.6	46.6	47.3	45.7		51.3		
EC MMHO/OM	6.44	6.91	9.09	8.90	5.72	5,67	5.03	4.91	9.89	7.58	9.21	71.7	9.51	8.20	9.02		4.58		
PH UNITS	7.92	7.75	6.68	7,41	7.65	7,59	8.04	66'1	8.06	7.57	7.32	7.45	7,52	7.49	7.29		71.7		
SAMPLE	0-1	1-3	0-1	1-3	0-1	1-0	1-3	0-1	₽ 1	0-1	1-3	6-1	1-3	0-1	1-3				
SAMPLE DATE																			
LOCATION	41RG14	41RG14	41RG17	41RG17	45RG32	45RG32	45RG32	45RG33	45RG33	45RG34	45RG34	45RG35	45RG35	45RG36	45RG36				
GAL #	S-4332	-4333	-4338	-4339	-4340	1340R	4341	4342	4343	4344	4345	4346	4347	4348	4349	0C-18	C-26	SQC-01	

%CACO3	0.942	0.942	0,942	1,044		
PYRS A-B TN/1000TN						
PYR A POT TN/1000TN						
A-B POT TN/1000TN	2.37	1,33	6.41	6.56		
NEUT POT TN/1000TN	9.42	9.42	9.42	10.4		
ACID POT TN/1000TN	7.06	8.09	3.02	3.87		
ORG S%						
PYR S %						
SULFATE S%						
TOT S %	0.226	0.259	0.097	0.124		
CLASS	б	SCL	CL		С	
% OLAY	33.75	31.25	31.25		37.50	
% SILT	28.75	21.25	28.75		28.75	
% SAND	37.50	47.50	40.00		33.75	
SAR	6.45		2.40		8.66	
SODIUM MEQ/L	27,5	38.4	5.8		30.4	
MAGNESIUM	14.5	19.8	3.92		8.64	
DALCIUM	22.0	22.7	7.68		15,9	
% SAT	43.6	40.4	40.5		44,0	
EC MMHO/CM % SAT	5.41	6.85	1.71		4,93	
PH UNITS	7.27	7.09	7.59		6.95	
DEPTH	0-12"	12-28"	28-36"			
SAMPLE DATE	07/15/05	07/15/05	07/15/05			
LOCATION			41RG18			
GAL#					QC-26	100-07

Client: PWCC-Kyoran Mine Project: PWCC-Kyoran Mine 1-19 and 21 Area Project: 1-19 and 21 Area Analysis pH-Sarbs COND SAR CaSarbs Ma-Sarbs Sand Sili Workorden: H60100053 Manyati pH-Sarbs COND SAR CaSarbs Ma-Sarbs Sand Sand <th>LABORATORY ANALYTICAL REPORT</th> <th>SPORT</th> <th></th> <th></th> <th></th> <th></th>	LABORATORY ANALYTICAL REPORT	SPORT				
Analysis Units Client Sample ID Up Loi 3-001 41RG19, 0-1' 0 1 3-002 41RG19, 1-3' 1 3 3-003 41RG20, 0-1' 0 1 3-005 41RG21, 0-1' 0 1 3-005 41RG21, 1-3' 1 3 3-006 41RG21, 1-3' 1 3 3-005 41RG21, 1-3' 1 3 3-006 41RG21, 1-3' 1 3 3-005 41RG21, 1-3' 1 3 3-006 41RG21, 1-3' 1 3 3-005 41RG21, 1-3' 1 3 1 1 1 3 3 1 1 1 3 3 1 1 1 1 3 1 1 1 1 1 1 1 1 1 1 3 1 1 1 <th></th> <th></th> <th></th> <th>Repo Date Re</th> <th>Report Date: 10/13/06 Date Received: 10/05/06</th> <th>10/13/06</th>				Repo Date Re	Report Date: 10/13/06 Date Received: 10/05/06	10/13/06
Units Units ID Client Sample ID Up Lot 0653-001 41RG19, 0-1' 0 1 3 0653-002 41RG19, 1-3' 1 3 3 0653-005 41RG20, 1-3' 1 3 3 0653-005 41RG20, 1-3' 1 3 3 0653-005 41RG21, 1-3' 1 3 3 063-005 41RG21, 1-3' 1 1 3 053-005 41RG21, 1-3' 1 1 3 053-005 41RG21, 0-1'' 0 1 4	atPst Mg-SatPst	t Na-SatPst Sand	id Silt	Clay	Texture	Sulfur, Total
Description Othern Similyte ID Oph Lun 0653-001 41RG19, 0-1* 0 1 3 0653-005 41RG20, 1-3* 1 3 3 0653-005 41RG21, 0-1* 0 1 3 0053-005 41RG21, 0-1* 0 1 3 0053-005 41RG21, 0-1* 0 1 3 0053-005 41RG21, 1-3* 1 3 0053-005 41RG100053 Analysis Analysis 01 Client Sample 1D Up Low 053-003 41RG10, 0-1* 0 1 3				%	unitiess	%
0053-001 41RG19, 0-1' 0 1 0053-002 41RG20, 0-1' 0 1 0053-005 41RG20, 0-1' 0 1 0053-005 41RG21, 0-1' 0 1 0053-005 41RG21, 0-1' 0 1 0053-005 41RG21, 1-3' 1 3 0054 PW/CC-Kayenta Mine 1 1 1-19 and J21 Area Analysis rder: J-19 and J21 Area fder: J06100053 Analysis 053-002 41RG19, 0-1' 0 053-002 41RG19, 0-1' 0 1	*	S K	R	Results	Results	Results
0653-002 418.G19, 1-3' 1 3 0653-003 418.G20, 0-1' 0 1 0653-005 418.G21, 0-1' 0 1 0653-005 418.G21, 0-1' 0 1 0653-005 418.G21, 0-1' 0 1 053-005 418.G21, 1-3' 1 3 0653-005 418.G21, 1-3' 1 3 0753-005 418.G21, 1-3' 1 3 0753-005 418.G21, 1-3' 1 3 074 PW/CC-Kayenta Mine 1 1 1 121 Area Analysis rder: H06100053 Analysis 1 0 1 1 053-002 418.G19, 0-1' 0 1 053-003 418.G20, 0-1' 0 1			35	33	CL	0.22
063-003 41RG20, 0-1' 0 1 0653-006 41RG21, 0-1' 0 1 0653-005 41RG21, 1-3' 1 3 0653-006 41RG21, 1-3' 1 3 0653-006 41RG21, 1-3' 1 3 0653-005 41RG21, 1-3' 1 3 0653-006 41RG21, 1-3' 1 3 0653-005 41RG21, 1-3' 1 3 1 1-19 and 1/21 Area Analysis rder: 1-19 and 1/21 Area Inite 1 1/11 1 1 053-002 41RG19, 0-1' 0 1 053-003 41RG20, 0-1' 0 1				33	CL	0.25
0653-006 41RG21, 1-3' 1 3 1 9 94 121 Area 1 9 94 121 Area 1 9 94 121 Area 1 0 121 Area Analysis 053-002 41RG19, 0-1' 0 1 053-002 41RG19, 0-1' 0 1 053-003 41RG20, 0-1' 0 1				30	CL	0,34
0653-006 41RG21, 1-3' 1 3 0653-006 41RG21, 1-3' 1 3 ALABORATORIES FWCC-Kayenta Mine 1-19 and J21 Area H06100053 H06100053 Analysis Analysis 653-001 41RG19, 0-1' 0 1 053-002 41RG19, 0-1' 0 1 053-002 41RG19, 0-1' 0 1 053-003 41RG20, 0-1' 0 1			31	26	-	0.15
0053-006 41RG21, 1-3' 1 3 EAEORATORIES EAEORATORIES PWCC-Kayenta Mine 1 3 rder: J-19 and J21 Area Analysis rder: H06100053 Analysis D Client Sample 1D Up Low 053-002 41RG19, 0-1' 0 1 3		26.8 36		30	CL	0.25
ENERGY LABORATORIES PWCC-Kayenta Mine J-19 and J21 Area H06100053 Analysis Analysis O53-001 41RG19, 0-1' D53-002 41RG19, 0-1' 053-002 41RG19, 1-3' 053-003 41RG20, 0-1' 053-003 41RG30, 0-1' 053-003-003 41RG30, 0-1' 053-003-003-003-003-003-003-003-003-003-	13.1	17.1 34		32	ы	0.34
Analysis Sulfur, Sulfu	LYTICAL RE	PORT		Repor Date Re	Report Date: 10/13/06 Date Received: 10/05/06	3/06 5/06
Units % <td>at Acid tial Potential</td> <td>Acid/Base Potential</td> <td></td> <td></td> <td></td> <td></td>	at Acid tial Potential	Acid/Base Potential				
Client Sample ID Up Low Results Results Results 3-001 41RG19, 0-1' 0 1 3 0.10 0.12 0.03 3-002 41RG19, 1-3' 1 3 0.10 0.12 0.03 3-003 41RG20, 0-1' 0 1 0.14 0.17 0.02	t t/kt	t/kt				
41RG19, 0-1' 0 1 41RG19, 1-3' 1 3 0.10 0.12 0.03 41RG20, 0-1' 0 1 0.14 0.17 0.02	ilts Results	Results				
41RG19,1-3' 1 3 0.10 0.12 0.03 41RG20,0-1' 0 1 0.14 0.17 0.02		٠				
41RG20, 0-1' 0 1 0.14 0.17 0.02		0				
		0				
		3				
H06100053-005 41R(21, 0-1' 0 1 0.10 0.14 0.02 8	4.2	N				

CATI	ON SA	GAL # LOCATION SAMPLE DATE	SAMPLE	PH UNITS	EC MMHO/CM	% SAT	CALCIUM	MAGNESIUM MEQ/L	SODIUM	SAR	% SAND	% SILT	% CLAY	CLASS	% CAGOS	TOT S % S	SULFATE S%	PYR S %	%S DHO	ACID POT TN/1000TN	NEUT POT TN/1000TN	A-B POT TN/1000TN	PVR A POT TN/1000TN	PYRS A-B TN/1000TN
7		8/30/10	0-1	6.34	5.26	36.8	18.2	33.6	19.3	3.80	47.50	27.50	25.00	SCL	0.256	0.588		0.125		18.4	2.56	-15.8	3.91	-1.34
-		8/30/10	0-1	6.34	5.26	37.3	18.2	33.3	19.2	3.79	47.50	26.25	26.25	SCL	0.157	0.576		0.125		18.0	1.57	-16.4	3.91	-2.33
	61RG9 8	8/30/10	1-3	6.57	5.33	41.9	18.7	32.2	21.0	4.16	45.00	27.50	27.50	CL/SCL	0.454	0.492		0.121		15.4	4.54	-10.8	3.78	0.76
															0.949	0.183		0.034		5.73	9.49	3.76	1.06	8.42
				7.20	4.30	45.4	4.89	2.02	35.8	19.2	27.50	32.50	40.00	CL/C										

Acid/Base Potential, t/kt	206	4	4	47	ъņ	
Acid Potential, tikt						
Neut Potential, t/kt	06	2	-	0	0	
file, % Sulfur, Organie, %		0.11	0.09	0.14	0.10	
Sulfur, Pyritic, %					0.19	
Sultur, Sulfate, % Sulfur, Pyritic, 9					0.58	
Sulfur, Total, %	10.0	.86	.82	780	0.88	
SAR, unitless	0.84	4.66	4.82	4.98	5.32	
Na-SatPst, med/l						
Mq-SatPst, meg/	13.2	150	127	109	103	
Ca-SatPst, megh						
COND, mmhos/cm						
6 Texture, unitiess pH-SatPst, s u	6.6	(9)	ŝ	e	CL 3.	
Clay, % T						
% Silt.%						
2	S6/29/2011 17:00 22	16/29/2011 17:00 46	06/29/2011 17:00 40	16/29/2011 17:00 36	06/29/2011 17:00 38	
h Matrix	Soil	Soil	Soll	Soil	Soil	
	3. 1-3					
Sample(D ClientSamp(D H11070045 0.1*	H11070042-010 61RG15, 1-	1070042-023 61RG22, 0-1'	1070042-024 61RG22, 1-	1070042-025 61RG23, 0-1'	- M	

NINDOLAL MICONIAL MICONIAL				121120		1				MEQL	MEGAL	MEQIL	N SAI	1	WOIPLINE O	11	CINC LL	AMPLE DATE DEPTH PH UNITS ED MMHORCM	STIND HA
36.1 -4.08	0.01	0.89	1.16	-0.41	CL	28.75	30.00	41.25	8.04	60.6		94.1	19.4 94.1	4	38.1 19.4	9.45 38.1 19.4	9.45 38.1 19.4	1 3.73 9.45 38.1 19.4	0-1 3.73 9.45 38.1 19.4
33.7 -5.10	0.02	0.80	1.08	-0.51	сг	30.00	33.75	36.25		67.7	•	81.6	19.1 81.6	19.1	38.8 19.1	38.8 19.1	9.35 38.8 19.1	3.63 9.35 38.8 19.1	3.63 9.35 38.8 19.1
33.7 -5.10	0.04	0.80	1,08	-0.51	CL	30.00	32,50	37.50		64.4		77.1	19.1 77.1		42.6 19.1	9.25 42.6 19.1	3.71 9.25 42.6 19.1	3.71 9.25 42.6 19.1	1-3 3.71 9.25 42.6 19.1
27.5 -2.04	0.04	0.53	0.88	-0.20	CL	31.25	33.75	35.00		2		7.87	19.9 79.7		42.3 19.9	42.3 19.9	8.55 42.3 19.9	4.94 8.55 42.3 19.9	0-1 4.94 8.55 42.3 19.9
25.2 -3.06	0.08	0.47	0.81	-0.31	CL	30.00	31.25	38.75		40.1		60.8	18.9 60.	18.9	39.5 18.9	7.10 39.5 18.9	4.83 7.10 39.5 18.9	4.83 7.10 39.5 18.9	1-3 4.83 7.10 39.5 18.9
24.4 -3.06	0.12	0.40	0.78	-0.31	CL	37,50	25.00	37.50		39,9		59.9			18.7	40.1 18.7	7.10 40.1 18.7	4.83 7.10 40.1 18.7	1-3 4.83 7.10 40.1 18.7
21.0 -2.04	0.02	0.43	0.67	-0.20	o	45.00	22.50	32.50		97.9		27.	20.5 27.	20.5	20.5	9.56 37.3 20.5	5.58 9.56 37.3 20.5	5.58 9.56 37.3 20.5	0-1 5.58 9.56 37.3 20.5
24.7 2.04	0.04	0.46	0.79	0.20	υ	45.00	25.00	30.00		116		16.0		18.6	49.7 18.6	10.8 49.7 18.6	5.78 10.8 49.7 18.6	1-3 5.78 10.8 49.7 18.6	11/9/12 1-3 5.78 10.8 49.7 18.6
18.9 0.00	0.11	0.28	0.61	00'0	SICLICL	36.25	43.75	20.00				19.6		19.5	43.3 19.5	4.20 43.3 19.5	5.94 4.20 43.3 19.5	5.94 4.20 43.3 19.5	11/9/12 0-1 5.94 4.20 43.3 19.5
20.6 1.02	0.05	0.37	0.66	0.10	CL	36.25	41.25	22.50				15.6		1.71	42.0 17.1	8.80 42.0 17.1	8.80 42.0 17.1	1-3 6.04 8.80 42.0 17.1	11/9/12 1-3 6.04 8.80 42.0 17.1
20.4 -1.02	60'0	0.35	0,65	-0.10	Ъ	31.25	32.50	36.25				33.2	20.2 33.2	20.2	39.9 20.2	7.10 39.9 20.2	5.37 7.10 39.9 20.2	5.37 7.10 39.9 20.2	0-1 5.37 7.10 39.9 20.2
20.0 0.00	20.0	0.36	0.64	00.00	CL	32.50	32.50	35.00				27.5		18.6	42.7 18.6	6.90 42.7 18.6	5,65 6,90 42.7 18.6	1-3 5.65 6.90 42.7 18.6	11/9/12 1-3 5.65 6.90 42.7 18.6
27.0 -2.04	0.10	0.48	0.86	-0.20	CL	31.25	37.50	31.25				44.3	21.1 44.3	21.1	37.8 21.1	9.60 37.8 21.1	5.53 9.60 37.8 21.1	5.53 9.60 37.8 21.1	0-1 5.53 9.60 37.8 21.1
24.8 -2.04	0.10	0.44	0.79	-0.20	CL	33.75	37.50	28.75				32.4		20.4	39.9 20.4	39.9 20.4	5.63 8.90 39.9 20.4	5.63 8.90 39.9 20.4	1-3 5.63 8.90 39.9 20.4
21.4 -2.50	0.02	0.50	0,68	-0.25	с	27.50	30.00	42.50		17.2		112			22.3	33.2 22.3	4.96 6.30 33.2 22.3	4.96 6.30 33.2 22.3	0-1 4.96 6.30 33.2 22.3
28.7 -1.49	<0.01	0.68	0.92	-0.15	SCL	23.75	26.25	50.00				95.4		20.4	35.0 20.4	5.30 35.0 20.4	4.24 5.30 35.0 20.4	4.24 5.30 35.0 20.4	11/9/12 1-3 4.24 5.30 35.0 20.4
52.1 -8.55	<0.01	1.15	1.67	-0.85	Ъ	33.75	28.75	37.50		1.22		211		21.1	40.7 21.1	9.40 40.7 21.1	2.34 9.40 40.7 21.1	0-1 2.34 9.40 40.7 21.1	11/9/12 0-1 2.34 9.40 40.7 21.1
48.4 -8.55	<0.01	1.11	1.55	-0.85	CL	36.25	28.75	35.00				189	21.9 189	21.9	42.3 21.9	42.3 21.9	2.44 8.30 42.3 21.9	2.44 8.30 42.3 21.9	1-3 2.44 8.30 42.3 21.9
0.43 38.8 -2.50 -41.3	0.20	0.61	1.24	-0.25	CL/SCL	27.50	27.50	45.00		17.4		90.6		20.0	33.8 20.0	4.90 33.8 20.0	4.90 33.8 20.0	0-1 3.51 4.90 33.8 20.0	11/9/12 0-1 3.51 4.90 33.8 20.0
27.6 -2.50	60.0	0.46	0.88	-0.25	ъ	31.25	32.50	36.25		51.0	47	58.4		19.1	40.5 19.1	6,40 40,5 19,1	4.37 6.40 40.5 19.1	1-3 4.37 8,40 40.5 19.1	11/9/12 1-3 4.37 8,40 40.5 19.1
37.0 -2.50	0.21	0.60	1.19	-0.25	CL	31.25	41.25	27.50				67.9		21.1	38.5 21.1	8.35 38.5 21.1	5.32 8.35 38.5 21.1	0-1 5.32 8.35 38.5 21.1	11/9/12 0-1 5.32 8.35 38.5 21.1
26.5 2.55	0.18	0.41	0.85	0.25	CL	31.25	37.50	31.25			4,	42.0	20.7 42.0	20.7	20.7	6.45 41.3 20.7	8.17 8.45 41.3 20.7	8.17 8.45 41.3 20.7	1-3 8.17 8.45 41.3 20.7
22.7 0.53	0.02	0.52	0.73	0.05	CL	31.25	28.75	40.00				43.5	19.4 43.3		47.7 19.4	47.7 19.4	8,30 47.7 19.4	5.82 8,30 47.7 19.4	0-1 5.82 8.30 47.7 19.4
17.1 4.56	0.14	0.23	0.55	0.46	СГ	31.25	28.75	40,00			1-	27.8			18.0	7.45 40.7 18.0	6.42 7.45 40.7 18.0	1-3 6.42 7.45 40.7 18.0	1-3 6.42 7.45 40.7 18.0
30.2 -4.51	0.09	0.68	0.97	-0.45	SL	12.50	30,00	57.50		58.4	-	186	22.9 186		22.9	29.3 22.9	10.1 29.3 22.9	3.61 10.1 29.3 22.9	0-1 3.61 10.1 29.3 22.9
35.6 -6.53	0.02	0.95	1,14	-0.65	SL	7.50	28.75	63.75		66.5	U.	339	28.3 339		28.3	30.0 28.3	14.4 30.0 28.3	3.23 14.4 30.0 28.3	1-3 3.23 14.4 30.0 28.3
27.0 -0.48	0.19	0.41	0.87	-0.05	CL	30.00	38.75	31.25	13.6	71.2		33,9	21.3 33.9		21.3	44.8 21.3	5.19 7.30 44.8 21.3	5.19 7.30 44.8 21.3	0-1 5.19 7.30 44.8 21.3
28.1 -0.48	0.17	0.45	0.90	-0.05	CF	27.50	38.75	33.75	15.3	83.9		37.8	22.5 37.6	41.4 22.5 37.5	8.05 41.4 22.5 37.5	8.05	5.40 8.05	11/8/12 1-3 5.40 8.05 41.4 22.5 37.5	1-3 5.40 8.05

PYRS A-B TW/1000TN	-23.9	-19,6	0.53	-4.34	7.59	-6.83	7.15	
PYR A POT TN/1000TN	0.25	<0.01	<0.01	1.84	<0.01	1.31	0.44	
A-B POT TN/1000TN	-35.5	-40.9	-13.1	-35.8	-16.1	-45.2	1.02	
NEUT POT TW/000TN	-23.7	-19.6	0.53	-2.50	7.59	-5.52	7.59	
ACID POT TN/1000TN	11.8	21.2	13.6	33.3	23.7	39.7	6.57	
ORG 5%	0.23	0.34	0.16	0.27	0.23	0.30	0,10	
PYR S %	0.01	<0.01	<0.01	0.06	<0,01	0.04	0.01	
SULFATE S%	0.14	0.36	0.28	0.74	0.55	0.93	0.10	
TOT S % SI	0.38	0.68	0.44	1.07	0.76	1.27	0.21	
% cAGOS	-2.37	-1.96	0.05	-0.25	0.76	-0.55	0.76	
CLASS	SL/SCL	SL	сL	CL	CL	-		ъ
% CLAY	20.00	18.75	32.50	32.50	30.00	26.25		37.50
% siLT	25.00	23.75	35.00	32.50	33.75	33.75		30.00
% SAND	55,00	57.50	32.50	35.00	36.25	40.00		32.50
SAR	2.56	2.76	2.88	10.15	2.62	1.23		19.9
SODIUM	12.0	12.8	15.7	62.9	14.8	9.53		37.4
MAGNESIUM MEQL	18.3	18.4	31.5	55.6	40.1	97.1		2.44
CALCIUM	25.3	24.8	27.8	21.3	23.9	22.8		4,63
% SAT	53.0	57.7	40.7	40.9	40.0	38,4		50.1
EC MMHO/CM	4.20	4.30	3.80	7.35	3,80	4,60		3.50
PH UNITS	3.73	3,56	6.11	5.28	5.28	4.71		8.18
SAMPLE DEPTH	0-1	1-3	0-1	1-3	6-1	1-3		
SAMPLE DATE	12/12/12	12/12/12	12/12/12	12/12/12	12/12/12	12/12/12		
LOCATION	3123-N9	3123 N9			3331-N9	3331-N9		
BAL N	1212-078-01	1212-078-02	1212-078-03	1212-078-04		1212-078-06	QC-29	QC-45

T PYRAPOT PYRSA-B		-23.0 2.19 -0.57				0.69	-4.85 -0.03 2.62	0.00	0.53		
A-B POT TW/1000TN	5 -48.						-				
NEUT POT TN/1000TN	-6.15	1.62		7.44	4.53	3.56	2.56			0.65	
ACID POT TN/1000TN	42.0	24.6	11.2	13.8	20.8	22.8	7.44	4.29	26.7	25.8	
ORG S%	0.32	0.20	0.12	0.16	0.22	0.20	0.10	0.00	0.22	0.17	
PYR S %	0.14	0.07	0.14	0.09	0.01	0.02	00.0	0.00	0.02	0.05	
SULFATE S%	0.89	0.52	0.10	0.19	0.44	0.51	0.14	0.14	0.62	0.60	1
TOT S % SU	1.34	0.79	0.36	0.44	0.66	0.73	0.24	0.14	0.86	0.83	1000
% CACO3 T	-0.61	0.16	0.65	0.74	0.45	0.36	0.26	0.65	-0.13	0.06	10.0
CLASS	-	5	С	СГ	L.	CL	CL	С	CL	Ч	
% CLAY	22.50	.23.75	30.00	27.50	26.25	27.50	32.50	32.50	30.00	30.00	
% SILT	36.25	33.75	35.00	36.25	36.25	32.50	35.00	35.00	37.50	35.00	
% SAND	41.25	42.50	35.00	36.25	37.50	40.00	32.50	32,50	32.50	35.00	
SAR	2.97	4.60	6.89	5.85	1.93	1.91	2.57	1.80	2.76	6.89	
SODIUM	30.4	30.3	27.4	27.1	9.74	9.74	10.7	7.74	19.4	35.3	
MAGNESIUM MEQIL	189	67.3	9.54	17.0	29.3	31.9	13.0	13.1	80.0	32.9	
CALGIUM	21.1	19.7	22.1	26,0	21.5	19.9	21.7	23.8	18.2	19.6	
% SAT	35.3	39.1	37.1	35.7	41.4	39.6	46.1	45.8	44.8	41.6	100000
EC MMHO/CM	15	7.68	4.61	5.2	4.19	4.14	3.46	3.17	7.01	6.33	
PH UNITS	3.56	5.89	7.15	7.18	6.28	6.04	6.02	7,20	4.69	5.23	
SAMPLE		1-3		1.3	0-1	1-3	0-1	1-3	5	1.3	
SAMPLE DATE	4/11/13	4/11/13	4/11/13	4/11/13	4/11/13	4/11/13	4/11/13	4/11/13	4/11/13	4/11/13	
LOCATION S	J19 1964	J19 1964	J19 1982	J19 1982	N9 3330	N9 3330	N9 3120	N9 3120	N9 3126	N9 3126	
GAL #	1304-084-11 J	1304-084-12 J	304-84-33 J	1304-84-34 J	1304-84-41	304-84-42	304-84-43	1304-84-44 1	1304-84-45 1	1304-84-46	and the second se

0-1 6.25 8.76 46.7 20.3 31.7 63.5 12.5 31.25 36.25 1-3 6.44 8.75 43.7 20.5 296 65.3 13.0 31.25 36.25 1-3 6.44 8.75 43.7 20.5 296 65.3 13.0 31.26 36.25 1-3 4.41 8.56 33.5 18.2 10.37 2.79 0.21 30.0 47.50 1-3 4.41 8.56 39.9 18.2 153.0 1.85 0.20 31.25 46.25 0-1 5.57 11.6 43.5 20.2 46.5 88.1 15.2 38.75 32.50 1-3 5.82 9.53 30.9 18.2 77.4 15.4 33.75 36.25 33.75 1-3 5.82 9.53 30.9 18.7 77.4 15.4 33.75 33.75 1-3 5.82 9.53 30.9 18.7 77.4	сг 0.367 ср. 0.166 ср. 0.166 0.166 0.166 0.166 0.166 0.166 0.467 0.467 0.467 0.467 0.668 0.467 0.668 0.467 0.668 0.467 0.668 0.467 0.668 0.467 0.4770000000000	567 0.706 166 0.333 170 1.144 171 1.148 1710 1.148 1710 1.169 166 0.915 166 0.915 166 0.915 166 0.915 166 0.915 166 0.055 166 0.055 167 0.558 170 0.709 568 0.709 568 0.509 568 0.509 569 0.709 569 0.709	6 0.431 3 0.445 9 0.809 9 0.882 5 0.588 5 0.518 5 0.518 5 0.538 5 0.336 8 0.345 9 0.721 9 0.721 9 0.345	0.086 0.180 0.060 0.022 0.149 0.149	0.190	22.1			
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0-1 381 656 535 209 103.7 2.79 0.35 26.25 45.00 1-3 4.48 8.43 37.5 18.3 162.1 1.66 0.31.5 45.00 1-3 4.48 8.43 37.5 18.3 162.1 1.66 0.21 30.00 47.50 1-3 5.67 11.6 43.5 20.2 46.5 88.1 15.2 38.75 36.26 1-3 5.62 97.9 46.4 19.0 31.7 77.4 15.4 33.75 36.26 0-1 5.68 7.58 49.2 18.7 77.4 15.4 33.75 36.26 1-3 5.68 7.60 31.7 77.4 15.4 36.25 33.75 1-3 5.68 7.40 48.8 19.4 15.3 56.25 33.75 1-3 5.58 74.0 48.8 19.4 15.3 56.25 32.50 1-3 7.35				0.060 0.022 0.033 0.149 0.100	002.0				
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$				0.022 0.033 0.149 0.100	0.275				
1-3 4.41 8.56 39.9 18.2 153.0 1.83 0.20 31.25 46.25 0-1 5.57 11.6 43.5 20.2 46.5 88.1 15.2 38.75 35.50 1-3 5.82 97.8 42.5 20.2 46.5 88.1 15.2 38.75 35.50 1-3 5.82 9.53 39.0 18.7 48.4 58.7 10.1 37.50 33.75 1-3 5.28 9.53 39.0 18.7 48.4 58.7 10.1 37.50 33.75 0-1 6.81 7.03 55.6 18.8 18.6 56.5 11.7 28.75 36.25 0-1 6.81 7.03 55.6 18.8 18.2 50.5 11.7 28.75 36.25 1-3 7.34 7.40 48.8 19.4 15.3 56.25 32.50 1-3 7.35 7.40 48.8 19.4 15.3 56.25 32.50 1-3 7.35 7.40 48.8 19.4 53.2				0.033 0.149 0.100	0.259		-2.35 -	-36.5 0.69	-3.04
0-1 5.57 11.6 43.5 20.2 46.5 88.1 15.2 38.75 32.50 1-3 5.82 9.79 46.4 19.0 31.7 77.4 15.4 33.75 36.25 1-3 5.82 9.79 46.4 19.0 31.7 77.4 15.4 33.75 36.25 1-3 5.88 7.58 9.53 39.0 18.7 74.4 15.4 33.75 33.75 1-3 5.58 9.53 39.0 18.7 48.4 58.7 10.1 37.50 33.75 1-3 7.38 53.6 18.8 18.2 50.5 11.7 28.75 36.25 1-3 7.38 7.40 48.8 19.4 15.3 59.2 14.2 36.25 32.50 1-3 7.34 3.08 54.2 19.3 15.1 28.7 36.25 32.50 1-3 7.43 3.05 54.2 16.3 16.7 36.25				0.149	0.274				
211/14 1-3 5.82 979 46.4 19.0 31.7 77.4 15.4 33.75 36.25 211/14 1-3 5.88 7.58 4.22 16.2 30.9 456 8.4 19.1 35.5 33.75 33.26 32.50 32.76 32.75 36.25 32.50 22.350 22.13/14 1-3 7.24 30.26				0.100	0.247				
2/11/14 0-1 5.88 7.58 4.22 18.2 30.9 45.6 8.41 36.25 33.75 2/11/14 1-3 5.28 9.53 39.0 18.7 48.4 58.7 10.1 37.50 33.75 2/12/14 1-3 5.26 9.53 39.0 18.7 48.4 58.7 10.1 37.50 33.75 2/12/14 1-3 7.35 5.40 48.8 19.4 15.3 50.2 31.75 2/12/14 1-3 7.35 7.40 74.8 19.3 15.1 58.7 14.2 36.25 32.50 2/13/14 1-3 7.40 74.8 47.0 19.3 15.1 58.7 14.2 36.25 32.50 2/13/14 1-3 7.24 3.26 52.4 24.5 27.4 56.5 11.25 36.25 32.50 2/13/14 1-3 7.24 3.20 50.4 24.5 27.4 56.5 11.36 26.25					0.199				
2/11/14 1-3 5.26 9.53 39.0 18.7 48.4 58.7 10.1 37.50 33.75 2/12/14 0-1 0.81 7.03 53.6 18.8 18.2 50.5 11.7 28.75 36.25 33.75 2/12/14 1-3 7.35 7.40 48.8 19.4 15.3 59.2 14.2 36.25 32.50 2/12/14 1-3 7.36 7.40 48.8 19.4 15.1 58.7 14.2 36.25 32.50 2/13/14 1-3 7.30 5.06 52.4 24.6 22.4 66.1 1.36 26.25 41.25 2/13/14 1-3 7.24 3.20 50.4 24.5 27.4 5.22 1.02 27.50 42.25 2/13/14 1-3 7.24 3.20 50.4 24.5 27.4 5.22 1.02 27.50 42.25 2/13/14 1-3 7.24 3.20 50.4 24.5 27.4				0.044	0.323				
2/12/14 0-1 6.81 7.03 53.6 18.8 18.2 50.5 11.7 28.75 38.25 2/12/14 1-3 7.35 7.40 48.8 19.4 15.3 59.2 14.2 36.25 32.50 2/12/14 1-3 7.35 7.40 48.8 19.4 15.3 59.2 14.2 36.25 32.50 2/12/14 1-3 7.40 7.49 47.0 19.3 15.1 58.7 14.2 36.25 32.50 2/13/14 0-1 7.31 7.49 24.5 27.4 56.1 14.2 36.75 42.55 2/13/14 1-3 7.24 3.20 50.4 24.5 27.4 56.2 14.12 2/13/14 1-3 7.24 3.20 50.4 24.5 27.4 56.2 14.12 2/13/14 0-1 6.78 38.4 21.7 50.6 14.1 2.34 35.26 2/13/14 0-1 6.78				0,079	0.319				
2/12/14 1-3 7.35 7.40 488 19.4 15.3 59.2 14.2 36.25 32.50 2/12/14 1-3 7.40 7.40 47.0 19.3 15.1 58.7 14.2 36.25 32.50 2/12/14 1-3 7.40 7.40 47.0 19.3 15.1 58.7 14.2 36.25 32.50 2/13/14 0-1 7.31 3.08 52.4 2.46 2.24 5.52 10.2 27.50 42.50 2/13/14 0-1 6.78 3.66 50.4 2.45 2.74 5.22 10.2 27.50 42.50 2/13/14 0-1 6.78 4.62 38.4 2.17 50.6 14.1 2.34 38.76 39.26 2/13/14 0-1 6.78 4.62 38.4 2.17 50.6 14.1 2.34 38.76 39.26				0.077	0.176				
2/12/14 1-3 7.40 7.49 47.0 19.3 15.1 58.7 14.2 36.25 32.50 2/13/14 0-1 7.31 3.06 52.4 24.6 22.4 6.61 1.36 26.25 41.25 2/13/14 1-3 7.24 3.20 50.4 24.5 27.4 5.22 1.02 27.50 42.50 2/13/14 1-3 7.24 3.20 50.4 24.5 27.4 5.22 1.02 27.50 42.50 2/13/14 0-1 6.78 4.62 38.4 21.7 50.5 1.41 2.34 38.75 38.25				0.113	0.202				
2/13/14 0-1 7.31 3.08 52.4 24.6 22.4 6.61 1.36 26.26 41.25 2/13/14 1-3 7.24 3.20 50.4 24.5 27.4 5.22 1.02 27.50 42.50 2/13/14 0-1 6.78 4.62 38.4 21.7 50.6 14.1 2.34 38.75 36.26 20.00000000000000000000000000000000				0.129	0.192				
2/13/14 1-3 7.24 3.20 50.4 24.5 27.4 5.22 1.02 27.50 42.50 2/13/14 0-1 6.78 4.62 38.4 21.7 50.6 14.1 2.34 38.75 36.26				0.013	0.209				
2/13/14 D-1 B.76 4.62 38.4 21.7 50.6 14.1 2.34 38.75 36.26				<0.010	0.263			1	
				0.072	0.306				
2/13/14 1-3 0.02 0.46 32.6 24.5 3/.8 42.1 7.54 45.00 38.75				0.235	0.201				
2/13/14 0-1 7.85 6.23 60.5 6.49 4.21 57.4 24.8 21.25 37.50				0.010	0.114				
2/13/14 1-3 7.52 6.86 57.9 8.58 5.27 63.1 24,0 22.50 32.50				0.006	0.119				
1-3 7.42 6.84 58.7 8.53 5.23 82.6 23.9 22.50 32.50				0.019	0.112				
2/12/14 0-1 7.45 6.93 57.8 20.7 14.1 62.6 15.0 26.25 33.75				0.204	0.135				
2/12/14 1-3 8.36 2.8 62.7 1.44 0.81 30.4 28.7 21.25 31.25									
2/11/14 0-1 6.08 6.63 46.3 18.2 27.6 49.2 10.2 36.25 33.75			3 0.412	0.032	0.229				
1-3 6.32 7.21 46,4 19,4 29,0 54,4 11,1 31.25 37,50				0.073	0.230				
r 2/12/14 0-1 5.95 5.89 44.4 18.3 32.7 45.2 8.96 36.25 37.50			l	0.139	0.180				
2/12/14 1-3 6.01 5.85 43.6 19.8 34.3 43.9 8.45 40.00 32.50				0.154	0.205				
2/12/14 1-3 6.08 5.67 45.2 20.3 33.8 43.9 8.46 40.00 32.50			7	0.169	0.186				
2/13/14 0-1 4.40 8.19 37,6 20,6 273,1 2.33 0.19 32,50 47,50	Ì		Ĩ	0.067	0.538				
0 2/13/14 1-3 3.31 17.7 35.3 22.4 893.5 0.43 0.02 46.25 38.75			2	<0.010	1.014			1	
2/12/14 0-1 8.06 6.00 47.9 20.3 14.3 53.1 12.8 43.75 28.75 3									
2/12/14 1-3 7.95 6.23 49.3 19.3 16.6 55.2 13.0 41.25			2 0.124	0.032	0.117			0.18 1.00	7.68
15.7 50.9 12.3 41.25 30.00				0.014	0.114			Ĩ	8.24

PYRS A-B TN/1000TN	-5.82	2.63	4.74	7.15	-2.29	-1.32	-2.77	-2.90	19.69					4.67	-12.81	-9.84	0.74	14,69	12.76	8.97
PYR A POT TN/1000TN	1.47	0.03	2.94	1.53	-2.06	-1.03	4,44	3.56	3.03					0.31	1.44	-0.53	3.93	5.02	5.94	0.72
A-B POT P TIVI 000TN T	-21.7	-10.4	-16.0	-7.82	43.0	43.6	-15.0	-18.9	-10,8	8.46	8.04	14.4	3.15	-44.7	-78.7	43.4	-25.3	-13.6	-13.0	3.59
NEUT POT TN/1000TN TI	-4.35	2.67	7.68	8.68	4.35	-2.35	1.66	0.66	22.72	33.75	33.75	35.76	22.72	-4.35	-11.37	-10.37	4.67	19.71	18.71	9.68
ACID POT NI TW/1000TN Th	17.4	13.0	23.6	16.5	38.6	41.2	16.7	19.5	33.5	25.3	25.7	21.3	19.6	40.3	67.3	33.1	29.9	33.3	31.7	6.09
oRo.s% A	0.166	0.136	0.212	0.128	0.502	0.509	0.324	0.368	0.340					0.541	0.918	0.342	0.320	0.338	0.263	0.098
PYR S %	0.047	0.001	0.094	0.049	<0.010	<0.010	0.142	0.114	0.097					0.010	0.046	<0.010	0.126	0.161	0.190	0.023
SULFATE 5% P	0.344	0.280	0.451	0.351	0.800	0.843	0.068	0.143	0.636					0.739	1.191	0.733	0.513	0.568	0.562	0.075
TOT 5 % SU	0.556	0.417	0.757	0.528	1.236	1.319	0.534	0.625	1.072	0.809	0.823	0.682	0.626	1.290	2.155	1.058	0.958	1.067	1.016	0.195
% CACOS	<0.010	0.267	0.768	0.868	<0.010	<0.010	0.166	0.066	2.272	3.375	3.375	3.576	2.272	<0.010	<0.010	<0.010	0.467	1.971	1.871	0.968
CLASS	CL	SCL	or	SCL	ы	5	ы	CL/SCL	сг	oL	ы	сг	CL	ы	Ъ	С	Ъ	Ъ	С	
% CLAY			28.75				35.00						28.75		28.75					
% SILT	35,00	26.25	31.25	27.50	38.75	32.50	27.50	23.75	33.75	28.75	28,75	31.25	28.75	33.75	28.75	35.00	30.00	35.00	28.75	
GNAS X	37.50	50.00	40.00	48.75	30.00	36.25	37.50	45.00	32,50	42.50	42,50	40.00	42.50	37.50	42.50	30.00	41.25	32.50	40.00	
SAR	9.40	8.78	7.06	8,29	5,58	12.1	9.17	23.7	9,68	13.4	13.6	12.2	9.29	1.66	0.03	14.9	18.0	4.46	19.6	
SODIUM	51.3	50.9	45.2	53.1	52.6	118	23.5	87.4	53.1	64.4	66.6	62.6	48.3	14.2	0.39	108	107	21.4	109	
MAGNESIUM	39.2	46.2	62.4	61.9	160	173	5.55	10.3	39.4	27.9	28.6	32.9	34.9	128.3	290.4	88.0	53.7	24.0	43,3	
CALCIUM	20.4	21.1	19.7	19.9	18.6	17.8	7.63	16.9	20.8	18.1	19.1	19.9	19.2	17.9	22.3	17.5	17.71	22.0	18,6	
% SAT	39.1	37.3	42.4	42.0	45.1	46.3	54.9	57.5	42.2	41.7	42.4	40,4	41.2	42.3	43.2	52.3	45.9	45.4	41.1	
EC MMHO/CM	5.83	6.04	6.12	6.79	7.83	11.8	2.65	7.25	6.03	6.85	6.74	6.86	5.67	6.16	12.0	11.1	10.9	3.82	10.3	
PH UNITS	7:04	6.86	6.63	7.43	3.95	3,99	5.12	5,29	6.99	7.66	7.65	7,61	7.10	3.55	2.62	4.98	6,49	7.14	7.35	
SAMPLE	0-1	1.3	0-1	1-3	0-1	1-3	0-1	1-3	0-1	1-3	1-3	0-1	1-3	<u>-</u>	1-3	0-1	1-3	0-1	1-3	
SAMPLE DATE	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	2/14/14	
LOCATION	3015	3015	2881	2881	2910	2910	2992	2992	2937	2937	2937	2911	2911	2965	2965	2991	2991	2990	2990	
GAL#	1402-159-01	1402-159-02	1402-159-03	1402-159-04	1402-159-05	1402-159-06	1402-159-07	1402-159-08	1402-159-09	1402-159-10	1402-159-10R	1402-159-11	1402-159-12	1402-159-13	1402-159-14	1402-159-15	1402-159-16	1402-159-17	1402-159-18	

0000000 200 2000 0000 <	2130 2/10/14 0-1 6.67 7.88 45.6 19.8 2130 2/10/14 1-3 6.88 8.04 49.2 19.0 2130 2/10/14 1-3 6.02 8.04 49.2 19.0 2082 2/11/14 1-3 4.02 11.8 36.8 24.9 2110 2/11/14 1-3 6.05 5.13 48.0 7.0 2111 2/11/14 1-3 6.05 5.13 48.9 20.9 2111 2/11/14 1-3 6.05 5.13 48.0 74.9 2111 2/11/14 1-3 6.04 5.74 47.5 70.9 2111 2/11/14 1-3 6.93 6.94 7.16 70.9 2101 2/11/14 1-3 6.93 6.57 5.16 70.9 2101 2/11/14 1-3 5.93 6.94 7.16 77.7 2017 2/11/14 1-3 5.93 6.16	SAR	% SAND	% SILT	% CLAY CI	CLASS %	% CACO3 TOI	TOTS% SULF	SULFATE 5% PY	PYR S % OF	ORG 5% AC TN	ACID POT NEU TIN1000TN TN/10	NEUT POT A-E TN/1000TN TN/1	A-B POT PYR TN/1000TN TN/1	PYR A POT PYRS A-B TN/1000TN TN/1000TN
2000 2010 0.00 <th< td=""><td>2130 2/10/14 1.3 6.08 8.04 49.2 19.0 2082 2/11/14 1.3 4.02 11.1 3.82 45.7 22.9 2110 2/11/14 1.3 4.02 11.1 3.82 4.67 22.9 2111 2/11/14 1.3 4.02 11.1 3.82 4.67 22.9 2111 2/11/14 1.3 6.08 5.13 4.67 7.8 2111 2/11/14 1.3 6.08 5.13 4.67 7.90 2111 2/11/14 1.3 6.27 5.34 4.03 7.93 2001 2/13/14 0.1 6.98 6.64 4.76 16.9 2017 2/11/14 1.3 6.54 4.40 41.8 20.9 2017 2/13/14 0.1 5.93 5.66 7.92 2.93 2017 2/13/14 0.1 5.93 5.64 7.62 2.84 2.92 2017</td><td>15.9</td><td>32.50</td><td>36.25</td><td></td><td>CL CL</td><td></td><td></td><td>0.438</td><td>0.144</td><td>0.249</td><td>25.9</td><td>3.67</td><td>-22.3</td><td>4.50</td></th<>	2130 2/10/14 1.3 6.08 8.04 49.2 19.0 2082 2/11/14 1.3 4.02 11.1 3.82 45.7 22.9 2110 2/11/14 1.3 4.02 11.1 3.82 4.67 22.9 2111 2/11/14 1.3 4.02 11.1 3.82 4.67 22.9 2111 2/11/14 1.3 6.08 5.13 4.67 7.8 2111 2/11/14 1.3 6.08 5.13 4.67 7.90 2111 2/11/14 1.3 6.27 5.34 4.03 7.93 2001 2/13/14 0.1 6.98 6.64 4.76 16.9 2017 2/11/14 1.3 6.54 4.40 41.8 20.9 2017 2/13/14 0.1 5.93 5.66 7.92 2.93 2017 2/13/14 0.1 5.93 5.64 7.62 2.84 2.92 2017	15.9	32.50	36.25		CL CL			0.438	0.144	0.249	25.9	3.67	-22.3	4.50
7000 71114 1 410 410 710 111 710 111 710 <td>2082 2/11/14 0-1 4.06 3.82 45.7 22.9 2082 2/11/14 1-3 4.02 11.7 3.82 45.7 22.9 2110 2/11/14 1-3 4.02 11.7 3.80 8.7 24.9 2111 2/11/14 1-3 6.08 9.06 48.9 20.8 2111 2/11/14 1-3 6.08 9.06 48.9 20.9 2111 2/11/14 1-3 6.08 8.06 47.6 16.6 2111 2/11/14 1-3 6.54 4.40 41.8 19.3 2101 2/11/14 1-3 6.53 5.64 4.75 16.6 2017 2/11/14 1-3 6.54 4.40 41.8 20.9 2017 2/11/14 1-3 6.54 4.40 41.8 20.9 2017 2/11/14 1-3 5.8 6.57 51.6 19.2 2017 2/11/14 1-3</td> <td>16.2</td> <td>32.50</td> <td>37.50</td> <td></td> <td>d d</td> <td>0.467</td> <td></td> <td>0,423</td> <td>0.108</td> <td>0,239</td> <td>24.1</td> <td>4.67</td> <td>-19.4</td> <td>3.37</td>	2082 2/11/14 0-1 4.06 3.82 45.7 22.9 2082 2/11/14 1-3 4.02 11.7 3.82 45.7 22.9 2110 2/11/14 1-3 4.02 11.7 3.80 8.7 24.9 2111 2/11/14 1-3 6.08 9.06 48.9 20.8 2111 2/11/14 1-3 6.08 9.06 48.9 20.9 2111 2/11/14 1-3 6.08 8.06 47.6 16.6 2111 2/11/14 1-3 6.54 4.40 41.8 19.3 2101 2/11/14 1-3 6.53 5.64 4.75 16.6 2017 2/11/14 1-3 6.54 4.40 41.8 20.9 2017 2/11/14 1-3 6.54 4.40 41.8 20.9 2017 2/11/14 1-3 5.8 6.57 51.6 19.2 2017 2/11/14 1-3	16.2	32.50	37.50		d d	0.467		0,423	0.108	0,239	24.1	4.67	-19.4	3.37
2002 211/14 13 4.22 11/1 9.00 4.20 11/1 9.00 2.00 4.00 1.00 0.461 0.01 0.010 0.461 0.010 0.461 0.010 0.461 0.010 0.461 0.010 0.461 0.010	2082 2/11/14 1-3 4.02 11.7 40.0 27.8 2102 2/11/14 1-3 6.08 9.06 4.89 24.9 2111 2/11/14 1-3 6.08 9.06 4.89 20.9 2111 2/11/14 1-3 6.08 9.06 4.89 20.9 2111 2/11/14 1-3 6.08 9.06 4.89 20.9 2111 2/11/14 1-3 6.08 9.06 4.90 16.6 2111 2/11/14 1-3 6.29 6.88 5/15 4.90 16.6 2007 2/13/14 1-3 6.29 6.88 5/16 192 2017 2/11/14 1-3 5.34 4.00 17.1 20.3 2017 2/11/14 1-3 5.38 7.16 39.4 27.7 2017 2/11/14 1-3 5.86 5.19 39.4 27.7 2017 2/11/14 1-3 5.86	2.68	35,00	38.75			<0.010		0.546	0.038	0.470	32.9	-4.35	-37.2	1.19
7000 71111 713 7101 713 7101 713 71011 7101 7101	2082 2/11/14 1.3 4.02 11.8 36.8 24.9 2110 2/11/14 0.1 6.65 5.13 4.8.9 20.9 19.6 2111 2/11/14 0.1 6.65 5.13 4.8.9 5.0.9 19.6 2111 2/11/14 0.1 6.65 5.13 4.8.9 20.9 19.6 2111 2/11/14 1.3 6.54 5.34 4.9.0 16.5 16.9 2017 2/13/14 0.1 6.65 5.13 4.8.9 10.2 16.5 2017 2/11/14 1.3 6.29 6.88 5.16 19.2 22.3 2017 2/11/14 1.3 6.54 7.40 39.1 27.7 2056 2/11/14 1.3 7.38 7.40 39.1 27.7 2056 2/11/14 1.3 7.38 7.40 39.1 27.7 2056 2/11/14 1.3 7.40 39.1 7.40 2	4.52	30.00	45.00	25.00	7	<0.010		0.804	0.001	0.464	39.6	-4.35	-44.0	0.03
2110 21114 1:1 0.116 0.136 0.036 0.	2110 2711/14 0-1 6.18 8.39 50.9 19.6 2111 2711/14 1-3 6.08 513 5.4 48.5 19.6 2111 2711/14 1-3 6.08 513 5.4 48.5 19.6 2111 2711/14 1-3 6.27 5.34 48.5 19.6 2111 2717/14 1-3 6.27 5.34 48.5 19.6 2007 2717/14 1-3 6.26 5.44 47.6 16.9 2017 2717/14 1-3 6.54 4.40 41.8 20.9 2017 2717/14 1-3 6.54 4.40 41.8 28.0 2056 2717/14 1-3 5.3 36.6 41.2 28.0 2056 2717/14 1-3 5.36 5.79 39.1 27.7 2056 2717/14 1-3 5.86 5.79 39.7 27.9 2056 27171/14 1-3	4,29	28.75	46.25	25.00	-	<0.010		0.841	0.035	0.483	40.2	-4.35	-44.6	-1.09
7110 7114 1.1 0.00 0.01 0.034 0.036	2110 2711/14 1-3 6.08 9.06 48.9 20.8 2111 2711/14 1-3 6.57 5.13 48.5 19.6 2111 2711/14 1-3 6.57 5.13 48.5 19.6 2111 2711/14 1-3 6.53 5.13 48.5 19.6 2000 2713/14 1-3 6.53 5.64 47.0 16.5 2017 2717/14 1-3 6.53 5.67 5.1.6 19.2 2017 2717/14 1-3 6.54 4.40 41.8 22.3 2056 2717/14 1-3 5.67 5.79 39.1 27.7 2056 2717/14 1-3 5.86 5.00 38.0 19.4 2058 2717/14 1-3 5.86 5.00 38.1 17.4 2058 2717/14 1-3 5.86 5.00 38.1 17.4 2168 27/14 1-3 5.86 5.00	14.6	33.75	37.50		CL	0.166		0.455	0.105	0.239		1.66	-23.3	3.28
2111 21144 2114 21144 2114 21144 2114 21144 2114 21144 2114 21144 2114 21144 2114 21144 2114 21144 2114 21144 2114 21144 2114	2111 21111 211114 0-1 0.65 5,13 46.5 19.6 2111 2111/14 1-3 6.27 5.13 46.5 19.6 2111 2111/14 1-3 6.27 5.13 46.5 16.6 2000 2/13/14 1-3 6.29 6.88 5.18 19.2 2007 2/13/14 1-3 6.29 6.88 5.18 19.2 2017 2/11/14 1-3 6.29 6.88 5.18 19.2 2017 2/11/14 1-3 6.29 6.88 5.18 19.2 2055 2/11/14 1-3 5.38 7.40 39.1 27.7 2056 2/11/14 1-3 3.86 6.00 39.1 27.7 2056 2/11/14 1-3 3.86 6.00 39.1 27.7 2056 2/11/14 1-3 3.86 6.00 39.1 27.7 2058 2/11/14 1-3 3.86 <td>15.5</td> <td>33.75</td> <td>36.25</td> <td></td> <td>CL</td> <td>Ģ</td> <td></td> <td>0.428</td> <td>0.089</td> <td>0.251</td> <td></td> <td>2.67</td> <td>-21.3</td> <td>2,78</td>	15.5	33.75	36.25		CL	Ģ		0.428	0.089	0.251		2.67	-21.3	2,78
2111 21114 2114 <t< td=""><td>2111 2111/14 1-3 6.27 5.34 49.0 16.5 2000 2/13/14 1-3 6.31 5.4 47.5 16.9 2001 2/13/14 1-3 6.39 6.54 47.5 16.9 2001 2/13/14 1-3 6.59 6.88 5.16 19.2 2017 2/13/14 1-3 6.54 4.40 41.8 22.3 2017 2/11/14 1-3 6.56 4.40 41.8 22.3 2017 2/11/14 1-3 6.57 3.96 47.2 22.3 2056 2/11/14 1-3 3.87 7.95 39.6 19.5 2056 2/11/14 1-3 3.87 7.95 39.6 19.4 2056 2/12/14 1-3 3.87 7.95 39.6 19.4 2051 2/12/14 1-3 5.88 7.40 39.4 7.7 2052 2/12/14 1-3 5.88 5.7</td><td>10.4</td><td>40.00</td><td>32.50</td><td></td><td>CL.</td><td>Ĩ</td><td></td><td>0.355</td><td>0.139</td><td>0.245</td><td></td><td>3.67</td><td>-19.4</td><td>4.33</td></t<>	2111 2111/14 1-3 6.27 5.34 49.0 16.5 2000 2/13/14 1-3 6.31 5.4 47.5 16.9 2001 2/13/14 1-3 6.39 6.54 47.5 16.9 2001 2/13/14 1-3 6.59 6.88 5.16 19.2 2017 2/13/14 1-3 6.54 4.40 41.8 22.3 2017 2/11/14 1-3 6.56 4.40 41.8 22.3 2017 2/11/14 1-3 6.57 3.96 47.2 22.3 2056 2/11/14 1-3 3.87 7.95 39.6 19.5 2056 2/11/14 1-3 3.87 7.95 39.6 19.4 2056 2/12/14 1-3 3.87 7.95 39.6 19.4 2051 2/12/14 1-3 5.88 7.40 39.4 7.7 2052 2/12/14 1-3 5.88 5.7	10.4	40.00	32.50		CL.	Ĩ		0.355	0.139	0.245		3.67	-19.4	4.33
2111 2114 111 61 </td <td>2111 211/14 1-3 0.31 5.4 47.5 16.9 2000 2/13/14 0-1 6.98 6.57 51.5 51.5 19.2 2007 2/13/14 0-1 6.98 6.57 51.5 51.5 19.2 1961 2/13/14 0-1 6.53 36.0 47.5 16.3 2017 2/11/14 0-1 6.53 36.0 47.2 22.3 2056 2/11/14 0-1 5.79 39.1 27.7 28.0 2056 2/11/14 1-3 3.87 7.40 34.2 49.2 2056 2/11/14 1-3 3.87 7.95 39.6 19.4 2056 2/11/14 1-3 3.87 7.95 39.6 19.4 2058 2/11/14 1-3 5.86 5.00 39.7 21.0 2168 2/12/14 1-3 5.84 5.67 32.6 23.7 2168 2/12/14 1-3</td> <td>11.2</td> <td>35.00</td> <td>35,00</td> <td></td> <td>GL</td> <td>Ĩ</td> <td></td> <td>0,333</td> <td>0.178</td> <td>0.218</td> <td></td> <td>3.67</td> <td>-19.1</td> <td>5.56</td>	2111 211/14 1-3 0.31 5.4 47.5 16.9 2000 2/13/14 0-1 6.98 6.57 51.5 51.5 19.2 2007 2/13/14 0-1 6.98 6.57 51.5 51.5 19.2 1961 2/13/14 0-1 6.53 36.0 47.5 16.3 2017 2/11/14 0-1 6.53 36.0 47.2 22.3 2056 2/11/14 0-1 5.79 39.1 27.7 28.0 2056 2/11/14 1-3 3.87 7.40 34.2 49.2 2056 2/11/14 1-3 3.87 7.95 39.6 19.4 2056 2/11/14 1-3 3.87 7.95 39.6 19.4 2058 2/11/14 1-3 5.86 5.00 39.7 21.0 2168 2/12/14 1-3 5.84 5.67 32.6 23.7 2168 2/12/14 1-3	11.2	35.00	35,00		GL	Ĩ		0,333	0.178	0.218		3.67	-19.1	5.56
200 21/9/4 0.1 0.00 0.10 0.000 0.100 0.100 0.101 0.10	200 2/13/14 0-1 0.98 6.57 51.5 19.2 1961 2/13/14 1-3 6.54 4.40 41.8 51.8 19.3 1961 2/13/14 1-3 6.54 4.40 41.8 220.3 1961 2/13/14 1-3 6.54 4.40 41.8 22.3 2017 2/11/14 1-3 6.54 4.40 41.8 22.3 2017 2/11/14 1-3 6.54 4.40 41.8 22.3 2056 2/11/14 1-3 3.87 7.95 38.4 17.4 2058 2/11/14 1-3 3.86 8.00 38.0 19.4 2058 2/11/14 1-3 3.86 5.67 32.6 21.0 1958 2/13/14 1-3 3.86 5.67 33.0 19.4 2056 2/11/14 1-3 3.86 5.67 32.6 21.0 2051 2/17/14 1-3 3.86 <td>11.7</td> <td>35.00</td> <td>36.25</td> <td></td> <td>сг</td> <td></td> <td></td> <td>0.339</td> <td>0.162</td> <td>0.230</td> <td></td> <td>3.67</td> <td>-19.2</td> <td>5.07</td>	11.7	35.00	36.25		сг			0.339	0.162	0.230		3.67	-19.2	5.07
200 210944 13 626 636 100 0238 2010 0238 2010 0238 2010 0238 2013 215 216 217144 13 616 400 13 270 401 1338 100 0238 0100 0238 2173 517 2017 71141 13 720 720 720 720 720 720 720 720 720 720 720 721 <	200 2/13/14 1-3 6.29 6.88 5/1.8 19.3 1961 2/13/14 1-3 6.54 4.40 7.2 22.3 1961 2/13/14 1-3 6.56 5/19 341.8 280.0 2017 2/11/14 1-3 6.56 5/79 342 40.2 2056 2/11/14 1-3 3.86 7.40 36.4 17.4 2055 2/11/14 1-3 3.87 7.40 36.4 17.4 2056 2/12/14 1-3 3.87 7.40 36.4 17.4 2055 2/12/14 1-3 3.87 7.40 36.4 17.4 2056 2/12/14 1-3 3.87 7.03 42.7 18.3 2056 2/11/14 0-1 6.56 5.70 39.7 18.4 2158 2/11/14 0-1 6.24 5.15 30.7 25.9 2168 2/11/14 0-1 6.24 5.15 <td>12.4</td> <td>35.00</td> <td>35.00</td> <td></td> <td>GL</td> <td>ļ</td> <td></td> <td>0.183</td> <td>0.086</td> <td>0.198</td> <td></td> <td>5.67</td> <td>-8.92</td> <td>2.68</td>	12.4	35.00	35.00		GL	ļ		0.183	0.086	0.198		5.67	-8.92	2.68
10:1 179/41 1:1 0.54 0.461 0.471 0.245 0.461 0.471 0.241 0.	1981 2/13/14 0-1 5.83 3.60 47.2 2.2.3 2017 2/11/14 1.3 6.54 4.40 41.8 281.0 2017 2/11/14 1.3 6.54 4.40 41.8 281.0 2017 2/11/14 1.3 6.54 4.40 41.8 281.0 2056 2/11/14 1.3 3.87 7.95 39.6 19.5 2056 2/12/14 1.3 3.87 7.95 39.6 19.5 2056 2/12/14 1.3 3.87 7.95 39.6 19.4 2051 2/12/14 1.3 3.87 7.95 39.6 19.4 2051 2/12/14 1.3 5.94 7.03 4.27 19.3 2052 2/11/14 1.3 5.88 7.03 4.27 19.3 2195 2/17/14 1.3 5.88 5.67 32.6 23.7 2129 2/17/14 1.3 5.88 5.67	8.76	32.50	37.50		ы			0.551	0.100	0.283		4.67	-24.5	3.12
17114 1.1 0.1 2.0 1.1 1.1 5.0 3.7.0	1961 2/13/14 1-3 0.54 4.40 4.18 28.0 2017 2/11/14 0-1 5,75 5,79 39.1 27.7 2016 2/11/14 0-1 5,76 5,79 39.1 27.7 2056 2/11/14 1-3 7.86 5,79 39.4 7.42 2056 2/11/14 1-3 3.87 7.86 39.6 19.5 2056 2/11/14 1-3 3.87 7.86 39.6 19.4 2056 2/12/14 1-3 3.86 5.00 38.0 19.4 2051 2/12/14 1-3 5.86 5.07 32.6 23.7 2058 2/11/14 1-3 5.84 5.67 32.6 23.7 2148 2/10/14 1-3 5.84 5.67 32.6 25.3 2149 2/10/14 1-3 5.84 5.67 32.6 25.3 2149 2/10/14 1-3 5.84 5.73 <td>2.02</td> <td>42.50</td> <td>35.00</td> <td></td> <td>1</td> <td></td> <td></td> <td>0.533</td> <td>0.103</td> <td>0.241</td> <td></td> <td>5.67</td> <td>-21.7</td> <td>3.23</td>	2.02	42.50	35.00		1			0.533	0.103	0.241		5.67	-21.7	3.23
2017 21114 01 675 573 640 004 0241 0273 647 2056 21114 10 675 573 580 11 670 300 0241 0247 2233 2773 2056 21114 10 336 700 117 0565 0100 117 0569 041 0241 2233 2373 2056 21144 10 613 300 614 103 300 2236 223 2317 2316	2017 2/11/14 0-1 6.75 5.79 39.1 27.7 2056 2/11/14 1-3 7.38 7.62 34.2 49.2 2056 2/11/14 1-3 7.38 7.62 34.2 49.2 2056 2/11/14 1-3 3.87 7.95 39.8 17.4 2051 2/12/14 1-3 3.87 7.95 39.8 17.4 2051 2/12/14 1-3 3.87 7.95 39.8 19.4 2051 2/12/14 1-3 3.86 8.00 38.0 19.4 2052 2/11/14 1-3 3.86 5.67 32.8 19.4 2132 2/11/14 1-3 4.58 5.67 32.6 21.0 2149 2/11/14 1-3 5.61 3.23 42.0 25.3 2149 2/10/14 1-3 5.68 5.77 32.6 21.8 2149 2/10/14 1-3 5.88 5.33 <td>1.93</td> <td>37,50</td> <td>37.50</td> <td>25.00</td> <td></td> <td></td> <td></td> <td>0.342</td> <td>0.002</td> <td>0.087</td> <td></td> <td>1.69</td> <td>-1.78</td> <td>0.07</td>	1.93	37,50	37.50	25.00				0.342	0.002	0.087		1.69	-1.78	0.07
2017 2114 1 7 3 1 1 2 </td <td>2017 2/11/14 1-3 7.38 7.62 34.2 49.2 2056 2/11/14 1-3 3.87 7.40 36.4 17.4 2056 2/11/14 1-3 3.87 7.40 36.4 17.4 2051 2/12/14 1-3 3.86 8.00 38.0 19.4 2051 2/12/14 1-3 3.86 8.00 38.0 19.4 2051 2/12/14 1-3 3.86 7.03 42.7 18.3 2051 2/12/14 1-3 4.68 7.03 42.7 18.3 2129 2/11/14 0-1 6.24 5.15 40.0 19.4 2129 2/11/14 0-1 6.24 5.15 40.0 19.4 2148 2/10/14 0-1 6.24 5.15 40.0 18.7 2160 2/10/14 0-1 5.86 5.46 5.70 49.2 25.9 2160 2/10/14 0-1 5.86<td>1.67</td><td>45,00</td><td>30.00</td><td>25.00</td><td>-</td><td></td><td></td><td>0.604</td><td>0.041</td><td>0.262</td><td></td><td>4.67</td><td>-23.7</td><td>1.29</td></td>	2017 2/11/14 1-3 7.38 7.62 34.2 49.2 2056 2/11/14 1-3 3.87 7.40 36.4 17.4 2056 2/11/14 1-3 3.87 7.40 36.4 17.4 2051 2/12/14 1-3 3.86 8.00 38.0 19.4 2051 2/12/14 1-3 3.86 8.00 38.0 19.4 2051 2/12/14 1-3 3.86 7.03 42.7 18.3 2051 2/12/14 1-3 4.68 7.03 42.7 18.3 2129 2/11/14 0-1 6.24 5.15 40.0 19.4 2129 2/11/14 0-1 6.24 5.15 40.0 19.4 2148 2/10/14 0-1 6.24 5.15 40.0 18.7 2160 2/10/14 0-1 5.86 5.46 5.70 49.2 25.9 2160 2/10/14 0-1 5.86 <td>1.67</td> <td>45,00</td> <td>30.00</td> <td>25.00</td> <td>-</td> <td></td> <td></td> <td>0.604</td> <td>0.041</td> <td>0.262</td> <td></td> <td>4.67</td> <td>-23.7</td> <td>1.29</td>	1.67	45,00	30.00	25.00	-			0.604	0.041	0.262		4.67	-23.7	1.29
2016 211/14 0:1 316 17.4 17.1 17.5 17.6 0.01 17.6 0.01 0.17.5 0.015 0.443 348 2.35 2058 217/14 1:3 387 500 19.4 17.7 47.0 30.0 250 1 ~0.00 117 0630 0.033 34.3 2.35 2058 27714 1:1 5.1 2.01 117 0.50 0.000 0.472 34.9 2.35 2051 27724 0.11 1.0 5.7 19.3 19.3 7.00 1.17 0.66 0.00 0.472 2.35 2051 2774 0.11 0.11 0.17 0.175 0.014 0.193 2.35 2051 2771/14 1.1 2.35 7.35 7.35 7.35 2.01 1.77 0.14 0.26 2.35 2.55 2051 217 1.3 2.35 2.35 2.00 1.27 0.010	2056 2/11/14 0-1 3.96 7.40 364 17.4 2056 2/12/14 1-3 3.87 7.95 39.6 19.5 2056 2/12/14 1-3 3.87 7.95 39.6 19.5 2051 2/12/14 1-3 3.87 7.95 39.6 19.4 2051 2/12/14 1-3 3.87 7.03 4.27 18.3 1958 2/13/14 1-3 6.94 7.03 4.27 18.3 2055 2/11/14 1-3 6.94 7.03 4.27 18.3 2129 2/11/14 1-3 5.88 5.43 33.7 18.4 2139 2/10/14 1-3 5.86 5.43 39.7 25.8 2140 2/10/14 1-3 5.48 5.70 49.7 18.7 2141 2/10/14 1-3 5.48 5.70 49.7 20.6 2142 2/10/14 1-3 5.48 5.70	1.43	55.00	26.25		SL							27.73	2.01	
2058 21/1/4 13 387 7/95 900 145 149 20.4 200 310 1117 0655 0003 0.443 349 -2.35 2051 21/214 13 630 630 164 110 215 117 0655 0030 0.443 349 -2.35 2051 21/214 13 630 630 320 117 0655 0.030 0.443 349 -2.35 2051 21/24 13 630 722 139 128 4200 700 1171 0655 0.039 0.443 349 -2.35 2162 214 610 712 139 128 4200 710 1571 1008 0.473 349 2.35 347 2.33 279 108 2.43 2.33 2.43 2.33 2.43 2.33 2.43 2.33 2.43 2.33 2.43 2.33 2.43 2.33 2.43	2056 2/11/14 1-3 3.87 7.95 39.8 19.5 2051 2/12/14 1-3 3.86 8.00 38.0 19.4 2051 2/12/14 1-3 3.86 8.00 38.0 19.4 2051 2/12/14 1-3 5.96 5.07 32.4 21.0 1958 2/13/14 1-3 6.94 7.03 42.7 18.4 2129 2/11/14 1-3 6.94 7.03 42.7 18.4 2129 2/11/14 1-3 6.84 7.03 42.7 18.4 2149 2/11/14 1-3 5.88 5.61 3.23 42.0 25.9 2149 2/10/14 1-3 5.86 5.70 49.8 27.8 2149 2/10/14 1-3 5.86 5.70 49.8 7.03 2149 2/10/14 1-3 5.86 5.70 49.2 25.9 2165 2/10/14 1-3 5.70 <td>1.75</td> <td>47.50</td> <td>30.00</td> <td>22.60</td> <td>-</td> <td></td> <td></td> <td>2172</td> <td>0,015</td> <td>0.429</td> <td></td> <td>-2.35</td> <td>-38.5</td> <td>0.47</td>	1.75	47.50	30.00	22.60	-			2172	0,015	0.429		-2.35	-38.5	0.47
2016 21/14 13 316 100 114 100 117 0.663 0.000 0.472 349 2363 2016 27/244 13 0.01 0.01 0.014 0.014 0.024 0.014 0.	2056 2/11/14 1.3 3.86 8.00 38.0 19.4 2051 2/12/14 0.1 6.05 6.52 39.8 19.4 2058 2/13/14 0.1 6.05 6.57 32.6 19.4 1958 2/13/14 0.1 6.15 6.57 32.8 19.4 1958 2/13/14 0.1 4.12 6.77 32.6 23.7 18.9 2129 2/11/14 0.1 4.12 6.77 32.6 23.7 23.6 2129 2/11/14 0.1 4.16 6.77 32.6 23.7 23.6 2129 2/11/14 0.1 6.16 3.43 37.7 21.9 23.7 2149 2/10/14 1.3 5.61 3.23 42.0 26.3 2160 2/10/14 1.3 5.61 3.73 32.7 16.7 2160 2/10/14 1.3 3.25 6.37 32.6 26.8 2160	2.01	40.00	35.00	25.00	1			0.635	0.039	0.443		-2.35	-37.2	1.22
2011 212/14 011 615 635 394 194 013 3250 4125 2855 1 0387 0715 0271 0174 018 223 337 1588 27144 011 412 677 233 237 231 237 231 237 231 233 530 234 233 233 530 234 233 530 234 233 530 234 233 530 234 233 530 234 233 530 234 <	2051 2/12/14 0-1 6.05 6.52 39.8 19.4 2055 2/12/14 1-3 6.94 7.03 42.7 18.3 2055 2/13/14 1-3 6.94 7.03 42.7 18.3 1958 2/13/14 1-3 6.94 7.03 42.7 18.3 2129 2/11/14 1-3 6.88 7.03 42.7 18.3 2129 2/11/14 1-3 5.88 7.46 37.8 18.4 2129 2/11/14 1-3 5.88 7.46 37.8 18.4 2149 2/10/14 1-3 5.48 5.70 49.2 25.9 2140 2/10/14 1-3 5.48 5.70 49.2 21.8 2140 2/10/14 1-3 5.58 5.18 43.3 18.7 2141 2/10/14 1-3 5.28 9.38 3.6.7 22.8 2145 2/10/14 1-3 3.22 9.38 <td>2.00</td> <td>41.25</td> <td>33.75</td> <td>25.00</td> <td>-</td> <td>į.</td> <td></td> <td>0.636</td> <td>600'0</td> <td>0.472</td> <td></td> <td>-2.35</td> <td>-37.2</td> <td>0.28</td>	2.00	41.25	33.75	25.00	-	į.		0.636	600'0	0.472		-2.35	-37.2	0.28
2011 212/14 1; 6;4 7/03 4;2 7/03 4;2 7/03 4;2 7/03 1/04 1/16 1/1	2051 2/12/14 1-3 6.84 7.03 427 18.3 1958 2/13/14 0-1 4.12 6.77 32.4 21.0 1958 2/11/14 0-1 4.12 6.77 32.4 21.0 2129 2/11/14 0-1 4.35 5.88 5.67 32.4 21.0 2129 2/11/14 0-1 6.34 5.15 40.0 19.9 21306 2/11/14 1-3 5.88 4.468 37.8 18.4 21095 2/10/14 0-1 6.53 5.88 3.43 39.7 25.3 2160 2/10/14 0-1 5.58 5.48 5.70 49.2 23.3 2160 2/10/14 0-1 5.53 5.18 43.3 19.7 2167 2/10/14 0-1 5.53 5.18 43.3 19.7 2167 2/10/14 1-3 5.33 8.7 20.3 23.5 2167 2/10/14 </td <td>11.7</td> <td>32.50</td> <td>41.25</td> <td>26.25</td> <td>_</td> <td></td> <td></td> <td>0.274</td> <td>0.174</td> <td>0.267</td> <td></td> <td></td> <td>-18.7</td> <td>5.44</td>	11.7	32.50	41.25	26.25	_			0.274	0.174	0.267			-18.7	5.44
1988 213/14 0.1 14.12 6.77 2.44 0.10 1.57 1.008 0.084 0.685 6.93 5.30 1283 2171/14 0.1 6.47 2.24 2.10 217 0.001 1.57 1.008 0.064 0.685 6.93 5.30 2.30 2.33 0.014 0.506 0.244 2.45 1.66 2128 271/14 1.3 5.61 3.75 3.750 37.50 <td>1968 2/13/14 0-1 4,12 6,77 32.4 21.0 1958 2/13/14 1-3 4.45 5.67 32.6 23.7 2129 2/17/14 1-3 5.83 5.67 32.6 23.7 2129 2/17/14 1-3 5.83 5.67 32.6 23.7 2149 2/17/14 1-3 5.61 3.43 39.7 25.8 2149 2/10/14 1-3 5.61 3.23 42.0 25.3 2149 2/10/14 1-3 5.61 3.43 39.7 25.8 2149 2/10/14 1-3 5.61 3.23 42.0 25.3 2160 2/10/14 1-3 5.63 5.18 43.3 18.7 2165 2/10/14 1-3 5.43 5.74 3.83 2.03 2165 2/10/14 1-3 5.43 6.74 3.83 2.03 2148 2/10/14 1-3 5.44 7.44<td>18.9</td><td>30.00</td><td>40.00</td><td></td><td>5</td><td></td><td></td><td></td><td>0.044</td><td>0.169</td><td></td><td></td><td>-10.3</td><td>1.37</td></td>	1968 2/13/14 0-1 4,12 6,77 32.4 21.0 1958 2/13/14 1-3 4.45 5.67 32.6 23.7 2129 2/17/14 1-3 5.83 5.67 32.6 23.7 2129 2/17/14 1-3 5.83 5.67 32.6 23.7 2149 2/17/14 1-3 5.61 3.43 39.7 25.8 2149 2/10/14 1-3 5.61 3.23 42.0 25.3 2149 2/10/14 1-3 5.61 3.43 39.7 25.8 2149 2/10/14 1-3 5.61 3.23 42.0 25.3 2160 2/10/14 1-3 5.63 5.18 43.3 18.7 2165 2/10/14 1-3 5.43 5.74 3.83 2.03 2165 2/10/14 1-3 5.43 6.74 3.83 2.03 2148 2/10/14 1-3 5.44 7.44 <td>18.9</td> <td>30.00</td> <td>40.00</td> <td></td> <td>5</td> <td></td> <td></td> <td></td> <td>0.044</td> <td>0.169</td> <td></td> <td></td> <td>-10.3</td> <td>1.37</td>	18.9	30.00	40.00		5				0.044	0.169			-10.3	1.37
1988 2713/14 13 448 567 32.6 23.7 146 63.7 23.0 14.7 13.1 14.8 17.7 13.1 14.8 17.7 13.1 14.8 27.1 14.1 14.1 14.8 14.7 14.8 14.7 14.8 14.7 14.8 14.7 14.8 14.7 14.8 14.7 14.8 14.7 14.8 14.7 14.8 14.7 14.8 14.7 14.8 1	1968 2/13/14 1-3 4.58 5.67 32.6 23.7 2129 2/11/14 0-1 6.84 5.15 40.0 19.9 2129 2/11/14 0-1 6.88 4.86 5.15 40.0 19.9 2095 2/11/14 1-3 5.51 3.43 39.7 25.9 2095 2/11/14 1-3 5.51 3.23 42.0 25.3 2149 2/10/14 1-3 5.61 3.23 42.0 25.3 2145 2/10/14 1-3 5.616 5.32 48.6 21.8 2167 2/10/14 1-3 5.616 6.32 48.7 26.6 2167 2/10/14 1-3 5.35 5.18 4.83 16.7 2165 2/10/14 1-3 3.24 7.44 38.7 20.3 2148 2/10/14 1-3 3.24 7.44 38.7 20.3 2148 2/10/14 1-3 3.24 </td <td>1.28</td> <td>42,50</td> <td>37.50</td> <td>20.00</td> <td>1</td> <td></td> <td></td> <td></td> <td>0.084</td> <td>0.485</td> <td></td> <td></td> <td>-54.6</td> <td>2.62</td>	1.28	42,50	37.50	20.00	1				0.084	0.485			-54.6	2.62
212 211/14 01 624 515 400 193 307 433 800 3750 36.55 1 0.065 0.237 0.016 0.247 239 267 2113 211/14 1 4 456 343 817 239 807 239 106 0.787 0.668 0.787 109 147 10 147 10 147 10 147 10 147 10 147 10 1016 0.787 0.166 0.787 0.167 0.167 1016 1016 1016 0.187 0.1	2128 2/11/14 0.1 6.24 5.15 40.0 19.9 2129 2/11/14 1.3 5.88 ,4.68 37.8 18.4 20965 2/11/14 1.3 5.88 ,4.68 37.8 18.4 20965 2/11/14 1.3 5.81 ,4.68 37.8 18.4 20965 2/10/14 1.3 5.86 6.32 48.6 21.8 2149 2/10/14 1.3 5.86 6.32 48.6 21.8 2145 2/10/14 1.3 5.86 6.32 48.6 21.8 2167 2/10/14 1.3 5.88 5.18 43.3 18.7 2165 2/10/14 0.1 5.53 5.18 38.7 20.3 2146 2/10/14 0.1 5.53 5.48 5.64 20.6 2146 2/10/14 0.1 5.53 5.18 38.7 20.3 2146 2/10/14 1.3 5.53 5.	0.91	46.25	33.75	20.00	_				0.084	0.508		2.35	-44.6	2.62
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2128 2/11/14 1-3 5.88 4.68 37.8 18.4 2095 2/11/14 0-1 4.95 3.43 39.7 25.9 2095 2/11/14 0-1 4.95 3.43 39.7 25.9 2095 2/11/14 0-1 5.88 5.43 39.7 25.9 2160 2/10/14 0-1 5.86 5.32 48.6 21.8 2160 2/10/14 0-1 5.88 5.18 43.3 19.7 2167 2/10/14 0-1 5.53 5.18 43.3 19.7 2167 2/10/14 0-1 5.53 5.18 43.3 19.7 2167 2/10/14 0-1 5.53 5.18 43.3 19.7 2145 2/10/14 0-1 7.42 3.84 2.03 2146 2/10/14 1-3 5.33 8.7 2.03 2146 2/10/14 1-3 3.44 7.44 36.5 19.6	9.60	37,50	36.25	26.25	5				0.106	0,267		2.67	-21.3	3.32
2006 211/14 0.1 4.95 3.43 3.97 25.9 45.0 6.26 1.04 47.50 30.00 22.60 1 0.146 0.144 0.196 17.5 166 2149 210/14 0.1 566 3.23 4.26 3.50 3.500 1.0 0.166 0.661 0.175 166 1.35 2149 270/14 0.1 566 5.23 4.05 3.500 35.00 0.500 0.175 166 1.35 246 1.35 246 1.35 246 1.35 246 1.35 246 1.35 246 1.35 360 35.00 0.10 0.341 0.175 0.166 0.174 0.135 0.136 0.135 216 1.06 2167 210/14 0.1 7.44 36.5 36.7 0.757 0.144 0.175 0.166 0.661 0.014 0.165 0.166 0.166 0.166 0.666 0.272 0.104 0.175 <td>2085 211/14 0-1 4.95 3.43 387 25.9 2095 21/1/14 1-3 5.61 3.23 3.87 25.3 2095 21/1/14 1-3 5.61 3.23 42.0 25.3 2149 27/0/14 1-3 5.61 3.23 42.0 25.3 2150 27/0/14 1-3 5.68 5.70 49.2 22.3 2167 27/0/14 1-3 5.68 5.70 49.2 22.3 2167 27/0/14 1-3 5.58 6.30 43.7 18.6 2167 27/0/14 1-3 5.48 6.70 49.3 18.7 2165 27/0/14 1-3 5.35 6.47 36.7 20.3 2165 27/0/14 1-3 5.33 6.14 45.3 20.3 2165 27/0/14 1-3 5.33 6.14 45.3 20.3 2165 27/0/14 1-3 5.33 6.14</td> <td>8.07</td> <td>37.50</td> <td>37.50</td> <td>25.00</td> <td>_</td> <td></td> <td></td> <td></td> <td>0.218</td> <td>0.244</td> <td></td> <td></td> <td>-22.9</td> <td>6.80</td>	2085 211/14 0-1 4.95 3.43 387 25.9 2095 21/1/14 1-3 5.61 3.23 3.87 25.3 2095 21/1/14 1-3 5.61 3.23 42.0 25.3 2149 27/0/14 1-3 5.61 3.23 42.0 25.3 2150 27/0/14 1-3 5.68 5.70 49.2 22.3 2167 27/0/14 1-3 5.68 5.70 49.2 22.3 2167 27/0/14 1-3 5.58 6.30 43.7 18.6 2167 27/0/14 1-3 5.48 6.70 49.3 18.7 2165 27/0/14 1-3 5.35 6.47 36.7 20.3 2165 27/0/14 1-3 5.33 6.14 45.3 20.3 2165 27/0/14 1-3 5.33 6.14 45.3 20.3 2165 27/0/14 1-3 5.33 6.14	8.07	37.50	37.50	25.00	_				0.218	0.244			-22.9	6.80
2066 2111/14 1:3 551 3:23 4:20 5:50 3:500 1:04 0:467 0:686 0:752 0:174 1:90 4:67 2149 21/0/14 1:3 548 5:72 488 7:1 745 30:00 35:00 35:00 2:00 1:35 5:00 1:36 1:35 2160 21/0/14 1:3 548 5.70 35:00 35:00 2:00 1:0 1:35 5:0 1:36 1:35 2160 21/0/14 1:3 548 5.70 36:00 35:00 2:00 1:1 1:35 3:1 1:35 3:1 1:35 3:1 1:10 1:25 2:33 3:67 2:33 3:67 2:33 3:67 2:33 3:67 2:35 0:10 1:10 1:25 0:10 1:10 1:25 0:10 1:10 1:10 1:10 1:10 1:10 1:10 1:10 1:10 1:10 1:10 1:10 1:10 1	2065 211/14 1-3 5.51 3.23 4.2.0 2.53 2149 210014 0-1 5.88 6.32 48.6 21.8 2140 210014 0-1 5.68 6.32 48.6 21.8 2150 210014 0-1 5.53 5.18 43.7 18.7 2167 21014 1-3 5.68 6.30 43.7 18.6 2167 21014 1-3 5.28 6.30 43.7 18.6 2167 21014 1-3 3.44 3.64 20.6 2167 21014 1-3 3.44 3.64 20.6 2148 21014 1-3 3.44 38.7 20.3 2148 21014 1-3 6.76 4.31 38.7 20.3 2165 21014 1-3 6.78 4.31 38.7 20.3 2165 21014 1-3 6.78 4.31 38.7 20.3 2165 <td>1.04</td> <td>47.50</td> <td>30.00</td> <td>22.50</td> <td></td> <td></td> <td></td> <td></td> <td>0.114</td> <td>0.186</td> <td></td> <td></td> <td>-15.8</td> <td>3.55</td>	1.04	47.50	30.00	22.50					0.114	0.186			-15.8	3.55
2149 2/10/14 0.1 5.88 6.32 48.6 2.18 33.4 5.26 35.00 35.00 35.00 25.00 13.5 26.0 10.6 0.250 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 <th0.6< th=""> <th0.6< th=""> <th0.6< th=""></th0.6<></th0.6<></th0.6<>	2140 210/14 0-1 5.88 6.32 4.8.5 21.8 2160 210/14 1-3 5.48 5.70 49.2 22.3 2160 210/14 1-3 5.48 5.70 49.2 22.3 2167 210/14 1-3 5.58 5.70 49.2 22.3 2167 210/14 1-3 5.58 5.30 43.3 18.7 2167 210/14 1-3 5.58 5.38 36.4 20.6 2148 210/14 1-3 3.25 9.38 36.4 20.3 2148 210/14 1-3 3.44 7.44 36.5 19.6 2148 210/14 1-3 5.33 6.14 45.3 20.3 2146 21/4/14 0-1 4.17 4.67 20.3 2166 21/4/14 0-1 4.80 6.75 45.4 19.9 580 21/4/14 1-3 5.33 6.14 45.3	1.04	42.50	32.50	25.00	-				0.152	0.174			-14.3	4.75
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	2148 270/14 1-3 5.48 5.70 49.2 22.3 2150 270/14 0-1 5.53 5.18 4.3 18.7 2167 2710/14 0-1 5.53 5.18 4.3 18.7 2167 2710/14 0-1 5.53 5.18 4.3 18.7 2167 2710/14 0-1 5.55 5.18 4.3 18.7 2167 2710/14 0-1 5.55 5.18 4.3 36.5 19.6 2148 2710/14 1-3 3.44 7.44 36.5 19.6 2148 2710/14 1-3 3.74 7.44 36.5 19.6 2148 2710/14 1-3 6.72 3.84 20.3 20.3 2146 2710/14 1-3 5.33 6.14 45.3 20.8 580 2714/14 0-1 4.80 6.75 45.4 19.9 580 214/14 1-3 5.38	9.52	35,00	35.00						0.167	0.245			-27.4	5.20
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	2150 210/14 0.1 5.53 5.18 43.3 19.7 2150 210/14 1.3 5.28 5.18 43.3 19.7 2167 210/14 1.3 5.28 5.30 43.7 19.6 2167 210/14 1.3 5.28 5.30 43.7 19.6 2167 210/14 1.3 5.28 5.30 43.7 19.6 2148 210/14 1.3 3.44 7.44 36.5 19.6 2146 210/14 1.3 5.39 4.31 38.7 20.3 2165 210/14 1.3 6.78 4.31 38.7 20.3 2165 210/14 1.3 5.33 6.14 45.3 20.8 580 214/14 0.1 4.80 6.75 45.4 19.9 580 214/14 1.3 5.38 5.68 37.6 14.3 2038 211/14 1.3 3.88 5.57	7.45	30.00	37.50						0.122	0.277			-19.9	3.80
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	2150 21'0'14 1-3 6.28 6.30 43.7 18.6 2167 21'01'4 1-3 6.28 6.30 43.7 18.6 2167 21'01'4 1-3 3.4 7.44 36.5 9.0.6 2148 21'01'4 1-3 3.4 7.44 36.5 10.6 2148 21'01'4 1-3 6.76 4.31 38.7 20.3 2148 21'01'4 1-3 6.76 4.31 38.7 20.3 2165 21'01'4 1-3 6.76 4.31 38.7 20.3 2165 21'01'4 1-3 6.32 4.67 4.43 20.6 2165 21'01'4 1-3 6.33 6.14 45.2 20.3 2165 21'01'4 1-3 6.36 6.69 45.4 19.9 580 21'41'4 1-3 6.96 5.69 37.6 14.3 2038 21'1/1/4 0-1 3.88 5.57	7.51	35.00	38.75	26.25	_				0.155	0.232			-23.0	4.83
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	2167 21/014 0-1 3.25 9.38 36.4 20.6 2167 21/014 1-3 3.44 7.44 36.5 19.6 2148 21/0144 1-3 7.42 36.5 19.6 2148 21/0144 1-3 7.42 36.5 19.6 2146 21/0144 0-1 7.42 36.7 20.3 2146 21/0144 0-1 4.72 4.67 44.2 20.3 2165 21/0144 1-3 5.33 6.14 45.3 20.8 2165 21/414 0-1 4.72 4.67 44.2 20.3 2165 21/414 0-1 4.80 6.75 45.4 19.9 580 21/414 1-3 5.33 6.14 45.3 20.8 580 21/114 0-1 3.88 5.57 37.4 14.3 2038 21/114 1-3 3.88 5.57 37.4 14.3	12.2	38.75	33.75		Ì				0.271	0.122			-19.6	8.47
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	2167 21/0/14 1-3 3.44 7.44 36.5 19.6 2148 21/0/14 0-1 7.42 3.94 38.7 20.3 2148 21/0/14 0-1 7.42 3.94 38.7 20.3 2165 21/0/14 0-1 4.72 4.67 44.2 20.3 2165 21/0/14 1-3 5.33 6.14 45.3 20.8 580 2/14/14 0-1 4.80 6.75 45.4 19.9 580 2/14/14 0-1 4.80 6.75 45.4 19.9 580 2/14/14 1-3 5.33 6.14 45.3 20.8 580 2/14/14 1-3 5.93 5.69 42.0 14.3 2038 2/14/14 1-3 5.94 5.66 42.0 14.3 2038 2/11/14 1-3 3.88 5.57 37.6 16.3	3.53	38.75	36.25	25.00	2				0.044	0.294			41.4	1.37
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	2148 2/10/14 0-1 7.42 3.94 38.7 20.3 2146 2/10/14 1-3 6.78 4.31 38.3 20.3 2165 2/10/14 1-3 6.78 4.31 38.3 22.9 2165 2/10/14 1-3 5.33 6.14 45.3 20.3 2165 2/14/14 1-3 5.33 6.14 45.3 20.8 580 2/14/14 0-1 4.80 6.75 45.4 19.9 580 2/14/14 1-3 5.33 6.14 45.3 20.8 580 2/14/14 1-3 5.80 5.68 42.0 14.3 2038 2/11/14 1-3 3.88 5.57 37.6 16.3 2038 2/11/14 0-1 3.98 5.57 37.6 16.3	3.62	47.50	32.50	20.00					0.076	0.250			-33.1	2.38
2148 2/10/14 1-3 6.76 4.31 38.3 22.9 20.6 31.7 6.76 30.00 22.50 L 0.667 0.652 0.446 -0.007 0.205 194 567 2165 2/10/14 0-1 4.72 487 44.2 20.3 36.0 42.5 8.01 32.50 21.9 -10.46 0.065 0.220 21.9 -10.4 2165 2/10/14 0-1 4.72 4.87 13.9 80.0 37.50 35.56 CL <0.010	2148 2/10/14 1-3 6.76 4.31 38.3 22.9 2165 2/10/14 D-1 4.72 5.46 4.31 38.3 22.9 2165 2/10/14 D-1 4.73 5.46 4.42 20.3 2165 2/10/14 D-1 4.73 5.33 6.14 4.42 20.3 2165 2/14/14 D-1 4.80 6.75 4.54 19.9 580 2/14/14 D-1 4.80 6.75 4.54 19.9 2036 2/11/14 D-1 3.98 5.67 3.76 14.3 2036 2/11/14 D-3 3.88 5.57 3.76 16.3	8.08	41.25	32.50	26.25	-				0,005	0.150			1.37	0.17
2165 2/10/14 D-1 4.72 4.87 44.2 203 35.0 42.5 8.01 32.50 36.25 31.25 CL <0.010	2165 221014 0-1 4.72 4.67 44.2 20.3 2166 221014 1-3 5.33 6.14 45.3 20.8 580 221414 0-1 4.80 6.75 45.4 19.9 580 221414 1-3 6.96 5.69 42.0 14.3 2038 221114 0-1 3.98 5.57 37.6 16.3 2038 221174 1-3 3.88 5.57 37.6 16.3	6.79	47.50	30.00	22.50				Ĵ	200.0	0.205			-13.8	-0.20
2165 2/10/14 1-3 5.33 6.14 45.3 20.8 42.2 62.2 11.1 30.00 37.50 32.60 CL 0.066 0.645 0.360 0.084 0.201 20.1 0.66 580 2/14/14 0-1 4.80 6.75 45.4 19.9 80.0 63.9 9.06 30.00 41.25 28.75 CL <0.010	2165 2110114 1-3 5.33 5.14 45.3 20.8 580 2114114 0-1 4.80 5.75 45.4 19.9 580 2114114 1-3 5.96 5.68 42.0 14.3 2036 2111114 0-1 3.95 4.96 37.4 14.3 2036 2111114 0-1 3.88 5.57 37.6 16.3	8.01	32.50	36.25		10				0.065	0.220			-32.3	2.01
580 21414 0-1 4.80 6.76 45.4 19.9 80.0 63.8 9.05 30.00 41.25 28.75 CL <0.010	580 2/14/14 0-1 4.80 6.75 45.4 19.9 560 2/14/14 1-3 6.96 5.69 42.0 14.3 2036 2/11/14 0-1 3.98 5.57 37.6 16.3 2036 2/11/14 0-3 3.88 5.57 37.6 16.3	11.1	30.00	37,50		5				0.084	0.201			-19.5	2.64
580 214414 1-3 6.96 5.68 42.0 14.3 29.1 64.8 13.9 30.00 42.60 27.50 CL 0.467 1.006 0.325 0.308 0.374 31.4 4.67 2036 2/11/14 0-1 392 4.96 37.4 14.3 131 10.9 1.28 47.50 31.5 L <0.010	580 2/14/14 1.3 6.96 5,69 42.0 14.3 2038 2/11/14 0-1 3.92 4.96 37.4 14.3 2038 2/11/14 1.3 3.88 5.57 37.6 16.3	9.05	30.00	41.25						0.093	0.320		0.34	-30.3	2.91
2036 2/11/14 0-1 3.92 4.96 374 14.3 131 10.9 1.28 47.50 31.25 21.25 L <0.010 1.216 0.829 0.019 0.368 38.0 4.35 2038 2/11/14 1-3 3.88 5.57 37.6 16.3 151 11.4 1.25 47.50 32.50 L <0.010 1.234 0.814 -0.030 0.451 38.5 4.35 2036 2/11/14 1-3 3.86 5.63 39.3 16.9 156 11.6 1.25 47.50 32.50 20.00 L <0.010 1.173 0.726 0.004 0.443 36.6 4.35 2036 2/11/14 1-3 3.86 5.63 39.3 16.9 156 11.6 1.25 47.50 32.50 20.00 L <0.010 1.173 0.726 0.004 0.443 36.6 4.35	2036 2/11/14 0-1 3.92 4.96 37.4 14.3 2036 2/11/14 1-3 3.88 5.57 37.6 16.3	13.9	30,00	42.50			1			0.308	0.374	31.4	4.67	-26.8	9.61
2036 2/11/14 1-3 3.88 5.57 37.6 16.3 151 11.4 1.25 47.50 32.60 20.00 L <0.010 1.234 0.814 -0.030 0.451 38.6 -4.35 2036 2/11/14 1-3 3.86 5.63 39.3 16.9 156 11.6 1.25 47.50 32.50 20.00 L <0.010 1.173 0.726 0.004 0.443 36.6 -4.35	2036 2/11/14 1-3 3.88 5.57 37.6 16.3	1.28	47.50	31.25	21.25		<0.010 1			0.019	0.368	38.0	4.35	-42.3	0.59
· 2036 2/11/14 1-3 3.86 5.63 39.3 16.9 156 11.6 1.25 47.50 32.50 20.00 L <0.010 1.173 0.726 0.004 0.443 36.6 4.35		1.25	47.50	32.50	20.00	1	<0.010	2		0:030	0.451	38.6	4,35	-42.9	-0.95
	: 2036 2/11/14 1-3 3.86 5.63 39.3 16.9	1.25	47.50	32.50-	20.00	1	<0.010		0.726	0.004	0.443	36.6	4.35	-41.0	0.11

PYRS A-B TN/1000TN	-13.5	-16.5	-1.18	-4.25	-4.97	0.70	-0.05	9.81		
TVI 000TN	12.2	11.2	3.84	3.91	4.62	2.97	3.72	0.87		
A-B POT TN/1000TN	-42.0	-45.3	-22.7	-30.1	-31.7	-15.0	-16.9	4.43		
NEUT POT TN/1000TN	-1.35	-5.36	2.67	-0.34	-0.34	3.67	3.67	10.7		
ACID POT TN/10801N	40.6	39.9	25.4	29.8	31.3	18.7	20.5	6.25		
ORG S%	0.335	0.338	0.229	0.296	0.291	0.198	0.214	0.101		
PYR S %	0.390	0.357	0.123	0.125	0.148	0.095	0.119	0.028		
SULFATE S%	0.577	0.582	0.460	0.532	0.564	0.306	0.325	0.071		
TOT \$ %	1.301	1.278	0.812	0.953	1.003	0.599	0.658	0.200		
% CAGO3	<0.010	<0.010	0.267	<0.010	<0.010	0.367	0.367	1.069		
CLASS	Ч	Ļ	СГ	or	СГ	CL	CL		CL	
% CLAY	27.50	26.25	28.75	27,50	27.50	30.00	28.75		37.50	
% SILT	35.00	36.25	36.25	35,00	35.00	33.75	33.75		31.25	
% SAND	37.50	37.50	35.00	37.50	37.50	36.25	37.50		31.25	
SAR	5.23	3.19	11.1	11.3	11.1	12.7	12.0		9.28	
WEOUL	44.4	23.0	60.5	71.8	68.3	63.1	59.2		33.8	
MAGNESIUM	125.1	86.4	42.5	62.1	58.6	30.9	29.9		8.12	
GALGIUM	18.8	17.8	17.0	18.3	17.3	18.8	19.0		18.3	
% SAT	35.8	36.8	41.3	39.9	38.6	41.7	42.2		53.8	
EC MMHO/CM	6.44	4.35	6.26	7.46	7.47	6,44	6.48		4.00	
PH UNITS	4.33	4.31	5.56	5.11	5,19	6.22	6.32		6.81	
SAMPLE	0-1	1-3	0-1	1-3	1-3	0-1	1.3			
SAMPLE DATE	2/11/14	2/11/14	2/12/14	2/12/14	2/12/14	2/11/14	2/11/14			
LOCATION	2073	2073	2052	2052	2052	2091	2091			
GAL#	1402-162-07	1402-162-08	1402-162-09	1402-162-10	402-162-10R	1402-162-11	1402-162-12	QC-29	QC-46	

2014-4

PYR S% ORG		%0	CLASS	% CLAY	% SILT	% SAND	SAR	MEQ/L		MAGNESIUM	CALCIUM MAGNESIUM S MEQIL MEQIL	CM % SAT CALCIUM MAGNESIUM MEQIL MEQIL	S EC MMHO/CM % SAT CALCIUM MAGNESIUM MEQIL MEQIL	PHUMITS ECMMHO/CM % SAT CACIUM MAGNESIUM MEQL MEQL	E SAMPLE PH UNITS EC MNHOICOM % SAT CALCIUM MAGNESUM DEPTH MECUL MECUL MECUL	N SAMPLEDATE SAMPLE DEPTH PHUMIS ECMMHOICM %SAT CALCIUM MAGNESIUM MEQ.L. MEQ.L.
0.59 0.16 0.23	26.0	<0.01	<u>ب</u>	26.25	30.00	43.75	6.47	47.7		88.7	20.0 88.7	36,2 20.0 88.7	7.40 36,2 20.0 88.7	4.18 7.40 36,2 20.0 88,7	0-1 4.18 7.40 36.2 20.0 88.7	6/13/14 0-1 4.18 7.40 36.2 20.0 88.7
0.21	0.68	0.05	-	26,25	32.50	41.25	14.7	82.7		43.3	43.3	38.5 20.1 43.3	9.26 38.5 20.1 43.3	6.21 9.26 38.5 20.1 43.3	1-3 6.21 9.26 38.5 20.1 43.3	1-3 6.21 9.26 38.5 20.1 43.3
0.04	0.72	L <0.01	CL/SCI	27.50	27.50	45.00	9.53	61.3	61.9 61.3		20.9 61.9	36.0 20.9 61.9	8.23 36.0 20.9 61.9	4.68 8.23 36.0 20.9 61.9	4.68 8.23 36.0 20.9 61.9	6/13/14 0-1 4.68 8.23 36.0 20.9 61.9
	0.17	0.71	SL	17.50	20.00	62.50	8.94	42.7			24.6	21.0 24.6	35.7 21.0 24.6	7.41 6,16 35.7 21.0 24.6	7.41 6,16 35.7 21.0 24.6	1-3 7.41 6,16 35.7 21.0 24.6
0.27 0.03 0.30		1.26	1	25,00	36.25	38.75	13.1	81.7	56.4 81.7		56.4	20.9 56.4	32.6 20.9 56.4	10.0 32.6 20.9 56.4	6.90 10.0 32.6 20.9 56.4	0-1 6.90 10.0 32.6 20.9 56.4
	0.38	1.37	-	21,25	32.50	46.25	11.9	56.9	28.3 56.9		28.3	17.5 28.3	29.8 17.5 28.3	1 7.44 7.02 29.8 17.5 28.3	1 7.44 7.02 29.8 17.5 28.3	1-3 7.44 7.02 29.8 17.5 28.3
0.17	0.92	0.05	CL	30.00	30.00	40.00	8.72	57.4			69.3	17.3 69.3	8,40 39.5 17.3 69.3	5.33 8,40 39.5 17.3 69.3	5.33 8,40 39.5 17.3 69.3	0-1 5.33 8.40 39.5 17.3 69.3
0.46 0.20 0.35	1.01	0.16	CL	28.75	32.50	38.75	9.08	56.2	57.1 56.2		57.1	20.0 57.1	40.3 20.0 57.1	5.83 7.85 40.3 20.0 57.1	5.83 7.85 40.3 20.0 57.1	1 1-3 5.83 7.85 40.3 20.0 57.1
0.21		0.38	Ч	30.00	33.75	36,25	16.8	86.6	33.7 86.6	j	19.3 33.7	19.3 33.7	41.6 19.3 33.7	9.36 41.6 19.3 33.7	0-1 5.77 9.36 41.6 19.3 33.7	0-1 5.77 9.36 41.6 19.3 33.7
0.34	0.67	0.38	С	27.50	28.75	43.75	17.5	74.4	18.5 74.4		18.5	17.5 18.5	40.7 17.5 18.5	8.57 40.7 17.5 18.5	1-3 6.37 8.57 40.7 17.5 18.5	· 1-3 6.37 8.57 40.7 17.5 18.5
		0.49	CL	27.50	28.75	43.75	17.2	72.6			18.3	41.6 17.1 18.3	41.6 17.1 18.3	6.35 7.94 41.6 17.1 18.3	1-3 6.35 7.94 41.6 17.1 18.3	6/13/14 1-3 6.35 7.94 41.6 17.1 18.3
0.31		0.05	Ч	32.50	36.25	31.25	21.4	125.8	51.6 125.8	ĺ	17.7 51.6	38.2 17.7 51.6	38.2 17.7 51.6	12.6 38.2 17.7 51.6	0-1 5.65 12.6 38.2 17.7 51.6	0-1 5.65 12.6 38.2 17.7 51.6
0.27		0.49	CL	28.75	36.25	35.00	33.0	155.6			28.3	38,4 16.3 28,3	14.7 38.4 16.3 28.3	6.69 14.7 38.4 16.3 28.3	I 1-3 6.69 14.7 38.4 16.3 28.3	6/13/14 1-3 6.69 14.7 38.4 16.3 28.3
0.15	0.50	0.16	SCL	25.00	26.25	48.75	7.18	37.9		39.8	39.8	40.0 15.8 39.8	40.0 15.8 39.8	6.25 5.91 40.0 15.8 39.8	F 0-1 6.25 5.91 40.0 15.8 39.8	F 0-1 6.25 5.91 40.0 15.8 39.8
0.12	0.62	1.48	-	25.00	28.75	46.25	14.5	65,2		23.7	23.7	36.7 16.6 23.7	7.95 36.7 16.6 23.7	1 7,03 7.95 36.7 16.6 23.7	7,03 7.95 36.7 16.6 23.7	1 1-3 7,03 7.95 36.7 16.6 23.7
	0.83	0.38	CL	27.50	33.75	38.75	6.25	36.2	50.5 36.2	50.5	16.5 50.5	36.6 16.5 50.5	0 36.6 16.5 50.5	5,87 6.30 36.6 16.5 50.5	5,87 6.30 36.6 16.5 50.5	4 0-1 5,87 6.30 36,6 16,5 50,5
0.23	0.89	0.38	5	27.50	28.75	43.75	17.5	81.9			36.1	14.6 36.1	39.9 14.6 36.1	10.3 39.9 14.6 36.1	6.62 10.3 39.9 14.6 36.1	4 1-3 6.62 10.3 39.9 14.6 36.1
	0.20	0.82														
			C	35,00	26.25	38.75	6.43	36.8		6.20	20.8 9.71	44.2 20.8 9.71	4.64 44.2 20.8 9.71	4.64 44.2 20.8 9.71	4.64 44.2 20.8 9.71	6.86 4.64 44.2 20.8 9.71 36.8

4.96 -7.81 1.09 3.86 8.92 0.10 5.12 7.93 -17.2 2.78 5.15 6.94 -19.0 6.28 0.66 -100 -273 3.47 -4.47
8.83 8.92 25.1 7.93 26.0 6.94 26.3 -1.00
0.09 0.32 0.20 0.30 0.11 0.29
0.69 0.83 0.33 <0.01 0.84 0.45
38.75 32.50 CL 37.50 31.25 CL
7.95 28.75 38. 5.69 31.25 37.
93.0 42.3 5.
9.49 38.1 17.5
01.0
conco anacias
ATTO TRA DR

PYRS A-B TN/1000TN	2.34	2.72	0.16	6.38	3.83	0.62	10.1			
PYR A POT TW1000TN	0.53	2.06	2.72	0.31	<0.01	0.34	0.41			
A-B POT TN/1000TN	-27.5	-25.7	-30.5	-32.5	-33.1	-34.7	-16.5	18.6	18.4	
NEUT POT TN/1000TN	2.88	4.78	2.88	6.69	3.83	76.0	10.5	31.5	31.5	
ACID POT TN/1000TN	30.4	30.5	33,4	39.1	36.9	35.6	27.0	13.0	13.1	
ORG S%	0.329	0.305	0.316	0.098	0.113	0.104	0.101			
PYR S %	0.017	0.066	0.087	0.010	<0.010	0.011	0.013			
SULFATE S%	0.627	0.605	0.667	1.145	1.076	1.026	0.750			
TOT S % S	0.974	0.975	1.069	1.253	1.182	1.141	0.864	0.415	0.419	
% CACOS	0.288	0.478	0.288	0.669	0.383	760.0	1.051	3,150	3,150	
CLASS	CL	C	CL	SCL	CL	Ы	CL	CL	CL	
% DLAY	28.75	27.50	32.50	21.25	27.50	28.75	27.50	27.50	27.50	
% 8ILT	32.50	28.75	36.25	25.00	32.50	32.50	32.50	30.00	30.00	
% SAND	38.75	43.75	31.25	53.75	40.00	38.75	40.00	42.50	42.50	
SAR	10.0	13.4	12.5	12.0	10.3	0.6	10.7	14.3	14.7	
sodium Meq.L	77.0	87.4	101	50.0	80.9	71.3	68.3	62.2	64.4	
MAGNESIUM MEQ/L	100	66.8	112	17.2	107	108	63.8	20.2	20.8	
CALCIUM	17.6	17.9	17.71	17.6	17.0	17.2	18.1	17.5	17.5	
% SAT	37.5	36.5	35.6	43.3	36,6	36.2	30.2	36.8	35.7	
EC MMHO/CM	11.9	11.5	14.3	6.68	12.6	12.0	10.1	7.80	7.90	
PH UNITS	5.64	5.94	5,53	5.88	5,90	5.02	2,09	7.72	7.72	
SAMPLE DEPTH	0-1	1-3	0-1	1-3	0-1	1-3	0-1	1-3	0-1	
SAMPLE DATE	11/20/14	11/20/14	11/20/14	11/20/14	11/20/14	11/20/14	11/20/14	11/20/14	11/20/14	
LOCATION	24-3016	24-3016	25-2880	25-2880	25-2850	25-2850	25-2851	25-2851	25-2851	
GALS	411-214-01	1411-214-02	1411-214-03	1411-214-04	1411-214-05	1411-214-06	1411-214-07	1411-214-08	411-214-08R	

SOLSE PPM								
AB-DTPA SE PPM								
TOT SE PPM								
PPM								
PYRS A-6 THUN000TH	11.18	6.38					7.29	-0.33
PYR A POT F	1.47	1.41					0.50	2.28
A-B POT P	-4.44	-15.8	12.6	4.74	6.60	9.15	-4.26	-13.5
NEUT POT A TN/1000TN TN	12.7	7.79	13.6	15.6	12.7	13.6	7.79	1.95
ACID POT NEU TH/1000TN TH/1	17.1	23.6	1.03	10.8	6.05	4,48	12.0	15.5
	160	0.215					0.138	199
N ORG SN	0	0.045 0.						0.073 0.
SK PYR S%	Ĩ.							
SULFATE S%	1	5 0.495	5	1	**			5 0.223
TOT S %	0.547	0.75	0.03	0.34	0.194	0.143	0.386	0.496
% OACO3	1.265	0.779	1.362	1.557	1.265	1.362	0.779	0.195
CLASS	CL	-	4	-	1	SCL	1	ŗ
% CLAY	28.75	25.00	26.25	23.75	25.00	25.00	22.50	20.00
% SILT	36.25	31.25	30.00	30.00	28.75	26.25	32.50	32.50
ONS M	35.00	43.75	43.75	46.25	46.25	48.75	45.00	47.50
AAR	13.3	12.3	3.15	3.32	5.02	6.13	25.8	19.1
NEQUL	68.3	63.5	8.74	8.66	24.0	29.1	116	90.9
MEQU	34.5	36.0	7.44	6.79	24.4	23.4	24.4	27.2
MEQIL MI	18.3	17.5	7.93	6.79	21.4	21.6	15.8	18.0
% SAT G			38.7		33.0	34.7		30.7
BC MMHOIGM						5,45		
PH UNITS BC N						6.65		
SAMPLE PH DEPTH PH						1-3		
SAMPLE DATE SA						11/20/14		
LOCATION SAMP						41-620 11/		
Ê(1							Ľ.
4 TVD	1411-215-01	1411-215-02	1411-215	1411-215	1411-215	1411-215-06	1411-215-07	1411-215-06

NT000FINT	-1.21	9.01	3.74	15.49	1.33	3.63	-			12.82	13 72	3.82	208	5.74	-0.44		8.37	7.51	6.06	5.13			5.41	7.58	-2.84	19.8	12.2	6.39				-0,89	-6.66	7.01	5.92		10.3	-0.40		2.32	3.68	
TN/1000TN TN/1	4.72	2.19	2.66	1.47	5.06	0.84				2 22	2.28	0.66	5.22	0.31	2.03		0.91	0.16	3.22	3.19			2.91	2,66	2.84	1.00	7.87	3.84				4.40	3.25	0.34	7.47		1.61	1.03		0.34	-0.69	
								12	0					Ś				Ĵ				94								11	8									ģ		
TN/10001/N1	11- 1	-3.6	9 -28												9 -23.0																										9.2	
NIMONUNT	3.5	11.	6.3	17.	6.3	4.4	251	. 66	23.	15 (16.0	4.4	11	5.4	1.59	15.0	9.26	7.36	9.26	8.3	13.12	23.7	8.3	10.2	<0.010	20.8	13.	10.2	14.1	6.36	7.35	3.51	1.55	7.35	6.35	18.5	12.2	0.62		2.0	3.0	
TN/10001N	14.8	14.9	34.4	20.3	26.1	56.2	14.0	141	13.7	28.2	24.9	26.7	21.5	28.2	24.6	10.2	1.11	12.4	13.5	13.7	8.4	15.7	13.7	33.1	35.3	32.2	14.7	21.6	9.43	6.19	6.87	29.3	31.6	8.2	16.9	15.7	21.9	15.4		12.4	12.2	
ORG S%	0.180	0.109	0.722	0.274	0.241	0.800	1111			0.359	0.364	0.375	0.219	0.364	0.401		0.229	0.237	0.126	0.131			0.128	0.362	0.381	0.416	0.229	0.197				0.330	0.204	0.091	0.184		0.243	0.191		0.129	0.146	
PYR 5%	0.151	0.070	0.085	0.047	0.162	0.027				0.071	0.073	0.021	0.167	-0.010	0.065		0.029	-0.005	0.103	0.102			0.093	0.085	0.091	0.032	0.028	0.123				0.141	0.264	0.011	0.015		0.061	0.033		-0.011	-0.022	
SULFATE S%	0.142	0.297	0.295	0.330	0.434	0.972				0.410	0.359	0.458	0.304	0.549	0.322		0.097	0.164	0.202	0.207			0.218	0.617	0.659	0.585	0.215	0.373				0.467	0.542	0.160	0.341		0.398	0.270		0.278	0.266	
10TS% 5L	0.473	0.476	1.100	0.651	0.837	1.800	0.448	0.450	0.438	0.840	0.796	0.854	0.690	0.903	0.788	0.326	0.355	0.396	0.432	0.440	0.270	0.504	0.439	1.060	1.130	1.030	0.472	0.693	0.302	0.198	0.220	0.939	1.010	0.263	0.540	0.502	0.702	0.493		0.396	0.391	
SUCCESSION OF	0.351	1.120	0.639	1.696	0.639	0.447	2.561	2.273	2.369	1.504	1.600	0.447	1.120	0.543	0.159	1.504	0.928	0.735	0.928	0.831	1.312	2.369	0.831	1.024	<0.010	2.080	1.312	1.024	1.408	0.639	0.735	0.351	0.159	0.735	0.639	1.888	1.216	0.063		0.198	0.299	
CEMIN	ы	SCL	1	-	OL	СГ	-		<u>د</u>	C	CL	Ъ	С	CL	сг	-	SCL	CF	SCL	SCL	SL	SL/SCL	1	С	OL	-	4	-	4	-	ų	CL	4	SL	SL	4	٦	٦		4	٦	
TAULAT	30.00	25.00	22.50	25,00	31.25	32,50	26.25	25.00	25.00	27.50	31.25	30.00	28.75	30.00	27.50	25.00	23.75	27.50	26.25	26.25	18.75	20.00	23.75	28,75	28.75	26.25	25.00	26.25	25.00	22.50	22.50	27.50	23.75	15.00	18.75	22.50	21.25	26.25		22.50	22.50	
M SILI	40.00	27.50	37.50	33.75	35.00	32.50	28.75	28.75	28.75	33.75	36.25	35.00	36.25	37.50	35.00	30.00	23.75	30.00	26.25	28.25	25.00	26.25	31.25	38.75	33.75	40.00	33.75	32.50	31.25	28.75	28.75	35.00	33.75	23.75	28.75	30.00	28.75	32.50		30.00	28.75	
N SANU	30.00	47.50	40.00	41.25	33.75	35.00	45.00	46.25	46.25	38.75	32.50	35.00	35.00	32.50	37.50	45.00	52.50	42.50	47.50	47.50	56.25	53.75	45.00	32.50	37.50	33.75	41,25	41.25	43.75	48.75	48.75	37.50	42.50	61.25	52.50	47.50	50.00	41.25		47.50	48.75	
UNC	12.7	30.6	7.72	13.4	18.7	13.9	10.6	11.0	11.2	13.7	12.5	12.5	17.3	17.5	24.7	11.9	14.2	12.9	10.5	9,89	19.1	20.7	17.3	18.6	19.6	21.6	21,3	18.0	19.3	19.1	18.3	16.0	17.7	2.84	3.62	18.1	20.3	0.92	0.93	1,50		
MEQIL	50.5	137	51.3	86.6	91.8	92.2	53.5	52.6	53.7	66.1	59.6	67.9	89.2	99.2	107.0	53.1	59.6	56.5	47.4	44.8	90.9	92.6	82.6	123	111	104.4	88.3	90.0	74.4	74.8	71.8	96.1	108	15.1	20.3	85.3	87.9	5.83	5.87	7,83		
MEQL	12.8	23.0	70.0	62.9	29.9	70.5	30.3	27.0	27.2	27.1	26.8	40.7	33.9	46.7	20.1	20.9	17.2	19.6	24.5	24.2	22.7	20.6	25.2	67.5	43.0	26.9	15.4	29.2	11.8	13.8	13.6	51.7	52.8	34.6	40.1	23.9	28.4	59.5	60.4	28.4		
MEQL	18.7	17.0	18.5	20.3	18.1	17.0	20.2	18.5	18.6	19.2	18.5	18.0	19.3	17.3	17.5	18,9	17.9	18.6	16.2	16.8	22.4	19.4	20.6	19.4	21.2	19.8	19.0	20.7	17.9	16.8	1.71	20.9	21.9	21.7	22.5	20.5	18.3	20.2	19.7	26.1		
INCH	41.1	37.2	38.0	38.8	37.7	35.6	34.9	33,9	33.4	41.2	43.8	39.7	39.7	37.7	35.0	35.3	34.2	41.1	37.9	42.2	36.7	36.8	41.6	45.7	42.2	40.7	42.3	42.3	39.7	34.9	35.6	42.3	38,9	31.5	37.3	36.1	34.4	41.3	40.4	33.1		
EC MMHOUCH	6.64	13.7	8.57	11.0	10.6	12.0	7.60	7.40	7.27	8.22	7.95	9.10	10.7	11.7	11,9	7.48	7.76	7.78	6.93	6.69	11.8	11.7	11.1	17.4	15.1	13.3	11.2	11.5	9.49	9.15	9.50	9.94	15.4	5.39	6.22	11.3	11.9	5.47	5.74	4.70		
PH UNITS	6.03	7.31	5.73	7,06	6.80	5.93	7.55	7.48	7.48	7.45	7.27	6.75	7.05	5.61	6.87	7.37	7.03	7.18	7.15	71.7	61.7	11.1	7.38	5.68	6,65	6,96	7.55	7.06	7.66	7.73	7.68	6.34	6.36	69.9	6.47	7.44	7.34	4.54	4.60	6.19		
DEPTH	0-1	1-3	0-1	1-3	0-1	1-3	6-1	1-3	1-3	5	1-3		1-3	6-1	13	0-1	1-3	0-1	1-3	1.3	-1-0	13	6	1-3	2	1-3	5	1.3	6-1	1-3	1-3	-1-0	1-3	0-1	1.3	0-1	1.3	0-1	61	1-3	1-3	
אשרבב טאוב	5/5/15	5/5/15	5/5/15	5/5/15	5/5/15	5/5/15	5/5/15	5/5/15	5/5/15	5/8/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/8/15	5/6/15	5/8/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	5/6/15	
NOUND	24-2962	24-2962	25-2335	25-2335	25-2367	25-2367	25-2334	25-2334	25-2334	25-2849	25-2849	25-2879	25-2879	25-2908	25-2908	25-2907	25-2907	25-2878	25-2878	25-2878	25-2848	25-2848	25-2333	25-2333	25-2366	25-2366	25-2365	25-2365	25-2332	25-2332	25-2332	25-2847	25-2847	25-2877	25-2877	25-2906	25-2906	26-2720	26-2720	26-2720	26-2720	
-	1505-099-01 24	1505-099-02 24	1505-099-03 25	1505-099-04 25	1505-099-07 25	1505-099-08 25	1505-099-09 25	1505-099-10 25	505-099-10R 25	1505-099-11 25	1505-099-12 25	505-099-13 25	1505-099-14 25	505-099-15 25	505-099-16 26	1505-099-17 25				m				-			505-099-27 25		1		~		1505-099-32 25	1505-099-33 25	505-099-34 25	1505-099-35 25	1505-099-36 25	505-099-39 26		11	1505-099-40R 26	

NAL IN	LOCATION	SAMPLE DATE	SAMPLE	PH UNITS	EC MMHO/CM	% SAT	CALCIUM	MAGNESIUM	SODIUM	SAR	% SAND	% SILT	% CLAY	CLASS	W CACOS	TOT S %	SULFATE 5%	PYR S %	ORG S%	ACID POT TN/1000TN	NEUT POT TN/1000TN	A-B POT TN/1000TM	PYR A POT TN/1000TN	PYRS A-B TN/1000TN
1507-046-15	46-221	7/3/15	0-1	6,90	9,18	53.6	25,3	30.5	66.6	12.6	36.25	30.00	33.75	or	1.289	0.320				10.0	12.9	2.89		
507-046-16	46-221	7/3/15	1-3	7.40	5.48	50.7	26.3	27.1	20.2	3.90	33.75	33.75	32.50	OL	2.083	0.281				8.77	20.8	12.1		
1507-046-25	46-381	7/3/15	0-1	7.52	2.81	43.4	14.5	15.2	7.22	1.87	50.00	25.00	25.00	SCL	0.198	0.215	-0.016	0.114	0.115	6.71	1.98	4.7	3.56	-1.58
1507-046-26	46-381	7/3/15	1-3	7.51	6.09	45.5	19.7	29.4	33.9	6.84	52.50	25.00	22.50	SCL	1,388	0.172				5.39	13.9	8.50		

PYRS A-B TN/1000TN	6.4	11.5			0 22	70'8	8 01	3 82	5.04	10.8	13.7	5.13	-9.61	5.96	15.9	10.6	0,40	4.02			9.05	8,59	8.31		13.1	5.09	8.14	-0.56	2.61	5.92	11.5	0.7	00.4	0 42	S. IA	10.0	-4.37	-7.92	7.00	10.8	19.2
PYR A POT TN/1000TN	4 00	4.56			1 BA	10	6 22	1.44	11.06	12.21	8,28	9.00	16,84	11.12	0,19	6.44	7.81	4.19			4.09	4.34	3.59		3.72	10,78	5.75	7.50	6.31	4.00	4.37	10.1	10'0	2.50	8.75	2	4.37	4.94	3.91	60.7	5.59
A-B POT TN/1000TN	8.42	-2.11	18.9	8 00	01.1	Not	5 0g	-20.5	-15.3	-3.43	-3.91	-5.59	-37.7	-23.0	-5.32	-5.32	-18.2	-13.9	3,95	9.41	-0.41	-0.43	-3.06	5,00	-5.97	-3.68	-1.49	-20.0	-15,6	-10.9	-8.03	88.0-	13.0	84.1-	20.87	1.26	-29.2	-23.6	-7.60	-22.2	-11.3
NEUT POT TN/1000TN	8.21	16.1	27.9	18.1	611	17.1	14 1	5 25	16.1	23.0	22.0	14.1	7.23	17.1	16.1	17.1	8.21	8.21	20.0	17.1	13.1	12.9	11.0	10.01	16.9	15.9	13.9	6.94	8.92	9.92	10.9	0.00	78.6	15.0	13.0	3.96	0.00	-2.98	10.9	17.9	24.8
ACID POT TN/1000TN	16.6	18.2	110	101	15.4	101 8	1 10	25.8	31.4	26.4	25.9	19.7	44.9	40.0	21.4	22.4	26.4	22.1	16.1	7.67	13.6	13.4	15.0	0.01	22.8	19.5	15.4	26.9	24.5	20.8	8.52 9.50	0.00	20.4	4.01	23.8	2.70	29.2	20.6	18.5	40.1	36.1
org s% 1	0 152	0.141			0 135	0.100	0 184	0.100	0.203	0.218	0.214	0.177	0.376	0.316	0.204	0.230	0.220	0.152			0.148	0.134	0.170		0.254	0.144	0,146	0.206	0.183	0.246	0.230	0.467	101.0	0 222	0 238		0.265	0.229	0.242	0.245	0.262
PYR S % 0	0.128	0.146			0.050	0.000	0 167	0.046	0.354	0.391	0.265	0.288	0.539	0.356	0.006	0.206	0.250	0.134			0.131	0.139	0.115		0.119	0.345	0.184	0.240	0.202	0.128	0.140	0.170	0/1/0	0.246	0.284		0.140	0.158	0.125	0.227	0.179
SULFATE S% P1	0.754	0.296			0 20R	004.0	0.324	0.678	0.448	0.236	0.350	0.166	0.522	0.610	0.476	0,282	0.375	0.422			0.155	0.155	0.194		0.359	0.137	0.163	0.416	0.398	0.292	0.360	200.0	080.0	0 301	0.258		0.529	0.272	0.226	0.812	0.660
TOTS% SULF	0.533	0.583	0.352	0 322	0 402	0 110	0.675	0.824	1.004	0.846	0.830	0.631	1.437	1.282	0.686	0.717	0.845	0.708	0.515	0.245	0.434	0.428	0.479	0.300	0.731	0.626	0.492	0.862	0.784	0.666	0.762	0.733	2010	0.738	0.760	0.087	0.933	0.659	0.593	1.283	1.156
% CACO3 TO	0.821	1.610	29792	1 807	1 117	1 708	1.412	0.525	1.610	2.299	2.201	1.412	0.723	1.708	1.610	1.708	0.821			1.708	1.314	1.293	1,190	1 686							100.1				1 388				1.091	1.785	2.480
CLASS % C																																					v	v			
% CLAY OL	31 25 CI	31.25 CL	31 25 CI	30 00 CI	31 25 01	25.00 1	31 25 CI	31.25 CL	27.70 CL	27.50 CL	28.75 CL	30,00 CL	26.25 L	25.00 L	25.00 L	23.75 L	23.75 SCL	27.50 CL	22.50 SCL	18.75 SL	26.25 SCL	25.00 SCL	28.75 CL	25.00 1	28.75 CL	27.50 CL	26.25 SCL	31.25 CL	31,25 CL	25.00 L	23./D SUL	24 DE DI	33 7E CI	30 ED CL	32 50 01	27.50 CL	27.50 CL	26.25 L	20.00 SL/SCL	31.25 CL	27 50 CL/SCI
% SILT % G	28.75	30.00	31 25								31.25						23.75						28.75											35.00							27 50
% SAND	40.00	38.75	37.50	36.25	35 00	41.25	33 75				40.00														35.00		47.50			43.75											45 00
	13.8						17.2													8.29					17.6												ĥ		7	ĺ.	
UM SAR	70.5	87.0	110	134	88.3	20.0	926	113	72.6	86.6	90.9	62.2	92.2	30.5	91.3	61.3	100	80.9	63.9	30.5	74.8	75.3									0.40								38.5		01 B
L MEQL	28.0	27.3	22.2	24.6	27.6	2 94	31.5	21.3	39,6	34,6	36.4	25.7	31.2	63.8							23.7	23.0									0.42										0 67
M MAGNESIUM MEQ/L	24.6													22.4								19.7									23.0		1.00			21.7					24.3
GALGIUM	61.0 2							51.2 2								47.1 2						4.00									40.Z 2.04										
W SAT	9.64 6				11 2 49				10.3 49		11.2 46	9.26 48	11.3 50									10.8 55		140																	45.4
EC MMHO/CM			7.90 12																																						8 12.1
H PH UNITS	7.42	2	2.5	79.7	1		1.7	7.6	1.1	1.7	7.72	7.47	7.0	6.95	7.04	7.2	6.60		7.60	7.37	7.61	96.7	8L.1 9D.7	763	1	7.50	2.6	6.80	6.98	1.19	11.1	111	24.7	1. L	7.43	6.56	5.17	4.29	6.73	6.86	7.18
SAMPLE DEPTH	0-1	1.3	0-1	57	0-1	5		1-3	0-1	1.3	1-3	0-1	1-3	0-1	1-3	5	1-3	6-1	1-3	6-1	?	7 2	1-0	2.5	2	0-1	1-3	5	2.0	5	2 4	24	5 -	2 2	1	0-1	1-3	0-1	1-3	0-1	- 20
SAMPLE DATE	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	GL/S/12	113115	713/45	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	113/15	110112	212145	212145	713/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15	7/3/15
LOCATION	25-2557	5			Ċ					0		26-2590	26-2590	26-2628	26-2628	26-2629 7							7807-97			26-2552 7					CCC2-07						26-2517 7	3	25-2518 7		25-2519 7
2												1																			٥										
BAL #	1507 047-01	1508 047-02	1509 047-03	1510 047-04	1511 047-05	1512 047-06	1513 047-07	1514 047-08	1515 047-09	1516 047-10	1517 047-10R	1518 047-11	1519 047-12	1520 047-13	1521 047-14	1522 047-15	1523 047-16	1524 047-17	1525 047-18	1526 047-19	1527 047-20	1528 04/-20R	15-140 0521	1531 047-23	1532 047-24	1533 047-25	1534 047-26	1507-047-27	1507-047-28	1507-047-29	1507-047-30P	1507-047-34	10-140-1001	1507-047-33	1507-047-34	1607-047-35	1507-047-36	1507-047-37	1507-047-38	1507-047-39	1507-047-40

TN/1000TN TN/1000TN						5.75 -34.3 5.75 -11.0 0.03 -5.32 12.4 -12.7
A-B POT PY IN/1000TN TN	-5.7	CCP	7.7	-61.1	-61.1 -54.1	-61.1 -54.1 -54.1
						-5.3 -5.29 -0.33
TN/1000TN						
ACID POT TN/10001/NT						55.9 48.8 53.7
WS BHO	0.27	0.34		0.53	0,53	0.53 0.52 0.55
PYR S %	0.44	1.80		0.18	0.18	0.18 0.00 0.40
SULFATE 5%	0.40	<0.010		1.08	1.08	1.08 1.04 0.77
707.5%	1.11	2.05		1.79	1.79	1.79 1.56 1.72
% CACO3	2.89	2.19		<0.010	<0.010	<0.010 <0.010 <0.010
CLASS	CL	CL		-	r SCL	scr scr
% CLAY	30.00	28.75		23.75	23.75 25.00	23.75 25.00 30.00
% SILT	27.50	33.75		31.25	31.25 25.00	31.25 25.00 20.00
% SAND	42.50	37.50		45.00	45.00	45.00 50.00 50.00
SAR	8.29	22.9		2.27	2.27	2.27 2.70 12.3
SODIUM MEQIL	42.8	99.2		23.4	23.4	23.4 27.2 74.4
MEQU	28.8	16.9		191	191	191 179 56.4
CALCIUM	24.6	20.7		21,5	21,5 24.0	21,5 24.0 17.2
% SAT	45.8	44.7		34.8	34.8 31.9	34.8 31.9 39.9
EC MMHOICM	7.49	12.5		15.0	15.0 14.6	15.0 14.6 10.8
PH UNITS	7.35	6.65		3.93	3.93 4.63	3.93 4.63 4.42
DEPTH	0-1	1.3		0-1	1-9-1- 1-1-1-	242
SAMPLE DATE	10/27/15	10/27/15		10/27/15	10/27/15	10/27/15 10/27/15 10/26/15
LOCATION	26-4681	26-4681		26-4715	26-4715 26-4715	26-4715 26-4715 56-2844
GAL#	510 298-03	1510 298-04			1510 298-05	

2015-5

PYRS A-B TN/1000TN	6.52	4.44						-3.55	-2.39		9.55	-0.58	0,83		10.83			4.22	5.90	11.08	15,48
PYR A POT TN/1000TN	1.72	1.81						6.81	5,65		3.37	2.66	3.06		2.09			6.00	4.31	3.66	0.16
A-B POT TN/1000TN	-5.56	-8.06	8.19	3.14	2.53	1.31	11.6	-29.0	-30.1	8.97	-7.76	-26.0	-40.9	0.08	-0.32	13.7	41.4	-23.7	-26.6	-13.8	-7.88
NEUT POT TN/1000TN	8.24	6.25	18.2	15.2	14.2	8.24	14.2	3.26	3.26	20.2	12.9	2.08	3.89	12.0	12.9	22.9	49.4	10.2	10.2	14.7	15.6
ACID POT TN/1000TN	13.8	14.3	10.0	12.1	11.7	6.94	2.62	32.2	33.3	11.2	20.7	28.1	44.8	11.9	13.3	9.16	7.98	34.0	36.8	28,6	23.5
ORG S%	0.14	0,16						0.32	0:30		0.21	0.31	0.44		0.11			0.33	0.36	0.26	0.27
PYR S%	0.06	0.06						0.22	0.18		0.11	0.09	0.10		0.07			0.19	0.14	0.12	0.01
SULFATE S%	0.24	0.24						0.50	0.59		0.34	0.50	0.89		0.25			0.57	0.69	0.54	0.48
TOT 5 %	0.44	0.46	0.32	0,39	0.37	0,22	0.08	1.03	1.07	0.36	0.66	06.0	1.43	0.38	0.42	0.29	0.26	1.09	1.18	0.91	0.75
% CAGO3	0.82	0.62	1,82	1,52	1.42	0.82	1,42	0.33	0.33	2.02	1.29	0.21	0.39	1.20	1.29	2.29	4.94	1.02	1.02	1.47	1.56
CLASS	0	0	0	0	0	CL	SCL	CL	CL	CL	CL	0	CL	SCL	SCL	CL	CL	CL	CL	CL	CL
% CLAY	42.50	42.50	51.25	51.25	50.00	30.00	26.25	35.00	33.75	38,75	33.75	43.75	32.50	26.25	26.25	32.50	31.25	37.50	37.50	33.75	36.25
% SILT	28.75	27.50	21.25	21.25	21.25	42.50	16.25	30.00	28.75	31.25	30.00	27.50	25.00	26.25	26.25	27.50	25.00	32.50	32.50	27.50	27.50
% SAND	28.75	30.00	27.50	27.50	28.75	27.50	57.50	35.00	37.50	30.00	36.25	28.75	42.50	47.50	47.50	40.00	43.75	30.00	30.00	38.75	36.25
SAR	16.3	16.0	16.8	15.3	15.3	5.60	4.63	8.86	8.74	18.8	15,5	10.8	2.74	8.53	11.2	14.1	7.43	11.9	10.3	12.1	15.6
SODIUM	73.5	69.69	61.8	58.7	58.7	27.8	19.6	51.3	59.6	88.3	74.8	67.9	26.3	38.1	52.2	55.7	30.1	67.4	55.7	62.2	79.2
MAGNESIUM	22.3	19.8	11.3	11.9	11.8	28.8	19.9	50.0	75.9	20.2	26.5	59.2	165	23.7	25.2	13.0	15.5	46.4	43.4	36.9	34.1
CALGIUM	18.6	18.1	15.7	17.71	17.8	20.4	15.8	121	17.1	23.9	20.3	19.7	19.9	16.3	18,0	18.1	17.3	18.1	14.5	16.4	17.4
% SAT	49.7	50.5	50.0	51.0	52.1	34.9	34.2	39.9	37.1	48.6	42.5	53.0	44.2	36.8	37.5	40.4	36.7	44.5	42.0	46.0	47.0
EC MMHO/CM	9.90	9.47	8.02	7.29	7.49	5.63	4.22	8.53	10.5	8.47	8.26	9.39	9.16	5.33	6.86	6.63	4.70	8.52	7.61	7.93	9.08
STINU H4	7.46	7.51	7.78	7.66	7.63	7.59	7.92	6.24	5.99	16.7	7.18	4,96	4.15	7.16	7.23	7.83	7.84	6.37	6.42	6.82	7.12
SAMPLE	1-0	1-3	0-1	1-3	ς. τ	6-1	1-3	0-1	1-3	0-1	e7-	0-1	1.3	0-1	1-3	0-1	1-3	0-1	1-3	0-1	1-3
SAMPLE DATE	1/20/16	1/20/16	1/20/16	1/20/16	1/20/16	1/20/16	1/20/16	1/20/16	1/20/16	1/20/16	1/20/16	1/20/16	1/20/16	1/20/16	1/20/16	1/20/16	1/20/16	1/21/16	1/21/16	1/21/16	1/21/16
LOCATION	57-2867	57-2867	57-2864	57-2864	57-2864	57-2862	57-2862	56-2918	56-2918	57-2994	57-2994	57-2865	57-2865	62-2950	62-2950	57-2996	57-2996	56-2820	56-2820	59-2829	59-2829
GAL#	1601169-33	1601169-34	1601169-49	1601169-50	1601169-50R	1601169-51	1601169-52	1601169-55	1601169-56	1601169-67	1601169-68	1601169-73	1601169-74	1601169-75	1601169-76	1601169-77	1601169-78	601169-83	601169-84	601169-87	601169-88

PYR S % OR	0.019 0.307 26.2	0.133 0.164 28.7	0.111 0.290 27.9	0.098 0.287 24.4	0.077 0.169 17.6	0.044 0.105 10.8	0.138 0.308 27.0	0.032 0.125 23.5	17.6		11,1	0.419 0.275 26.5	0.417 0.286 26.4	0.461 0.298 26.9	0.154 0.174 16.4	0.230 0.297 24.6	0.441 0.329 38.4	0.369 0.206 27.9	0.145 0.262 20.2	0.220 0.204 18.1	20.1	0.226 0.267 17.9	0.068 0.154 10.3		23.1	0.215 0.252 24.9			17.5	0.187 0.319 24.5	0,152	0,066 0.225 19.4	0.047 0.133 14.4	0.019	0.009 0.324 36.5	0.044 0.213 21.1	0.145
% CACO3 TOT S% SULFATE S%	0.838	0.919	0.894	0.782	0.565	0.347	0,866		0.563		0.355		0,846	0,860	0.526	0.788	1.230	0.894	0.645	0.579	0.643		0.328		0.738	1.68 0.798 0.331			0.560	0.785	0.753	0.620	0.83 0.462 0.282	0.785	1.167	0.677	1.124
T % CLAY CLASS	35.00	33.75	33.75	31.25	27.50	26.25	42.50	43.75	33.75	50.00	51.25	27.50	28.75	32.50	38.75	36.25	36.25	35.00	28.75	27.50	22.50	25.00	26.25	33.75	26.25	26.25	31.25	27.50	27.50	32.50	33.75	31.25	5 27.50 SCL	26.25	30,00		1 25.00 SCL
SAR % SAND % SILT	1.49 35.00 30.00	38.75	33,75	35.00	45.00	50.00	18.75	16.25	40.00	13.75	13.75		46.25	41.25	30.00	33.75	31.25	40.00	51.25	52.50		55.00	52.50	38,75	48.75	50.00	42,50		48.75	45.00	41.25	42.50	48.75		42.50		
CALCIUM MAGNESIUM SODIUM MEQIL MEQIL MEQIL	60.8	83.9	60.4	73.1	22.2 55.2 9.79	43.0		89.7	22.9	72.6	72.2	8.80	18.9 9.71 61.3	8.97	22.5	34.1		42.2	15.1	18.8	18.3 20.5 24.5	16.1	16,4	19.6	24.1		31.9	31.2		22.6	27.1	32.7	21.8 49.4 66.6	57.8	111	46.6	24.1 89.7 39.5
EC MMHO/CM % SAT						4.98 35.1				5.85 54.7		7.19 40.5				1		9,58 38.6			5.08 37.4		5.75 36.8														8.18 43.5
DATE SAMPLE PH UNITS	0-1		0-1	13	0-1	ۍ ا	0-1	1-3	0-1	1-3	1-3	Ū	1	1-3		13	6-1		0-1	13		1.3		1.3	0-1	13		1-3		0-1	1-3	5	4.3		4-3	0-1	3 1-3 4.09
LOCATION SA	24-4323	24-4323	24-4287	1604-089-04 24-4287 4/6/16	1604-089-05 24-4321 4/6/16	1604-089-06 24-4321 4/6/16	1604-089-07 24-4322 4/6/16	1604-089-08 24-4322 4/6/16	1604-089-09 24-3493 4/6/16	24-3493	24-3493	25-4535	25-4535	25-4535	25-4375	25-4375	25-4342	25-4342	25-4902	25-4902	25-4932	25-4932	24-4989	24-4989	24-5017	24-5017	24-5044	24-5044	3 24-5044	24-5018	24-5018	24-4990	24-4990	24-4286	24-4286	24-3494	 1604-089-48 24-3494 4/7/16

PYRS A-B TN/1000TN			9.65	4.43	4.13	1.66	0.90	-5,19	-4.19	5.61	1.40	1.98	2.86	7.97		-38.8	-36.1	8.78	121
PVR A POT TN/1000TN			1.00	1.59	3.75	6.22	5.12	3.81	5.59	5.97	7.40	9.59	5.94	11.9		43.0	47.6	8.34	42.0
A-B POT TN/1000TN	3.16	12.6	-0.01	-13.2	-8.68	-11.6	-15.3	-36.9	-43.8	-6.07	-6.28	-13.2	-18,8	-21.7	1.81	-59.0	-49.7	-5.29	10.6
NEUT POT TN/1000TN	5.10	14.4	10.7	6.03	7.88	7.88	6.03	-1.38	1.40	11.6	8.80	11.6	8.80	19.9	26.4	4,18	11.6	17.1	175
ACID POT TNU 1000TN	1.94	1.80	10.7	19.2	16.6	19.5	21.3	35.5	45.2	17.6	15.1	24.7	27.6	41.6	24.6	63.1	61.3	22.4	100
ORG S%			0.220	0.181	0.292	0.340	0.410	0.402	0'370	0.289	0.146	0.252	0.423	0.304		0.764	0.756	0.499	0 346
PYR S %			0.032	0.051	0.120	0.199	0.164	0.122	0.179	0.191	0.237	0.307	0.190	0.382		1.377	1.525	0.267	0 538
SULFATE S%			0.089	0.384	0.119	0.085	0.109	0.612	0.897	0.086	0.099	0.233	0.269	0.646		-0.120	-0.318	-0.048	0 145
TOT S % SI	0.06	0.06	0.34	0.62	0.53	0.62	0.68	1.14	1.45	0.56	0.48	0.79	0.88	1.33	0.79	2.02	1.96	0.72	1 03
% CAGO3	0.51	1.44	1.07	0.60	0.79	0.79	0.60	<0.010	0.14	1.16	0.88	1.16	0.88	1.99	2.64	0.42	1.16	1.71	1 25
CLASS	SL	SL	СГ	CL	СL	CL	CL	CL	CL	С	СL	СL	CL	СГ	СL	CL	SCL	С	ī
% CLAY	6.25	18.75	35.00	33.75	28.75	27.50	27.50	36.25	31.25	37.50	36.25	32.50	33.75	32.50	31.25	28.75	28.75	37.50	36.35
% SILT	25.00	21.25	31.25	31.25	27.50	28.75	28.75	27.50	32.50	23.75	23.75	31.25	27.50	26.25	26.25	30.00	25.00	36.25	35.00
% SAND	68.75	60.00	33.75	35.00	43.75	43.75	43.75	36.25	36.25	38.75	40.00	36.25	38.75	41.25	42.50	41.25	46.25	26.25	28 7K
SAR	1.74	0.73	4.57	2.77	11.4	10.3	9.92	5.84	8.70	18.7	16.2	8.80	16.9	20.2	19.4	17.6	16.9	15.8	17.6
NEQL	6.48	1.48	21.7	13.8	48.7	48.7	44.8	40.0	79.2	81.8	61.8	43.5	73.5	140	87.0	102	77.4	72.6	82 6
MAGNESIUM	6.70	1.58	24.1	30.8	18.0	25.3	23.0	76.4	149	18.8	13.8	30.7	22.0	81.2	24.0	51.4	24.1	24.8	26.3
GALCIUM	21.0	6.74	20.9	18.9	18.8	19.8	17.9	17.3	16.9	19.6	15.3	18.2	15.7	14.7	16.3	15.5	18.1	17.2	181
% SAT	28.1	34.8	40.8	38.5	39.9	37.6	36.0	35.2	35.8	41.9	43.3	35.4	38.6	42.8	31.9	39.1	36.9	42.3	105
EC MMHO/CM	3.20	1.32	5.50	5.01	7.44	77.7	7.31	8.99	13.8	10.3	8.24	7.46	9.52	15.9	10.6	12.7	9.92	9.62	10.3
PH UNITS	7.48	7.72	7.39	6.48	6.92	6.60	6.55	4.37	4.25	2.06	7.21	6.73	6.87	6.07	6.94	5.30	6.17	7.05	6 83
SAMPLE	0-1	1-3	5-	1-3	0-1	1-3	1-3	0-1	1.3	5	1-3	0-1	1-3	0-1	2	0-1	1-3	0-1	ert
SAMPLE DATE	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16	6/16/16
LOCATION	3058	3058	3075	3075	3076	3076	3076	4533	4533	4570	4570	4609	4609	4606	4606	4605	4605	4643	5PA2
GAL#	1606-237-35	1606-237-36	1606-237-37	1606-237-38	1606-237-39	1606-237-40	606-237-40R	1606-237-41	1606-237-42	1606-237-43	1606-237-44	1606-237-45	1606-237-46	1606-237-47	1606-237-48	1606-237-51	1606-237-52	1606-237-53	BUG-237-54

PYRS A-B TN/1000TN			-13.1	-8.32	
TU/1000TN			10.9	3.41	
A-B POT TN/1000TN	13.2	1.18	-28.1	-59.1	
NEUT POT	30.1	23.7	-2.15	-4.91	
ACID POT TN/1000TN	16.9	22.5	26.0	54.2	
ORG 5%			0.432	0.466	
PYR 5 %			0.349	0.109	
SULFATE 5%			0.051	1.159	
TOT 5 % 5	0.541	0.720	0.832	1.73	
% CAGOS	3.01	2.37	<0.001	<0.001	
CLASS	CL	CL	G	SCL	
% CLAY	30.00	30.00	35.00	27.50	
% SILT	27.50	28.75	26.25	22.50	
% SAND	42.50	41.25	38.75	50.00	
SAR	13.1	12.4	19.1	3.19	
SODIUM MEQ/L	57.0	57.0	94.0	21,9	
MAGNESIUM	19.4	24.4	30.7	74.0	
CALCIUM	18.4	18.2	17.6	20.3	
% SAT	40.3	42.7	42.6	45.5	
EC MMHO/CM	6.98	7.29	96'6	7.25	
PH UNITS	7.50	7.41	5.77	3.37	
DEPTH	0-1	1-3	0-1	1-3	
SAMPLE DATE	8/12/16	8/12/16	8/12/16	8/12/16	
LOCATION S	N9 4536	N9 4536	N9 4569	N9 4569	
gAL #	1608-155-11	-	1608-155-15 1	1608-155-16	

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EC MMHO/CM % SAT	% SAT	CALCIUM	MAGNESIUM MEQ/L	SODIUM	SAR	% SAND	% SILT	% CLAY	CLASS	% CACO3	TOTS% S	ULFATE S%	PYR S %	ORG 5%	ACID POT TN/1000TN	TW/1000TN	A-B POT TN/1000TN	PYR A POT TN/1000TN	PYRS A-B TN/1000TN
	20.3		18.3	90.9	20.7	50.00	21.25	28,75	SCL	0.96	0.48	00.0	0.16	0.36	14.9	9.56	-5.4	4.97	4.6
	20.6		16.0	115	27.0	42.50	22.50	35,00	СГ	0.56	0.63	0.00	0.17	0.58	19.7	5.57	-14.2	5.40	0.1
	21.2		23.3	58.7	12.5	50,00	23.75	26.25	SCL	3.35	0.39				12.2	33.5	21.4		
	18.4		20,0	60.5	13.8	31.25	35.00	33.75	С	2.87	0.74				23.2	28.7	5,51		
	19.4		17.0	56.5	13.3	60.00	17.50	22.50	SCL	1.04	0.40	0.11	0.05	0.24	12.5	10.4	-2.13	1.50	8.86
	20.6		20.0	46.1	10.2	57.50	17.50	25.00	SCL	0.96	0.28				8.8	9.56	0.72		
	19.4		17.9	79.2	18.4	63.75	16.25	20.00	SL/SCL	0.80	0.48	0.14	0.06	0.28	14.9	7.97	-6.91	1.94	6.0
40,4 19,4	19.4		22.5	88.7	19.4	55.00	21.25	23.75	SCL	1.12	0.73	0.17	0.16	0.41	22.8	11.16	-11.7	*	6.32
	21.2		26.1	27.9	5.74	45.00	26.25	28,75	CL/SCL	0.72	0.41	0.10	0.07	0.24	12.7	24.7	-5,51	2.09	5.0
20.5			25.8	54.4	11.3	56.25	21 25	22 50	NOS.	0.88	0.59	0.21	0.14	0.24	18.5	8.76	-9.78	4	4.3

PYRS A-B TN/1000TN		0.35	-0.02	9.03	2.69	-0.30	2.48	1 86	20 V	0 t t	0.10	2.09	-0.46	0.53	1.58	8,15	3.06	-2,90	-15.8	-2.03	2/15	1.87	-3.81	-2.30	-7.74	-4,16	-1.04	5.26	-1,06	-4.53	0.19	-2.87	-2.41	-1.49	0.11.		4 0 50 7	0.0	4,40	De.I	6 V F	10.0	0.61	12.8		-4.22	-0.40	15.1		1.25	8.76	5.07	3.26	5.49	-1.21	-1.78	-2.02	-3.27	-1.35	10.1	0,80	
PYR A POT TN/1000TN		3.62	<0.01	0.53	1.28	3.47	3.09	0.50	0.70	21.0	10.05	0.28	0.44	0.25	<0'01	2.39	0.89	0.26	<0.01	3.16	1.81	2.08	4.94	5.31	6.04	1.52	2.17	1.51	1.25	4.72	<0.01	3.06	3.54	3.56	15.8		10.02	10.02	0.43	1 13	2004	0.04	0.91	0.63		3.59	1.65	3.09		<0.01	<0.01	2.75	3.63	2.33	1.52	1,15	1.39	22.0	0.72	19.0	<0.U1	
A-B POT TN/1000TN	2,46	20.0	10.5	-12.4	-24.5	-21.3	-17.0	16.0	24.4	4. 0. 00	2	-36.8	-29.6	-37.9	-37.9	-15.8	-19.1	-26.9	-65.6	-27.5	-22.1	-21.4	-25.5	-20.3	-46.9	-44.7	-20.5	-13.6	-23.4	-26.5	-38.3	-37.4	-34.4	-27.2	-28.4	1.6.0	19.4	7.11-	14.4	800	0.04	12.0	-12.5	-8.45	60.0	-35.6	-32.2	-9.43	2.60	-30.4	-0.45	-24.3	+17.4	-17.2	-28.8	-56.3	-27.5	-38.1	-30.6	-35.8	-8.63	
NEUT POT TN/1000TN	16.0	3.97	-0.02	9.56	3.97	3.17	5.57	10.4	1 1 1	10.0	11.0	2.37	-0.02	0.78	1.58	10.5	3.95	-2.64	-15,8	1.13	3.95	3.95	1.13	3.01	-1.70	-2.64	1.13	6.78	0.19	0.19	0.19	0,19	1.13	2.07	CR.5	13.4	9.04	10.0	4.03	3.95	00.0		20.0	13.5	65.4	-0.63	1,25	18.1	21.9	1.25	8.76	7.82	6.88	7.82	0.31	-0.63	-0.63	-2.50	-0.63	-0.63	5.45	
ACID POT TN/1000TN	13.5	23.8	125	22.0	28.5	24.5	225	26.3	97.0	0.10		39.2	29.6	38.7	39.5	26.3	23.1	24.3	49.8	28.7	26.1	25.3	26.6	23.3	45.2	42.1	21.6	20.4	23.6	26.7	38.5	37,6	35.6	29.3	32.4	0.71	23.3	10.4	1.91	24.6	0.14	31.0	32.5	21.9	5,41	35.0	33.5	27.6	19.3	31.7	9.22	32.1	24.3	25.0	29.1	55.6	26.8	35.6	30.0	35.2	14.0	
ORG S%		0.27	12.0	0.26	0.24	0.25	0.29	0.20	0.24	40.0	2 2 0	0.52	0.33	0.46	0.62	0.18	0.27	0.05	0.04	0.34	0.34	0.32	0.34	0,41	0.63	0.54	0.27	0.21	0.22	0.28	0.30	0.26	0.29	0.36	0.36	0.00	70.0	0.40	0.10	0.03	0.00	0.33	0.33	0.21		0.47	0,44	0.24		0.43	0.21	D.43	0.43	0.41	0.28	0.61	0.33	0.42	0.28	97.0	0.16	
PVR 5 %		0.12	<0.01	0.02	0.04	0.11	0.10	0.08	000	20.0	10.02	10.0	0.01	0.01	<0.01	0.08	0.03	0.01	<0.01	0,10	0,06	0.07	0,16	0.17	0.19	0.05	0.07	0.05	0.04	0.15	<0.01	0.10	0.11	0.11	000		10.02	10.04	10.0	000	100	000	0.03	0.02		0.11	0.05	0.10		<0.01	<0.01	0.09	0.12	10.0	0.05	0.04	0.04	0.02	0.02	0.03	<0.0>	
SULFATE 5%		0.38	0.16	0.43	0.63	0.42	0.33	0.56	0000	20.0	0/.0	0./3	0.60	0.77	0.89	0.58	0.44	0.72	1,55	0.48	0.44	0.42	0.36	0.17	0.62	0.76	0.35	0.40	0.49	0.43	0.94	0.84	0.73	0.46	11.0	100	17.0	44.0	14.0	0.50	180	0.66	0.68	0.47		0.54	0.57	0.54		0.66	0.12	0.51	0.23	0.32	0.60	1.13	0.49	0.69	0.66	0.82	0.33	
TOTS% SU	0.43	0.76	0.40	0.70	0.91	0.78	0.72	0.84	4 1 4	0.4	1.12	1.25	0.95	1.24	1.26	0.84	0.74	0.78	1.60	0,92	0.84	0.81	0.85	0.75	1.45	1.35	0,69	0.65	0.76	0.86	1.23	1.20	1.14	0.94	1.04	0.40	0.65	0.00	10.0	0.79	P B C	66.0	1.04	0.70	0.17	1.12	1.07	0.88	0.62	1.01	0.30	1.03	0.78	0.80	0,93	1.78	0.86	1.14	0,96	1.13	0.47	
% CAGO3	1.595	0.397	<0.001	0.956	0.397	0.317	0.557	1 036	0.667	100.0	110.0	0.23/	<0.001	0.078	0.158	1.064	0.395	<0.001	<0.001	0,113	0.395	0.395	0.113	0.301	<0.001	<0.001	0.113	0.678	0.019	0.019	0.019	0.019	0.113	0.207	0.385	1.33/	0.301	10000	0.408	0.395	1 424	1061	1.995	1.346	6.540	<0.001	0.125	1.815	2.190	0.125	0.876	0.782	0.688	0.782	0.031	<0.001	<0.001	<0.001	<0.001	<0.001	0.595	
CLASS	SCL	SCI	SL/SCL	SCL	-	С	CL	100	100		г.		SCL	-	ċ	SCL	SCL	SL	SL	сL	С	сГ	SCL	CL	SCL	SCL	CL	CL	SCL	SCL	SCL	SCL	SCL	56	CL.	U.S.C.	200	3 0	3 0	3 0	20	SCI	SCL	SCL	SL	L	L	SL/SCL	SL	SCL	SCL	CL/SCL	SCL	CL/SCL	-	- 1	SCL	SCL	ъ СГ	5	SUL	
% CLAY	30.00																																																													
% SILT	20.00	26.25	22.50	17.50	28.75	28.75	31.25	22.50	34.95	27.00	20.02	31.25	20.00	28.75	30.00	26.25	23.75	16.25	27.50	28,75	26.25	25.00	23,75	26.25	26.25	21.25	27.50	26.25	22.50	22.50	22.50	25.00	23.75	23.75	07.07	23.73	32 50	07.50	07 50	30.00	25,00	23.75	22.50	26.25	23.75	32.50	30.00	27,50	26.25	22.50	23.75	26.25	22,50	25,00	28.75	28.75	25.00	23.75	31.25	28.75	25.00	
% SAND	50.00	46.25	57.50	58.75	50.00	41.25	40.00	55.00	57 ED	20.00	10.60	45.00	56.25	45.00	43.75	48.75	48.75	73.75	56.25	40.00	40.00	41.25	50,00	43.75	51.25	56.25	38.75	41.25	46.25	52.50	51.25	50.00	50.00	42.50	00.75	45.00	32.50	20.75	37 50	32 50	46.25	50.00	61.25	52.50	58.75	45.00	43.75	52.50	56.25	52.50	52.50	45.00	47.50	45.00	51.25	47.50	47.50	55.00	40.00	43.75	52.50	12.2
SAR	8.28	3.67	1.35	2.99	4.30	9.71	8.59	203	1 44		07.1	1.18	2.35	0.88	0.93	3,11	5.16	6.19	11,19	8.10	9.30	9.36	5.31	6.15	1.10	1.27	2.40	2.83	4.18	3.91	4.20	4.34	4.38	197	8.09	4.40	1 22	77.1	07.1	141	1 26	1 23	121	2.27	1,43	1.16	1.31	1.24	1.19	2.75	1.70	13.1	11.2	11.0	2.30	1.52	4.26	4.92	3.21	1.46	1.50	
SODIUM	42.5	20.9	5.87	20.6	32.5	50.9	45.2	18.4	205	200	0.01	811	1.71	7.96	8.74	17.1	33.2	48.3	114	40.1	47.0	47.4	31.0	35.1	11.0	13.7	13.7	14.8	22.6	19.5	35.8	35.8	36.6	38.0	41.4	40.4	0.04	10.1	7.00	7 44	00 8	7.74	7,53	12.1	6.31	60'6	10.0	7.48	6.61	15.7	8.31	64.8	48.7	47.0	19.4	13.0	28.1	47.0	23.4	5.11	9.00	
MAGNESIUM MEQL	29.8	43.0	11.9	72.9	93.8	35.8	35.5	106	107	1.01	0	9/1	92.1	145	158	37.8	64.4	99.5	181.8	32.3	32.0	31.8	50.2	47.7	184	215	46.1	30.9	40.2	31.6	127	119	122	6.15	01.0	1.02	1.01	26.6	0.00	32.0	40.6	45.5	44.6	29.7	11.7	104	96.3	42.9	29,9	46.7	25.3	34.6	21.3	20.8	118	122	69.4	161	88.9	1.16	50.6	
CALCIUM N MEQU	22.9	22.0	25.9	21.9	20.7	19.2	20.0	25.0	300	P. 4 4 C	1.12	7.77	20.5	19.6	20.1	22.7	18.2	22.2	25.7	16.8	19.0	19.5	18.0	17.5	17.71	20.4	18.9	24.1	18.2	18.0	18.5	17.0	17.8	9.71	4.11	20.2	20.8	0.04	25.1	23.4	41.2	33.4	32.9	26.9	27.5	17.8	20.0	30.2	31.4	19.1	22.5	14.7	16.8	15.7	22.9	24.8	17.1	21.2	17.7	18.5	8.12	
% SAT	47.1	45.8	51.1	43.3	40.8	42.2	48.5	42.0	0.95	44.0	0.00	38.0	43.0	47.6	44.3	39.3	37.9	34.7	35.6	46.1	48.8	49.6	40.6	44.3	35.4	35.0	45.7	46.2	44.1	41.1	37.6	34.1	34.4	48.2	41.1	40.04	4.40	1.04	46.4	48.3	414	42.3	42.7	37.9	30.3	41.8	43.7	38.0	35,4	45.5	44.3	48.4	56.1	54.3	37.4	38.2	44.1	39.4	45.0	50.0	43.8	
EC MMHO/CM	6.06	4.83	2.82	6.04	7.31	6.47	6.15	6.59	20.0	20.0	10.1	1.63	6.39	6.91	7.37	4.79	6.73	14.0	20.6	5.74	6.28	6.32	5.08	5.24	6.77	7.35	4.17	3.84	4.49	3.87	7.45	7.13	7.16	5.25	10.0	0.04	A DR	200.4	3 70	3.69	5.45	5.03	5.00	4.77	3.40	7.50	7.45	5.82	5,12	5.49	4.02	8.40	6.63	6.44	8.84	8.68	6.94	10.2	7.62	1.08	17.9	
PH UNITS E	7.16	5.38	4.13	4.89	4.99	5.23	5.30	5.55	5 70		Do 4	4.08	4.80	4.61	4.57	7.07	6.47	4.02	2.65	5.62	6.22	6.35	5.24	5.49	4,04	3.98	5.15	6.42	4.71	4.63	5.13	4.92	4.93	JR.C	0.40	0.00	6.47	de s	5.63	808	5 86	6.64	6.79	7.01	7.37	4.80	4.87	6.77	2,05	5.01	6.84	6.77	6.61	6.60	5.40	4.67	4.79	4.08	4.60	444	5.64	
SAMPLE	0-1	2 3	7	1-0	4°	0-1	5-1	0-1		2 0	2 2	5 :	2	6-1	-1-	0-1	e	6-1	5	1-0	1-3	1-3	1-0		0-1	1-3	6-1	1.3	0-1	1-3		5		5	2 2	3 *	22	5	2 2	5	2.5	5	5	0-1	6.4	6-1	1.3	0-1	1-3	0-1	1-3	0-1	1.3	67 - 1	5	1-3	5-0-1	1-3	1-0	? ·	5-	
SAMPLE DATE	11/9/16	11/9/18	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/0/16	11/01/0	01/0/11	OL/R/LL	91/6/11	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	9L/A/LL	01/8/11	01/8/11	01/8/11	01/0/11	11/0/18	11/9/18	11/0/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	11/9/16	1/15/16	1/15/16	1/15/16	1/15/16	11/15/16	1/15/16	1/15/16	11/15/16	11/15/18	11/15/16	91/21/11	91/91/11	Contraction of the second s
LOCATION SA	J19 4254			J19 4235					10 4230	00000 000	0075 01	8774 AL	119 4228	J19 4231	J19 4231	119 4275	J19 4275	119 4261	119 4261	J19 4253	J19 4253	J19 4253	19 4239			J19 4227	J19 4234	J19 4234	J19 4233	119 4233	4276	4276	4276	64242	0474	113 4230	0024						4225	ŝ.	2	2			4232	2468 1				4244	4252						4448	
		1611-120-03 J						1611-120-09 J1							2			1				N	1611-120-21 J1	1611-120-22 J1		1611-120-24 J1				£.	11		~			10 00-071-1101							~			611-120-43 J1	1	ŝ.	1			1	20	m			22		ð.	10 23 001 1191	Ĵ.	

PYRS A-B TN/1000TN		8.42	-5.03	1.48	-3.65	-6.04	3.26	1.10	3.35	3,26	0.44			3.05	-4.20	3.34	5.34	3,66	-0.99	4.87	-3,68	-12.8	-0.83	0.13	-7.37	0.42	-1,30	-9,45	9.42	5.42	6.11	-1.81	-0.02	2.77	45.0
PVR A POT TN/1000TN		1.34	5.65	16.0	2.34	5.75	1.94	4.09	1.84	1.94	3.84			0.31	3,91	3,69	1.69	0,62	2.53	2.16	5.22	9.78	3.28	5.06	4.34	2.03	3.75	11.9	0.34	0.69	0.00	3.34	2.47	4.25	6 24
A-B POT TN/1000TN	11.8	-0.84	-27.3	-27.3	-31,9	-28.0	-12.7	-11.6	-10.4	-12.0	-10.0	18.9	25.4	-16.9	-30.2	-9.27	-13.8	-10.5	-21.0	-15.9	-36.7	-73.9	-16.7	-19.5	-34.5	-20.1	-19.2	-18.4	-5.93	-9.43	-10.9	-33.1	-29.6	-29.1	2 28
NEUT POT TN/1000TN	16.2	9.77	0.62	2.45	-1.21	-0.29	5.19	5,19	5.19	5.19	4.28	21.7	27.1	3.37	-0.29	7,02	7.02	4.28	1.54	7.02	1,54	-3.03	2,45	5.19	-3.03	2.45	2.45	2.45	9.77	6.11	6.11	1.54	2.45	7.02	0.43
ACID POT TN/1000TN	4.38	10.6	27.9	29.8	30.7	27.7	17.9	16.8	15.6	17.2	14.3	2.71	1.74	20.3	29.9	16.3	20.8	14.8	22.5	22.9	38.2	70.8	19.2	24.7	31.5	22.5	21.6	20.9	15.7	15.5	17.0	34.6	32.0	36.1	78.0
org s%		0.14	0.22	0.29	0.34	0.31	0.32	0.34	0.38	0.41	0,52			0.32	0.39	0.20	0.25	0.20	0.24	0.28	0.56	0.90	0.41	0.29	0.38	0.33	0.49	0.32	0.22	0.14	0.18	0.26	0.25	0.59	1 20
PYR S %		0.04	0.18	E0.0	0.08	0.18	0.06	0,13	0.06	0.06	0.12			0.01	0.13	0.12	0.05	0.02	0.08	0.07	0.17	0.31	0.11	0.16	0.14	0.07	0.12	0.38	0.01	0.02	0.00	0.11	0.08	0.14	000
SULFATE S%		0.15	0.49	0.63	0.57	0.39	0.19	0.07	0.06	0.08	<0.01			0.32	0.44	0.21	0.36	0.26	0.40	0.39	0.49	1,05	0.10	0.34	0.49	0.32	0.09	0.00	0.27	0.33	0.37	0.74	0.69	0.43	0.07
TOT \$ %	0.14	0,34	0.89	0,95	0.98	0.89	0.57	0.54	0.50	0.55	0.46	0.09	0.06	0.65	0.96	0.52	0.67	0.47	0.72	0.73	1.22	2.27	0.61	0.79	1.01	0.72	0.69	0.67	0.50	0,50	0.55	1.11	1.03	1.16	3 AG
% CACOS	1.62	0.98	0.06	0.25	<0.01	<0.01	0.52	0.52	0.52	0.52	0.43	2.17	2.71	0.34	<0.01	0.70	0.70	0.43	0.15	0.70	0.15	<0.01	0.25	0.52	<0.01	0.25	0.25	0.25	0.98	0.61	0.61	0.15	0.25	0.70	×0.01
CLASS	CL	CL	CL	L	CL	CL	CL	بہ	SCL	-	SCL	OL	СГ	SCL	SL	SCL	сг	SCL	-	L	٦	-	SL/SCL	SL	C	L	1	CL	-	-	L	L	1	4	Ū
% CLAY	27.5	30.0	28.8	26.3	28.8	28.8	26.3	21.3	23.8	25.0	28.8	28.8	32.5	21.3	2.5	23.8	27.5	25.0	26.3	26.3	23.8	21.3	20.0	13.8	28.8	26.3	25.0	27.5	26.3	26.3	26.3	21.3	22.5	25.0	18.8
% SILT	31.3	31.3	32.5	31.3	28.8	31.3	33.8	28.8	27.5	31.3	17.5	28.8	31,3	23.8	18,8	27.5	31.3	15.0	31.3	30.0	30.0	31.3	27.5	22.5	37.5	35.0	35.0	32.5	28.8	30.0	30.0	31.3	28.8	31.3	213
SAND	41.3	38.8	38.8	42.5	42.5	40.0	40.0	50.0	48.8	43.8	53.8	42.5	36.3	55.0	73.8	48.8	41.3	60.0	42.5	43.8	46.3	47.5	52.5	63.8	33.8	38.8	40.0	40.0	45.0	43.8	43.8	47.5	48.8	43.8	90.0
SAR	2,08	4,34	9.70	12.0	5.08	7.10	14.6	9.51	9.33	10.5	19.0	3.71	4.02	6.67	15.2	5.28	7.52	5.20	6.91	7,15	2.99	3.82	9,51	19.0	3.22	6:39	17.0	25.0	9.89	13.5	13.5	5.99	8.23	0.75	D.B3
SODIUM	9.26	21.3	67,4	79.2	35.6	52.6	64.8	38.0	38.1	43.5	63.1	13.9	11.0	29.9	65.7	25.1	41.0	24.7	37.8	40.8	15.4	30.0	41.1	0.77	18.7	33.7	70.0	89.6	47.4	62.6	63.1	38.3	67.4	4.48	544
MAGNESIUM	14.9	22.5	78.3	68.3	78.5	93.0	21.2	12.8	13.1	15.5	9.0	11.5	6.6	19.1	12.3	24.4	39.7	24.1	41.6	45.0	31.3	104	18.5	11.2	46.1	37.1	16.1	10.4	27.4	25.9	26.5	63.7	116	48.6	129
CALCIUM	24.9	25.7	18.4	19.0	19.8	16.8	18.1	19.2	20.3	18.8	13.1	16.7	8.3	21.2	24.9	20.9	19.7	21.2	18.1	20.3	21.8	19.1	18.9	21.7	21.3	18.6	17.9	15.4	18.6	16.9	17.2	18.2	18.4	22.3	710
% SAT	45.1	46.8	44.3	44.4	44.8	44.0	43.3	44.4	44.7	46.5	38.5	47.3	48.9	39.5	38.4	38.8	44.7	38.9	41.9	43.0	39.4	40.6	40.7	36.1	40.7	41.0	45.8	46.3	42.8	40.3	41.5	39.2	39.0	41.8	49.0
EC MMHO/CM	3.51	4.95	10.2	11.0	7.74	9.72	8.12	5.54	5.70	6.19	7.70	3.46	2.40	5,58	9.17	5.44	7.60	5.43	7.26	7.66	4.89	9.56	6.45	10.2	6.55	6.58	9.11	10.9	7.75	9.19	9.22	8.75	12.9	4.80	14.0
PH UNITS	7.27	2.00	5.11	5.53	4.05	4.23	5.89	6.36	6,49	6.83	6.64	7.41	7.71	7.02	7.05	7.03	6.77	6.50	5.48	5.38	5.79	6.14	5.87	7.13	3.45	5.29	5.58	6.27	6.47	6.82	6.84	4.82	4.93	5.68	267
SAMPLE	0-1	1-3	0-1	13	0-1	1-3	5-1-0	1-3	2	5	1-3	-1-0	1-3	5	13	5	1.3	5	1-3	ς.	0-1	1-3	5	1-3	5	2	0-1	1-3	5	1-3	1.3	0-1	1-3	0-1	5-1
SAMPLE DATE	4/11/17	411117	411117	711117	4/11/17	4/11/17	411117	4/11/17	4/11/17	71/11/4	711114	4/11/17	711117	4/11/17	711117	711117	411117	711117	4/11/17	4/11/17	4/11/17	711117	4/11/17	4/11/17	711117	4/11/17	4/11/17	4/11/17	4/11/17	4/11/17	4/11/17	4/11/17	4/11/17	4/11/17	71117
LOCATION	J19 3040	J19 3040	J19 3048	J19 3048	J19 3049	J19 3049	J19 3059	J19 3059	J19 3059	J19 3066	J19 3066	J19 3162	J19 3162	J19 3163	J19 3163	J19 3164	J19 3164	J19 3165	J19 3165	J19 3165	J19 3060	J19 3060	J19 3061	J19 3061	J19 3062	J19 3062	J19 3063	J19 3063	J19 3064	J19 3064	J19 3064	J19 3077	J19 3077	N9 5095	N9 5095
GAL#	1704-115-01	1704-115-02	1704-115-05	1704-115-06	1704-115-07	1704-115-08	1704-115-09	1704-115-10	1704-115-10R	1704-115-11	1704-115-12	1704-115-13	1704-115-14	1704-115-15	1704-115-16	1704-115-17	1704-115-18	1704-115-19	1704-115-20	704-115-20R	1704-115-21	1704-115-22	1704-115-23	704-115-24	1704-115-25	1704-115-26	1704-115-27	1704-115-28	704-115-29	1704-115-30	704-115-30R	1704-115-31	1704-115-32	1704-115-33	1704-115-34

PYRS A-B TN/1000TN	5.89	2.92	4.23	0.11	0.55	
PYR A POT TN/1000TN	1.53	2.69	2.28	8.22	7.78	
A-B POT TN/1000TN	-7.34	-11.0	-11.4	-10.3	-11.0	
NEUT POT TN/1000TN	7.42	5.61	6.51	8.32	8,32	
AGID POT TW/1000TN	14.8	16.6	17.9	18.6	19.3	
ORG 5%	0.23	0.26	0.30	0.36	0.31	
PYR S %	0.05	0.09	0.07	0.26	0.25	
SULFATE 5%	0,19	0.19	0.21	<0.01	0.06	
TOT S % S	0.47	0.53	0.57	0.60	0.62	
% cAcca	0.74	0.56	0.65	0.83	0.83	
CLASS	CL	С	-	CL	ы	
% CLAY	30.00	27.50	25.00	31.25	31.25	
% SILT	30.00	28.75	30.00	33.75	33.75	
% SAND	40.00	43.75	45.00	35.00	35.00	
SAR	6.96	8.91	11.5	14.3	14.7	
NEQL	34.2	47.0	57.9	66.6	68.7	
MAGNESIUM	24.9	35.0	30.5	23.9	24,3	
CALCIUM	23.3	20.6	19.7	19.7	19.4	
% SAT	44.4	47.4	43.4	50.7	47.3	
EC MMHO/CM	5.00	6.09	6.69	6.98	7,05	
PH UNITS	6.83	6.68	6.94	7,06	7.11	
SAMPLE	0-1	13	0-1	13	1-3	
SAMPLE DATE	5/24/17	5/24/17	5/24/17	5/24/17	5/24/17	
LOCATION	J19 3166	J19 3166	J19 3167	J19 3167	J19 3167	
GAL#	1706-001-03	1706-001-04	1706-001-05	1706-001-06	706-001-06R	

PYRS A-B TN/1000TN			10.2		7.20	10.8	8.16	9.55	4.72	3.32	5.73	3.55		-11.4	111	1.60	-6.18	-0.97	-0.84	-4,65	-2.67	-4.70	-0.42	-3.77	-10.2	-8.61	-2.90	2.53	1.98	5.78	3.36	6.38	6.22	19.2		3.13	3
PYR A POT TN/1000TN			4.44		7.44	2.84	1.72	1.28	5.15	4.65	2.25	9.18		16.5	18.1	8.28	11.3	8,00	5.97	7.87	6.84	8,87	1,75	5.09	16.3	14.7	6.12	2.59	1.25	1.25	2.72	8.25	5.56	6.87		6,75	2
A-B POT P	9,33	3.46	-0.36	20.7	-3.39	-1.00	-1.52	-1.04	-5.96	-3.99	-4.78	-10.0	9.61	-24.3	-23.1	-17.3	-27.4	-22.9	-27.9	-26.1	-34.4	-34.5	-28.7	-29.9	-25.3	-23.5	-23.6	-14.8	-16.0	-11.9	-11.8	-5.91	-10.6	-0.77	2.29	-17.9	2
NEUT POT PUT	11.8	10.8	14.6	34.6	14.6	13.7	9.9	10.8	9.88	7.98	7.98	12.7	19.4	5.13	7.03	9.88	5.13	7.03	5,13	3.23	4.18	4.18	1.32	1.32	6.08	6.08	3.23	5.13	3.23	7.03	8.08	14.6	11.8	26.0	28.9	9.88	22.2
ACID POT NE TN/1000TN TN	2.45	7.37	15.0	13.9	18.0	14.7	11.4	11.9	15.8	12.0	12.8	22.7	9.78	29.4	30.1	27.2	32.5	29.9	33.1	29.3	38.6	38.6	30.0	31.2	31.4	29.6	26.8	19.9	19.3	18.9	17.9	20.5	22.4	26.8	26.6	27.8	
ORG 5% AC			0.14		0.14	0.14	0,16	0.09	0.20	0.27	0.33	0.22		0.31	0.20	0.32	0.21	0.31	0.30	0.27	0.30	0.38	0.32	0.34	0,44	0.29	0.28	0.29	0.21	0.22	0.18	0.30	0.22	0.32		0.20	
PYR S % 0			0.14		0.24	0.09	0.06	0.04	21/0	0.15	0.07	0.29		0.53	0.58	0.27	0.36	0.26	0.19	0.25	0.22	0.28	0.06	0.16	0.52	0.47	0.20	0.08	0.04	0.04	0.09	0.26	0.18	0.22		0.22	;
SULFATE S% P			0.20		0.20	0.24	0.16	0.25	0.15	<0.01	00.0	0.22		0.10	0.18	0.28	0.48	0.39	0.57	0.41	0.71	0.58	0.58	0.50	0.05	0.19	0.38	0.26	0.37	0.35	0.31	0.40	0.32	0.32		0.47	
TOTS% SUI	0.08	0.24	0.48	0.45	0.58	0.47	0.37	0.38	0.51	0.38	0.41	0.73	0.31	0.94	0.96	0.87	1.04	0.96	1.06	0.94	1.23	1.24	0.96	1.00	1.00	0.95	0.86	0.64	0.62	0.61	0.57	0.66	0.72	0.86	0.85	0.89	
% CACOS	1.18	1.08	1.46	3.46	1.46	1.37	0.99	1.08	0.99	0.80	0.80	1.27	1.94	0.51	0.70	0,99	0.51	0.70	0.51	0.32	0.42	0.42	0.13	0.13	0.61	0.61	0.32	0.51	0.32	0.70	0.61	1.46	1.18	2.60	2.89	0.99	
CLASS	CL	SCL	CL	CL	CL	CL	CL	SCL	CL	CL	CL	CL	С	CL	CL	CL	CL	4	OL	Ъ	СL	сг	сГ	OL	Ъ	CL	Ъ	СГ	CL	CL	CL	SCL	CL	SL	SL	SL	;
% CLAY	35.00	31.25	33.75	32,50	33.75	33.75	37.50	23.75	28.75	33.75	33.75	31.25	32.50	28.75	27.50	30.00	31.25	26.25	28.75	28.75	27.50	28.75	31.25	31.25	31.25	32.50	32.50	35.00	36.25	33.75	36.25	25.00	33.75	18.75	18.75	31.25	
% SILT	23.75	21.25	28.75	28.75	30.00	27.50	30.00	23,75	27.50	26.25	27.50	27.50	25.00	28.75	30.00	30.00	28.75	30.00	28.75	28.75	28.75	31.25	32.50	32.50	30.00	28.75	26.25	25.00	27.50	26.25	26.25	25.00	33,75	20.00	21.25	32.50	
% SAND	41.25	47.50	37.50	38.75	36.25	38.75	32.50	52.50	43.75	40.00	38.75	41.25	42.50	42.50	42.50	40.00	40.00	43.75	42.50	42.50	43.75	40.00	36.25	36.25	38.75	38.75	41.25	40.00	36,25	40.00	37,50	50.00	32.50	61.25	60.00	36.25	- and
SAR	3.58	2.98	13.9	10.6	13.5	12.3	12.5	7.15	6.19	9.80	9.84	13.7	15.4	20.1	20.2	12.1	12.1	11.0	11.3	11.0	13.4	17.6	10.0	7.27	12.9	13.1	17.8	18.2	15.2	16.7	16,6	16.4	20.4	17,3	11.7	11.1	
SODIUM	14.7	17.71	73.1	54.4	66.6	63.1	65.7	38.4	31.4	45.7	46.5	75.3	67.4	99.2	82.2	66.6	69.6	69.2	78.7	73.5	104	104	76.6	51.8	79.2	75.3	100	85.3	81.8	86.1	84.4	88.3	97.9	84.4	71.3	0.79	1
MAGNESIUM MEQIL	20.7	48.7	32.3	30.8	28.3	29.8	34.1	34.5	29.0	22.6	23,1	39.4	16.9	28.3	16.1	39.7	46.2	60.1	76.8	70.7	97.9	48.8	97.1	81.6	54.8	46.2	43.2	24.4	31.8	24.1	23.5	34,9	23.9	16.6	54.0	131	
MEQ/L	13.1	22.0	22.9	22.0	20.4	22.6	20.9	23.2	22.4	20.8	21.7	21.1	21.7	20.3	17.0	20.7	19.5	19.2	20.9	19.2	21.6	21.3	19.2	19.8	20.1	19.7	19.7	19.4	26.3	29.2	28.4	23.2	22.1	30.7	20.4	21.3	
% SAT	42.9	40.9	49.9	44.3	45.1	46.5	51.5	33.4	43.1	55.4	55.2	41.5	41.2	48.5	43.9	40.8	43,9	38.9	39.4	38.4	39.4	40.2	43.7	44.1	41.4	48.9	43.1	44.9	36.5	37.6	36.9	33.5	42.8	30.1	32.1	43.4	
EC MMHO/CM	3.54	5.53	9.33	7.56	8.55	8,32	8.63	6.59	5.74	6.46	6.80	9.61	8.11	11.2	9.15	8.88	9.50	10.1	11.6	10.9	13.6	12.3	11.7	9.15	10.3	9.61	11.2	9.47	9.72	9.77	9.59	10.3	10.3	9.72	9,68	14.3	
PH UNITS	7.73	7.42	7.18	7.55	7.05	7.43	7.31	7.37	6.96	6.83	6.82	6.23	7.25	6.24	6.27	6,10	6.23	5.62	5.67	5.63	5.02	5.74	5.00	5.06	6.02	5.91	5.54	6.30	5.37	5.80	5.82	6.51	61.9	6.42	6.73	6.19	
SAMPLE	0-1	1-3	0-1	1-3	-1	1-3	0-1	1-3		1-3	1-3		1-3	6-1	1-3		1-3	6-1	13	1-3	0-1	1-3	0-1	1.3	5	13	5	1-3	6-1	1-3	1-3	6-1	1-3	0-1	1-3	0-1	
SAMPLE DATE	7/6/17	7/16/17	7/6/17	7/6/17	7/6/17	7/6/17	7/8/17	7/6/17	7/18/17	7/8/17	7//8/17	71/8/17	7/6/17	7/6/17	7/6/17	7/6/17	7/6/17	7/6/17	7/6/17	718/17	7/6/17	7/6/17	7/6/17	7/6/17	7/6/17	7/6/17	7/8/17	7/6/17	7/6/17	7/6/17	7/8/17	7/6/17	7/6/17	7/6/17	7/18/17	7/6/17	
LOCATION 5	2837	2837	2833	2833	2936	2936	2834	2834	2938	2938	2938	2902	2902	2910	2910	2907	2907	2805	2905	2905	3023	3023	2908	2908	2904	2904	3050	3050	3051	3051	3051	3054	3054	3026	3026	3022	
GAL #	1707-068-01	1707-068-02	1707-068-03	1707-068-04	1707-068-05	1707-068-06	1707-068-07	1707-068-08	1707-068-09	1707-068-10	1707-068-10R	1707-068-11	1707-068-12	1707-068-15	1707-068-16	1707-068-17	1707-068-18	1707-068-19	1707-068-20	1707-068-20R	1707-068-21	1707-068-22	1707-068-23	1707-068-24	1707-068-25	1707-068-26	1707-068-27	1707-068-28	1707-068-29	1707-068-30	1707-068-30R	1707-068-31	1707-068-32	1707-068-33	1707-068-34	1707-068-35	

PYRS A-B TN/10001N								6.26			3.27	-2.94	0.41	2.41	1.66	-2.47	-0,93	-1.50	6.75	13.3	-3,43	0.37
PYR A POT TN/1000TN								1.72			2.81	3.31	2.81	0.81	3.47	4.75	4.15	1.87	5.03	3.25	<0.01	<0.01
A-B POT	4.34	6.81	4.87	19.4	12.9	10.5	0.19	-7.24	7.75	5.23	-18.7	-36.4	-24.3	-22.6	-21.4	-22.2	-22.2	-27.9	-1.83	-6.60	-42.1	-31.6
NEUT POT	13.7	13.7	19.4	27.0	21.3	21.3	9.88	7.98	21.3	18.4	6.08	0.37	3.23	3.23	5.13	2.28	3.23	0.37	11.8	16.5	-3.43	0.37
ACID POT TN/1000TN	9.34	6.87	14.5	7.56	8.35	10.8	69.6	15.2	13.5	13.2	24.8	36.7	27.5	25.8	26.6	24.5	25.4	28.3	13.6	23.1	38.7	32.0
ORG S%								0.26			0.36	0.26	0.43	0.36	0.28	0.30	0.33	0.29	0.28	0.35	0.48	0.51
PYR S %								0.06			0.09	0,11	0.09	0.03	0.11	0.15	0.13	0.06	0.16	0.10	<0.01	<0.01
SULFATE S%								0.17			0.35	0.81	0.36	0.44	0.46	0.33	0.35	0.56	00.0	0.29	0.77	0.55
TOTS% SI	0.30	0.22	0.46	0.24	0.27	0.34	0.31	0.49	0.43	0.42	0.79	1,18	0.88	0.83	0.85	0.78	0.81	0.90	0.44	0.74	1.24	1.02
% CACOS	1.37	1.37	1.94	2.70	2.13	2.13	0.99	0.80	2.13	1.84	0.61	0.04	0.32	0.32	0.51	0.23	0.32	0.04	1.18	1.65	<0.01	0.04
CLASS	CL	CL	ы	CL	SCL	SCL	С	SCL	С	CL	CL	CL	С	Ъ	С	CL	С	СГ	СГ	CL	CL	С
% CLAY	32.50	30.00	27.50	30.00	23.75	26.25	30.00	27.50	30.00	32.50	32.50	32.50	31.25	32.50	32.50	32.50	31.25	30.00	38.75	32.50	32.50	33.75
17IS %	30.00	31.25	28.75	28.75	27.50	27.50	30.00	26.25	31.25	30.00	33.75	32,50	32.50	31.25	32.50	30.00	31,25	32.50	28.75	26.25	33.75	30.00
% SAND	37.50	38.75	43.75	41.25	48.75	46.25	40.00	46.25	38.75	37.50	33.75	35.00	36.25	36.25	35.00	37.50	37.50	37.50	32.50	41.25	33,75	36.25
SAR	10.5	7.49	7.27	6.79	4.70	8.84	10.4	11.1	9.80	8.57	9.60	5.43	10.6	10.1	9.90	10.6	11.8	8.88	17.7	18.1	3.2	11.4
SODIUM MEQ/L	48.7	36.8	40.6	34.4	25.3	44.4	51.3	54.4	49.2	43.5	55.7	39.4	65.7	62.2	60.9	68,3	67.0	64.8	82.2	86.1	23.1	64.4
MAGNESIUM MEQAL	20.8	25.0	38.3	27.7	32.0	26.7	25.8	23.3	28.1	28.2	44.9	83.9	56.0	55.0	54.9	61.2	43.5	86.4	23.7	25.0	81.9	44.3
MEQ/L	22.1	23.2	24.1	23.8	26.0	23.8	23.0	24.7	22.3	23.4	22.3	21.3	21.3	21.1	20,9	21.1	21.5	20.1	19.6	20.2	21.0	19.6
%SAT	50.3	43.2	40.1	40.4	35.6	35.9	38.6	36.6	38.1	40.0	40.7	42.4	40.1	40.8	40.1	40.7	39.6	38.4	47.8	43.3	43.3	45.1
EC MMHO/CM	6,83	6.01	7.02	6.05	5.60	7.05	7.31	7.45	7.08	6.57	8.35	8.41	9.68	9.32	9.27	10.2	9.26	10.7	9,92	7,39	10.3	8.93
PH UNITS	6.98	6.98	7.06	7.31	7.12	7.28	7.26	7.02	6.95	7.13	6.28	5.01	5.93	5.79	5.74	5.33	5.65	4.48	6.99	7.06	3.57	5.22
DEPTH	61	1-3	0-1	1-3	0-1	1-3	0-1	1-3	6-1	1-3	0-1	1-3	0-1	1-3	0-1	1-3	0-1	5	0-1	1-3	0-1	1-3
SAMPLE DATE	THITT	THITT	THITT	THINT	THITT	TRIAT	THITT	THITT	LUUL	LULL	LULL	LVILL	LUILL	LULL	THINT	THIT	Tri177	THITT	7/6/17	7/6/17	7/6/17	7/16/17
LOCATION	3186	3186	3188	3188	3189	3189	3185	3185	3187	3187	3068	3068	3070	3070	3173	3173	3069	3069	3053	3053	3052	3052
GAL#	707-095-01	707-095-02	707-095-03	707-095-04	707-095-07	707-095-08	707-095-11	707-095-12	707-095-15	707-095-16	707-095-17	1707-095-18	707-095-21	1707-095-22	707-095-23	707-095-24	707-095-25	707-095-26	707-095-33	707-095-34	707-095-35	707-095-36

TN/1000TN	-4.91	-12.5	7.37	-12.0		3.91	0.32	4.44		12.8		13.4				9.74	15.0
TIN1000TN TI	-1.37	0.56	1.56	14.3		7.87	1.00	0.69		0.91		2.16				3.94	1.56
A-B POT PI	-55.5	-76.4	-9.60	-30.6	5.41	-20.6	-30.1	-28,3	6.80	-6.34	0.46	-1.39	1.53	1.11	8.55	-8.51	-0.14
TN/1000TN TN	-6.28	-12.0	8.93	2.28	21.3	11.8	1.32	5.13	21.3	13.7	18.4	15,6	17.5	18.4	18,4	13.7	16.5
ACID POT NEL	49.2	64.4	18.5	32.9	15.9	32.3	31.4	33.4	14.5	20.0	18.0	17.0	16.0	7.29	9.89	22.2	16.7
ORG 5% ACI	0.62	1.00	0.16	0.23		0.29	0.23	0.35		0.16		0.13				0.19	0.19
PYR 5% OR	-0.04	0.02	0.05	0.46		0.25	0.03	0.02		0.03		20.0				0.13	0.05
SULFATE S% PYF	1.00	1.04	0.38	0.36		0.49	0.74	0.70		0.45		0.34				0.39	0.29
TOT S % SULFA	1.57	2.06	0.59	1.05	0.51	1.04	1.01	1.07	0.46	0.64	0.58	0.54	0.51	0.23	0.32	0.71	0.53
% CACOS TOT	<0.01	<0.01	0.89	0.23	2.13	1.18	0.13	0.51							1.84	1.37	1.65
		·		_													
VY CLASS	0 CI	O C			0 CL		ũ		5		2		Å	-			
% CLAY	1	27.50			30.00												
" SILT	46.25	46.25	30.00	31.25	33.75	28.75	31.25	26.25	31.25	30.00	31.25	32.50	28.75	33.75	37.50	35.00	31.25
% SAND	26.25	26.25	50.00	41.25	36.25	42.50	41.25	50.00	36.25	36.25	36.25	35.00	38.75	28.75	28.75	28.75	36.25
SAR	0.01	0.03	12.8	19.6	0.89	3.50	4.33	1.80	10.9	10.9	10.9	13.1	12.8	0.34	0.72	16.5	13.6
MEGAL	0.13	0.26	87,4	108	3.81	19.1	32.8	11.5	57.0	62.2	66.6	76.1	71.8	1.67	3.90	83.5	65.7
MEQIL	110	178	71.2	40.8	11.2	35.2	90.5	51.4	31.9	42.9	45.2	40.7	37.9	24.2	33.7	30.9	25.3
MEGUL	30,9	28.0	22.0	20.0	25.2	24.5	24.1	29.6	22.3	21.8	29.0	27.2	25.1	24.5	24.8	20.4	21.3
% SAT	39.5	37.4	33.4	40.5	41.2	39.9	36.9	38.7	42.1	43.3	42.6	43.1	42.1	43.6	41.5	47.1	46.3
EC MMHO/CM	12.2	23.9	13,4	13.4	2.69	5.17	9,10	6.03	9,52	10.9	9.22	10.4	10.5	3.32	4.15	12.9	10.2
PH UNITS E	2.16	1.94	7.07	5.36	7.12	6.54	4.29	6.41	7.44	7.10	7.24	7.23	7.24	7.10	7.29	7.29	7.41
DEPTH	0-1	1-3	0-1	1-3	0-1	1-3	0-1	1-3	0-1	1-3	0-1	1-3	1-3	0-1	1-3	0-1	1-3
SAMPLE DATE	8/25/17	8/25/17	8/25/17	8/25/17	8/25/17	8/25/17	8/25/17	8/25/17	8/24/17	8/24/17	8/24/17	8/24/17	8/24/17	8/25/17	8/25/17	8/24/17	8/24/17
OCATION SI	5020	5020	5069	5069	5068												
GAL# L	708296-11	708296-12	708296-13	708296-14	708296-15	708296-16	~		1708296-27				08296-30R	708296-31	708296-32	708296-33	708296-34

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PYRS A-B TN/1000TN	1.21	-1.38	-6.42	-6.89	-0.01	6.56	4.68	6,33	2.03	-21.0	-19.3	-2.16	-4.09	-5.94	-14.9	-14.9	-0.05	-5.12	-4.33	6.53	
PYR A POT TN/1000TN	1.50	3.09	1.16	2.62	2.72	2.12	4.00	3.34	4.65	17.71	14.1	10.8	10.8	7.65	4.75	4.72	4.75	2.84	1.06	2.16	
A-B POT TN/1000TN	-14.5	-25.0	-58.2	-68.2	-30.4	-23.5	-22.9	-20.1	-18.0	-54.7	-56.2	-21.9	-28.4	-26.5	-65.5	-67.2	-23.6	-49.3	-51.6	-16.7	
NEUT POT TN/1000TN	2.71	1.71	-5.26	-4.27	2.71	8,68	8.68	9.68	69.9	-3.27	-5.26	8.68	6.69	1.71	-10.2	-10.2	4,70	-2.28	-3.27	8,68	
ACID POT ACID POT T	17,18	26.7	53.0	63.9	33.1	32.2	31.6	29.8	24.7	51.4	51.0	30.6	35.1	28.2	55.3	57.0	28.3	47.0	48.3	25.4	
ORG S%	0.22	0.25	0.44	0.48	0.30	0.28	0.22	0.20	0.19	0.44	0.44	0.35	0.39	0.33	0.44	0.44	0.32	0.45	0.46	0.23	20.0
PVR S %	0.05	0.10	0.04	0.08	0.09	0.07	0.13	0.11	0.15	0.57	0.45	0.35	0.35	0.25	0.15	0.15	0.15	60.0	0.03	10.07	
SULFATE 5% P	0.26	0.51	1.22	1.49	0.68	0.69	0.66	0.64	0.46	0.64	0.74	0.29	0.39	0.33	1.18	1.24	0.44	79.0	1.05	0.52	0.0
tors % su	0.55	0.86	1.70	2.05	1.06	1.03	1.01	0.95	0.79	1.65	1.63	0.98	1.12	0.90	1.77	1.82	0.91	1.50	1.55	0.81	
% CACOS	0.27	0.17	<0.010	<0.010	0.27	0.87	0.87	0.97	0.67	<0.010	<0.010	0.87	0.67	0.17	<0.010	<0.010	0.47	<0.010	<0.010	0.87	
CLASS	CL	CL/SCL	сг	ц	SCL	SCL	CL/SCL	С	CL	CL	CL	SCL	SCL	SCL	SCL	SCL	CL	CL	CL	CL	č
% CLAY	33.75	30.00	31.25	28.75	28.75	27.50	28.75	32.50	31.25	30.00	30.00	26.25	27.50	26.25	23.75	25.00	32.50	35.00	33.75	33.75	00 00
% SILT	30.00	25.00	28.75	28.75	25.00	26.25	26.25	30.00	31.25	28.75	27.50	26.25	26.25	26.25	25.00	23.75	27.50	28.75	30.00	28.75	24.05
% SAND	36.25	45.00	40.00	42.50	46.25	46.25	45.00	37.50	37.50	41.25	42,50	47.50	46.25	47.50	51.25	51.25	40.00	36.25	36.25	37.50	20.00
SAR	11.4	16.9	5.20	5.79	5.94	6.27	6,16	12.2	11.6	60'1	7.70	8.63	9.69	8.24	2.15	2.15	13.6	19,4	17.2	14.5	1 0 0
SODIUM	59.2	99.2	60.5	65.2	38.3	39.7	38.3	64.8	60.9	43.1	49.6	44.8	48.3	50.5	21.1	20.8	78.3	132	101	73.9	000
MAGNESIUM	33.0	46.0	249	234	60.7	57.8	55,5	35.5	34.6	54.2	63.0	29.5	27.1	54.1	169	166	46.6	69.4	51.7	31.8	
GALCIUM	21.2	23.1	21.0	20.7	22.4	22.4	21.7	21.3	20.6	19.5	20.0	24.4	22.5	20.8	23.4	22.3	19.3	23.2	18.0	20.5	0.00
% SAT	39.4	42.2	38.7	41.3	39.4	42.0	42.1	43.2	41.0	37.9	37.5	37.5	38.9	36.2	37.2	37.3	41.2	40.3	42.1	39.9	0.04
EC MMHO/CM	8.33	11.0	15.1	14.7	7.59	7.45	7.41	8.63	8,35	7.63	8.38	6.85	6.91	8.19	10.7	10.8	10.2	13.0	12.1	8.98	000
STINU HA	6.16	6.35	4.28	4.45	5.93	7.00	7.02	6.72	6.70	5.13	5.18	6.24	6.16	5.74	3.03	3.03	6.32	4.66	4.66	6.99	C 7 E
SAMPLE	0-1	1-3	0-1	1-3	0-1	1-3	1-3	6-1	1-3	5	13	0-1	1.3	0-1	5	1-3	0-1	1-3	1-3	0-1	
SAMPLE DATE	10/18/17	10/18/17	10/18/17	10/18/17	10/18/17	10/18/17	10/18/17	10/19/17	10/19/17	10/19/17	10/19/17	10/19/17	10/19/17	10/19/17	10/19/17	10/19/17	10/18/17	10/18/17	10/18/17	10/19/17	40140147
LOCATION	4721	4721	4532	4532	4753	4753	4753	4688	4688	4716	4716	4717	4717	4718	4718	4718	4722	4722	4722	4651	ADEA
GAL #	1710-194-01	1710-194-02	1710-194-03	1710-194-04	1710-194-09	1710-194-10	710-194-10R	1710-194-11	1710-194-12	1710-194-15	1710-194-16	1710-194-17	1710-194-18	1710-194-19	1710-194-20	710-194-20R	1710-194-29	1710-194-30	710-194-30R	1710-194-31	00 101 014

PYRS A-B TN/10001/NT	8.27	Ĺ		-6.60													0.60	8.54	10.7	14.1	17.2	
PYR A POT TN/1000TN	2.41	9.56	5.373	7.3	5.97	3.62	1.87	8.12	3.47	23.5	9.31	8.25	5.50	8.03	10.0		6.09	4.12	<0.01	2.56	3.44	
A-B POT TN/1000TN	-13.2	-14.6	-25.4	-23.1	-13.0	-18.3	-6.24	-5.79	-6.97	-33.0	-17.2	-17.5	-8,26	-36.6	-27.3	47.9	-7,89	-10.5	-2.35	-4.69	-0.58	1
NEUT POT TN/1000TN	10.7	7.69	-3.27	0.71	4.70	2.71	10.7	9.68	8,68	5,69	6.69	13.7	18.6	7.69	13.7	57.9	6.69	12.7	10.7	16.6	20.6	
ACID POT TN/1000TN	23.9	22.3	22.1	23.8	1.71	21.0	16.9	15.5	15.7	38.7	23.9	31.2	26.9	44.2	41.0	10.0	14.6	23.2	13.0	21.3	21.2	La
ORG 5%	0.24	0.42	0.45	0.44	0.21	0.25	0.14	0.15	0.16	0.45	0.33	0.33	0.31	0.42	0.35		0.10	0.22	0.23	0.31	0.27	101
PYR 5%	0.08	0.31	0.17	0.23	0.19	0.12	0.06	0.26	0.11	0.75	0.30	0.26	0.18	0.26	0.32		0.20	0.13	<0.010	0.08	0.11	
SULFATE S%	0.45	0.00	0.09	0.09	0.16	0.31	0.34	0.08	0.23	0.04	0.13	0.41	0.38	0.74	0.64		0.17	0.40	0.19	0.29	0.30	
TOT 5 % 5	0.76	0.71	0.71	0.76	0.57	0.67	0.54	0.50	0.50	1.24	0.76	1.00	0.86	1.42	1.31	0.32	0.47	0.74	0,42	0.68	0.68	
% CAGO3	1.07	0.77	<0.010	0.07	0.47	0.27	1.07	0.97	0.87	0.57	0.67	1.37	1.86	0.77	1.37	5.79	0.67	1.27	1.07	1.66	2.06	
CLASS	SCL	CL/SCL	SCL	CL	CL	CL	CL	CL	CL	CL	CL	CL	CL	CL/C	CL	() ()						
% CLAY	30.00	32.50	25.00	22.50	28.75	27.50	21.25	21,25	21.25	30.00	32.50	33.75	35.00	35.00	36.25	37.50	37.50	38.75	36.25	40.00	37.50	
% SILT	22.50	22.50	25.00	21.25	25.00	23.75	21.25	23.75	22.50	26.25	31.25	30,00	27.50	27.50	27.50	28.75	28.75	30.00	33.75	30.00	26.25	
% SAND	47.50	45.00	50.00	56.25	46.25	48.75	57.50	55.00	56.25	43.75	36.25	36.25	37.50	37.50	36.25	33.75	33.75	31.25	30.00	30.00	36.25	
SAR	9.14	21.0	20.5	20.8	9.88	8.98	4,92	1.22	1.23	9.87	17.4	14.8	18.5	6.38	6.82	10.8	20.0	13.1	22.2	14.2	13.9	
SODIUM	56.1	90.06	85.7	82.6	46.5	45.7	27.6	5.74	5.79	48.3	78.3	80.0	95.3	39.1	39.6	48.3	6'06	66.1	99.2	67.0	63.5	
MAGNESIUM	55.3	18.8	15.4	11.8	24.8	31.6	42.0	20.8	20.9	26.6	21.0	39.6	34.6	52.3	44.7	20.9	23.1	31.7	22.0	25.4	22.5	1000 m
CALGIUM	20.1	18.1	19.6	19.8	19.7	20.1	20.8	23.5	23.5	21.3	19.6	18.9	18.6	22.6	22.8	19.0	18.3	19.5	17.9	19,1	19.0	
% SAT	38.0	40.9	40.1	40.6	39.6	22.3	34.8	33.1	32.6	38.4	41.8	40.0	41.8	37.5	41.3	42.5	45.1	44.2	43.4	42.0	44.0	1
EC MMHO/CM	8.67	9.74	9.21	8.82	6.63	6.85	5.98	3.44	3.49	6.93	8.94	9.71	10.9	7.32	7.15	6.54	10.0	8.41	10.7	8.37	7.93	1111
PH UNITS	6.52	7.12	6.83	6.80	7.23	71.17	6.55	7.02	7.03	6.59	7.04	7.33	7.47	6.56	6.8	7.46	7.34	7.14	7.62	7.30	7.36	100
SAMPLE	0-1	1.3	0-1	1-3	0-1	1-3	0-1	1-3	1-3	0-1	1-3	0-1	1-3	5-1	1-3	0-1	1-3	0-1	1-3	6-1	1-3	
SAMPLE DATE	10/18/17	10/18/17	10/18/17	10/18/17	10/18/17	10/18/17	10/18/17	10/18/17	10/18/17	10/18/17	10/18/17	10/18/17	10/18/17	10/19/17	10/19/17	10/19/17	10/19/17	10/19/17	10/19/17	10/19/17	10/19/17	
LOCATION	5066	5066	4531	4531	5064	5064	5065	5065	5065	4682	4682	4683	4683	4748	4748	4749	4749	4750	4750	4752	4752	
GAL#	1710-195-01	1710-195-02	710-195-03	710-195-04	710-195-07	710-195-08	710-195-09	710-195-10	710-195-10R	(710-195-13	1710-195-14	1710-195-15	1710-195-16	1710-195-21	1710-195-22	710-195-23	1710-195-24	1710-195-25	710-195-26	710-195-29	710-195-30	and the state of t

PYRS A-B TN/1000TN					-5.36	1.04	-14.2	-13.0	-16.2	-3,13	5,11-	-21.0	6.32	A 30
PYR A POT TN/1000TN					11.4	5.94	9,28	4.06	5.34	4.15	10.4	1.16	0.66	1 69
A-B POT IN/1000TN	7.65	11.5	0.43	4.18	-23.9	-25.2	-58.6	-65.5	-80.4	-37.3	-64.4	-44.7	-24.0	18.6
NEUT POT TN/1000TN	11.9	12.9	4.99	8.96	5.98	6.97	4.92	-8.89	-10.9	1.03	-0.96	-19.8	6.97	5 98
ACID POT TN/1000TN	4.25	1,40	4.56	4.78	29.9	32.2	53.6	56.6	69.5	38.3	63.4	24.9	31.0	24.5
ORG 5%					0.23	0.24	0.35	0.52	0.48	0.35	0.52	0.14	0.16	0.15
PYR 5%					0.36	0.19	0.30	0.13	0.17	0.13	0.33	0.04	0.02	0.05
SULFATE 5%					0.37	0.60	1.07	1.16	1.58	0.74	1.18	0.62	0.81	0.58
TOT 5 % 5	0.14	0.04	0.15	0.15	0.96	1.03	1.72	1.81	2.23	1.23	2.03	0.80	0.99	0.79
% CAGOS	1.19	1.29	0.50	06'0	0.60	0.70	<0.01	<0.01	<0.01	0.10	<0.01	<0.01	0.70	0.60
CLASS	CL	SCL	CL	CL	CL	CL	CL	CL	С	SCL	CL	SCL	SCL	SCI
% CLAY	35.00	25.00	28.75	33.75	31.25	30.00	30.00	31.25	31.25	26.25	27.50	22.50	21.25	21.25
% SILT	26.25	25.00	38.75	36.25	31.25	28.75	32.50	31.25	32.50	26.25	28.79	23.75	22.50	22.50
% SAND	38.75	50,00	32.50	30.00	37,50	41.25	37.50	37.50	36.25	47.50	43.75	53.75	56.25	56.25
SAR	28.5	39.0	9.08	8.90	10.8	8.66	0,83	2.20	1.81	5.67	8.47	3.50	2.65	2.81
NEQL	48.3	37.7	49.6	46.5	96.1	63.9	7.00	17.0	15.5	39.8	64.8	23.8	17.8	19.5
MAGNESIUM	2.85	1.04	2.74	1.31	49.1	35.8	133	100	127	77.8	91.3	69.1	66.3	712
CALCIUM	2.88	0.83	56.9	53.4	110.3	73.4	8.03	19.5	20.7	20.9	25.7	23.9	24.0	25.2
% SAT	40.7	33.1	40.1	42.6	34.9	39.2	33.3	35.3	38.5	37.3	37.6	34.2	35.2	34.1
EC MMHOICM	4.91	3.78	4.97	4.59	11.0	8.75	7.97	7.38	7.41	8.35	9.55	6.82	6.11	6.48
PH UNITS	7.90	8.45	7.56	8.13	6.33	6.03	3.19	3.32	3.32	5.62	4.51	7.04	6.91	6.83
DEPTH	0-1	1-3	0-1	1-3	6-1	1-3	0-1	1-3	1-3	5-	1-3	0-1	12	1-3
SAMPLE DATE	4/13/18	4/13/18	4/13/18	4/13/18	4/11/18	4/11/18	4/11/18	4/11/18	4/11/18	4/11/18	4/11/18	4/11/18	4/11/18	4/11/18
LOCATION	2945	2945	4256	4256	4493	4493	4494	4494	4494	5126	5126	5142	5142	5142
GAL #	1804-127-01	1804-127-02	1804-127-51	1804-127-52	1804-127-57	1804-127-58	1804-127-59	1804-127-60	1804-127-60R	1804-127-65	1804-127-66	1804-127-69	1804-127-70	804-127-70R

GAL	LOCATION	SAMPLE DATE	DEPTH	PH UNITS	EC MMHO/CM	%SAT	MEQL	MEGAL	MEQL	SAR	W SAND	% SILT	% CLAY	CLASS	% CAGO3	101 8%	SULFATE S%	PYR 3%	ORG S%	TN/1000TN	TN1000TN	TNUODOTN	TUNODOTN	TNHOODTN
1806-195-13	4496	6/19/18	0-1	6.51	10.8	38.1	20.3	28.1	73.9	15.0	40.00	27.50	32.50	CL	0.97	1.14	0.65	0.32	0.17	35.6	9.66	-25.9	9.87	-0
1806-195-14	4496	6/19/18	1-3	5.09	13.9	35.8	18.0	118	71.8	8.72	38.75	27,50	33.75	CL	<0.01	1.81	1.05	0.36	0.40	56.6	-3.23	-59.8	11.3	41-
1806-195-17	4495	6/19/18	0-1	6.49	10.6	34.4	21.5	44.7	79.6	13.8	38.75	28,75	32.50	CL	0.87	0.83	0,36	0.16	0.31	25.8	8.67	-17.2	5.00	3.67
1806-195-18	4495	6/19/18	1-3	6.63	11.5	32.2	17.7	35.4	81.8	15.9	35.00	31.25	33.75	CL	1.16	0.82	0.32	0.26	0.24	25.8	11.6	-14.1	8.06	3.5
1806-195-19	4534	6/19/18	0-1	6.64	4.85	38.1	22.5	18.4	6.05	1.34	66.25	22.50	11.25	SL	2.95	0.12				3.65	29.5	25,8		
1806-195-20	4534	6/19/18	1-3	6.75	5.58	40.8	24.3	19.4	22.7	4.87	50.00	27,50	22.50	SCL	7.76	0.22				6.93	77.6	70.6		
806-195-20R	4534	6/19/18	1-3	6.80	5.26	40.5	22.1	17.7	21.0	4.71	51.25	26.25	22.50	SCL	7.76	0.24				7.52	77.6	70.0		
1806-195-25	4571	6/19/18	0-1	6.42	9.16	40.3	21.8	28.9	58.3	11.6	38.75	30,00	31.25	CL	0.97	0.69	0.19	0.33	0.17	21.4	9.66	-11.8	10.3	0
1806-195-26	4571	6/19/18	1-3	6.52	10.2	40.3	18.1	29.3	70.9	14.6	31.25	32.50	36.25	CL	0.67	1.11	0.56	0.35	0.19	34.6	69.9	-27.9	11.0	4
1806-195-33	5092	6/19/18	0-1	6.05	6.00	38.9	24.7	40.3	17.7	3.11	36.25	31.25	32.50	CL	1.16	0.69	0.30	0.10	0.29	21.4	11.6	-9.79	3.06	8
1806-195-34	5092	6/19/18	1.3	6.18	5.79	37.4	24.5	40.4	16.0	2.80	36.25	30.00	33.75	CL	1.96	0.78	0.36	0.14	0.27	24.3	19.6	4.74	4.43	15,15
1806-195-35	5114	6/19/18	1-0	6.13	12.8	38.7	20.0	75.4	72.2	10.5	46.25	25.00	28.75	SCL	0.67	1.00	0.38	0.16	0.45	31.1	6.69	-24.5	5.00	1.6
1806-195-36	5114	6/19/18	1-3	6.04	11.7	37.8	18.7	82.0	56.5	7.97	42.50	26.25	31.25	СГ	0.57	1.01	0.41	0.16	0.43	31.4	5.70	-25.7	5.06	0.6
1806-195-37	5093	6/19/18	0-1	6.06	9.71	34.6	27.6	79.4	34.8	4.75	41.25	30.00	28.75	CL	0.67	1.11	0.70	0.02	0.40	34.6	6,69	-28.0	0.50	.9
1806-195-38	5093	6/19/18	1-3	6.18	70.7	29.5	26.6	60.9	13.8	2.09	53.75	25.00	21.25	SCL	1.66	0.55	0.28	0.04	0.23	17.2	16.6	-0.56	1.21	15

PYRS A-8 TNI1000TW	-0.60
PYR A POT TN/1000TN	1.20
A-B POT TN/10001N	-15.3 -24.1
NEUT POT TN/1000TN	2.72 3.71
AGID POT TN/1 000TN	18.1 27.8
ORG 5%	0.137 0.243
PVR S %	0.038 0.138
SULFATE S%	0,402 0,509
TOT 5 %	0.578 0.890
% CACO3	0.272 0.371
CLASS	scr
% CLAY	22.5 23.8
% SILT	23.8 25.0
% SAND	53,8 51,3
SAR	2.39 5.89
SODIUM	13.4 40.0
MAGNESIUM	39.3 72.7
CALGIUM	23.1 19.6
AR % SAT	33.1 32.2
PH UNITS EC MMHOICM	5,43 9.37
PH UNITS	5,48 5.61
SAMPLE	0-1 1-3
SAMPLE DATE	8/15/18 8/15/18
LOCATION	5087 5087
GAL#	1808-214-35 1808-214-36

GAL #	LOCATION	SAMPLE DATE	SAMPLE DEPTH	STINU H4	EC MMHOICM	% SAT	CALCIUM	MAGNESIUM	NEQ/L	SAR	% SAND	% SILT	% CLAY	CLASS	% CAGO3	101 S %	SULFATE S%	PYR S %	ORG S%	ACID POT TW/1000TN	NEUT POT TW/1000TN	A-B POT TM/1000TN	PVR A POT TN/1000TN	PYRS A-B TM1000TM
1809-178-05	4644	9/21/18	0-1	5.51	10.6	37.6	18.4	63.3	67.4	10.5	35.00	30.00	35.00	CL	0.20	1.27	0.44	0.45	0.37	39.6	1.97	-37.7	14.2	-12
1809-178-06	4644	9/21/18	1-3	5.57	16.3	38.4	19.8	111	113	13.9	33.75	30.00	36.25	5	0.20	1.33	0.72	0.26	0.35	41.5	1.97	-39.5	8.20	-6.23
909-178-06R	4644	9/21/18	1-3	5.59	14.8	39.9	19.3	110	111	13.8	36.25	28.75	35.00	CL	0.20	1.14	0.58	0.25	0.31	35.7	1.97	-33.8	7.67	-5.6

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2018-4

1811-256-01 5088 1811-256-02 5088 1811-256-03 5091 1811-256-05 5089 1811-256-05 5089	LOCATION SAMPLE DATE	SAMPLE	PH UNITS	EC MMHOICM	% SAT	CALCIUM MEQ/L	MAGNESIUM MEQ/L	SODIUM	SAR	% SAND	% SHT	% CLAY	CLASS	% CACO3	TOT S % SU	SULFATE S% P	PYR S %	ORG S% A	ACID POT N TN/1000TN T	NEUT POT TN/1000TN	A-B POT TN/1000TN	PYR A POT TN/1000TN	PYRS A-B TN/1000TN
	11/28/18	0-1	6.97	6.30	41.7	19.7	56,1	57.9	9.40	40.00	31.25	28.75	сŗ	0:90	0.99	0.54	0.18	0.27	31.1	9.02	-22.1	5.69	3.34
	11/28/18	1-3	6.75	6.79	39.3	19.1	68.5	58.3	8.81	42.50	27.50	30,00	5	0.70	1.15	0.73	0.14	0.29	35.9	7.02	-28.9	4.25	2.77
	11/28/18		5.61	9,08	44.1	19.6	17.6	0.76	13.9	32.50	36.25	31.25	ы	0.30	1.22	0.46	0.36	0.39	38,0	3.01	-35.0	11.3	-8.30
	11/28/18	1-3	6.35	9,10	37.0	20.6	38.3	110	20.3	51.25	25.00	23.75	SCL	1.20	0.81	0.41	0.14	0.25	25.2	12.0	-13.1	4.47	7.5
	11/28/18	0-1	6.12	8.15	38.9	20.6	135	52.6	5.97	41.25	28.75	30.00	or	0.70	1.67	1.04	0.13	0.49	52.1	7.02	-45.1	4.09	2.9
	11/28/18	1-3	4.82	6.53	42.5	19,9	77.5	44.8	6.42	45.00	27.50	27.50	ರ	0.80	1.26	0.76	0.10	0.40	39.3	8,02	-31.3	3.12	4.9
	11/28/18	6-1	7.54	5.21	35.6	21.8	62.9	26.0	4.00	56.25	23.75	20.00	SCL	0.60	0.36	0.27	0.01	0.09	11.2	6.01	-5,19	0.19	5.8
	11/28/18	0-1 Dup	7.48	4.23	35.3	23.6	46.2	16.0	2.70	56.25	23.75	20.00	SCL	0.60	0.33	0.24	0.02	0.07	10.2	6.01	-4.18	0.53	5.4
1811-256-09 5090	11/28/18	1-3	7.27	4.89	33.2	21.1	59.6	20.7	3.27	61.25	21.25	17.50	SL	0.70	0.25	0.18	0.02	0.06	7.9	7.02	-0.92	0.47	6.6
1811-256-10 5110	11/28/18	0-1	6.21	5.93	39.2	21.9	59.6	35.9	5.62	46.25	27.50	26.25	SCL	0.60	1.02	0.61	0.12	0.29	31.7	6.01	-25.7	3.62	2.3
~	11/28/18	5	6.40	5.80	41,5	21.9	68.4	34.3	5,10	47.50	27.50	25.00	SCL	0.60	0.97	0.55	0.10	0.32	30.2	6.01	-24.2	3.12	2.89
	11/28/18	1-3	8.32	6.32	37.5	21.5	72.1	44.4	6,49	46.25	28.75	25.00	-	0:30	0.91	0.56	0.08	0.27	28.3	3.01	-25.3	2.53	0.4
	11/28/18	0-1	5.84	6.51	36.9	35.7	85.8	21.5	2.76	50.00	28.75	21.25	7	0.50	0.70	0.56	0.00	0.14	21.9	5.01	-16.8	0.06	4,9
	11/28/18	0-1 Dup	5.84	6.57	36.8	33.2	89.7	21.3	2.72	52.50	26.25	21.25	SCL	0.40	0.83	0.67	0.01	0,15	25.9	4.01	-21.9	0.22	3.79
	11/28/18	1-3	4.46	4.40	39.9	21.0	104	10.7	1.35	45.00	31.25	23.75	-	<0.001	1.10	0.81	00.00	0.29	34.3	4.01	-38.3	0.03	-4.04
	11/28/18	0-1	7.41	5.57	40.9	35.7	57.8	11.1	1.62	48.75	28.75	22.50	-	2.11	0.59				18.5	21.1	2.51		
	11/28/18	1-3	7,80	4.27	41.5	40.0	24.1	8.48	1.50	52.50	27.50	20.00	SCL	7.02	0.35				11.0	70.2	59.2		
	11/28/18	6-1	7,55	4,26	36.8	31.7	32.0	13.8	2.45	51.25	27.50	21.25	SCL	2.51	0.31				9.53	25.1	15.5		
	11/28/18	1-3	6.88	5.10	39.5	34.2	57.6	12.5	1.85	46.25	28.75	25,00	7	3.01	0.95				29.8	30.1	0.26		
	11/28/18	0-1	6.74	4,34	40.0	28.9	35.8	16.9	2.98	37.50	32.50	30.00	ы	1.70	0.65	0.37	<0.01	0.28	20.2	17.0	-3.15	<0.01	17.0
	11/28/18	0-1	7,88	4.83	33.8	21.9	64.5	16.1	2.46	56.25	26.25	17.50	SL	1.20	0.13				4.08	12.0	7.95		
m	11/28/18	0-1	7.99	4.83	32.5	21.8	64.3	16.0	2.43	56.25	26.25	17.50	SL	1.20	0.13				4.05	12.0	8.0		
	11/28/18	1-3	8.10	5.41	32.7	21.6	91.3	12.4	1.66	60.00	22,50	17,50	SL	1.20	0.20				6.26	12.0	5.768		
	11/28/18	1-3 Dup	8.12	5.82	31.8	22.2	101	14.3	1.82	61.25	22.50	16.25	SL	1,10	0.18				5.68	11.0	5.34		
	11/28/18	0-1	6.53	7.84	38,5	19.3	61.7	57.0	8,95	42.50	27.50	30.00	CL	0.70	0.85	0.50	0.10	0.26	26.7	7.02	-19.7	3.03	3.9
	11/28/18	1-3	8.24	9.78	41.4	18.7	80.8	83,9	11.9	38.75	28.75	32,50	CL	09'0	1.11	0.75	0.07	0.29	34.6	6.01	-28.6	2.06	3,95
	11/28/18	0-1	6,58	7.91	40.7	18.7	63.8	57.9	9.01	38.75	30.00	31.25	CL CL	0.70	1.05	0.62	0.19	0.23	32.7	7.02	-25.7	6.00	1.0
	11/28/18	0-1 Dup	6.56	8.02	40.1	19.3	67.4	57.4	8.72	41.25	28.75	30.00	С	0.60	0.99	0.58	0.16	0.25	30.8	6.01	-24.8	5.00	1.0
	11/28/18	1-3	6.26	8.51	38.2	19,4	83.1	63.9	8,9	43.75	26.25	30.00	С	0.40	1.10	0.69	0.15	0.26	34.3	4.01	-30.3	4.59	-0.5
	11/28/18	6-1	6.54	8.47	36.8	20.5	68.1	69.2	10.4	47.50	26.25	26.25	SCL	0.60	1.02	0.58	0.17	0.27	31.7	6.01	-25.7	5.34	0.6
	11/28/18	1-3	6.46	8.28	35.4	19.9	77.4	61.8	8.86	46:25	27.50	26.25	SCL	0.40	0.88	0.50	0.12	0.25	27.4	4.01	-23.4	3.87	0.1
	11/28/18	0-1	5.52	7.69	36.5	21.2	88.9	41.5	5,59	43.75	28.75	27.50	Ъ	0.20	1.14	0.74	0.08	0.33	35.7	2.01	-33.7	2.37	0-
	11/28/18	0-1 Dup	5.62	7.87	33.6	22.7	91.3	42.9	5.68	45.00	28.75	26.25	-	0.20	1.11	0.75	0.08	0.28	34.7	2.01	-32.7	2.62	-0.6
	11/28/18	1-3	5.94	5,53	38.9	22.5	50.3	25.6	4.24	43.75	27.50	28.75	CL	0:30	1.04	0.50	0.20	0.35	32.5	3.01	-29.5	6.22	-3.5
	11/28/18	1-3	6.68	4.35	47.7	37.9	28.1	7.92	1.38	48.75	27.50	23.75	SCL	3.71	0.83				26.0	37.1	11.1		
	11/28/18	1-0	6.56	6.15	38.7	22.7	47.8	39.1	6.58	40.00	28.75	31.25	G	0.50	96.0	0.59	0.05	0.32	30.1	5.01	-25.0	1.69	3.33
	11/28/18	-1- 1-0	6.33	5.25	37.2	23.3	37.8	35,0	6.34	43.75	28.75	27.50	CL	0.40	0.68	0.37	0.13	0.18	21.4	4.01	-17.3	4.06	-0.0
	11/28/18	5	6.67	4.35	32.7	29.0	31.2	18.9	3.44	56.25	22.50	21.25	SCL	1.30	0.25				7.96	13.0	5.07		
	11/28/18	1-3	3,94	5.50	34.2	24.7	74.3	11.4	1.63	56.25	22.50	21.25	SCL	<0.001	0.89	0,69	0.04	0.16	27.9	-5,01	-32.9	1.22	-6.23
	11/28/18	0-1	6.46	9.55	37.2	22.0	38.8	97.4	1221	40,00	28.75	31.25	СГ	0.70	1.13	0.48	0.36	0.29	35.2	7.02	-28.2	11.2	-4.17
~	11/28/18	0-1	6,48	9,55	37.1	22.5	39.2	98.7	17.8	40.00	28.75	31.25	CL	0.70	1.13	0.43	0.40	0.30	35.2	7.02	-28.2	12.4	-5.42
1811-256-41 5130	11/28/18	0-1 Dup	6,51	8,76	35.2	23.2	39.4	102	18,3	41.25	27.50	31.25	С	0.70	1,14	0.42	0.41	0.31	35.5	7.02	-28.5	12.7	-5.7
1811-256-42 5130	11/28/18	1-3	3.73	11.2	33,6	24.0	277	49.2	4.01	47.50	27.50	25.00	SCL	<0.01	1.31	0.13	0.73	0.46	40.9	-8.02	-48.9	22.8	-30
	11/28/18	0-1	5.88	9.08	33.6	24.0	277	49.2	4.01	47.50	27.50	25.00	SCL	0.20	1.06	0.61	0.15	0.31	33.2	2.01	-31.2	4.72	-2.71
1811-256-44 5129	11/28/18	1-3	6.22	8,45	38.3	22.2	85.6	70.5	9.60	40.00	30.00	30,00	С	0.30	0.94	0.53	0.12	0.29	29.2	3.01	-26.2	3.78	-0.77

PYRS A-B TN/1000TN	2,60	0.81	6.93	-0.72	6.68	5.05	21.0	28.4	-4.31	-2.03	-1.94	9.12	
PYR A POT TN/1000TN	-0.59	-0,81	1,09	1.72	1.34	0.97	-0.97	-0.28	4.31	2.03	1.94	0.91	
A-B POT P	-17.0	-29.0	-23.5	-45.5	-27.5	-18.9	-33,8	-32.7	-36.5	-33.6	-32.5	-4.93	1 45
NEUT POT	2.01	00'0	8.02	1,00	8.02	6.01	20.1	28.1	<0.01	<0.01	<0.01	10.0	19.0
ACID POT NI	19.0	29.0	31.6	46.5	35.5	24.9	53.8	60.7	36.5	33.6	32.5	15.0	17.6
ORG S% TN	0.21	0.21	0.15	0.22	0.16	0.18	0.60	0.73	0.48	0.33	0.34	0.16	
PYR S % 0	<0.01	<0.01	0.04	0.06	0.04	0.03	<0.01	<0.01	0.14	0.07	0.06	0.03	
SULFATE P	0.42	0.75	0.83	1,21	0.94	0.59	1.16	1.23	0.55	0.68	0.64	0.29	
TOTS% S	0.61	0.93	1.01	1.49	1.14	0.80	1.72	1.94	1.17	1.08	1.04	0.48	0.56
% CACO3 T	0.20	0.00	0.80	0.10	0.80	0.60	2.01	2.81	<0.01	<0.01	<0.01	1.00	1 90
CLASS	-	CL	7	SL	CL	0L	CL	CL	-	С	CL	0	C
% CLAY	26.25	27.50	25.00	16.25	27.50	35.00	31.25	30.00	23.75	28,75	30.00	42.50	41 25
% SILT	28.75	27.50	30.00	23.75	31.25	30.00	38.75	37.50	32.50	36.25	35.00	35.00	32.50
% SAND	45.00	45.00	45.00	60.00	41.25	35.00	30.00	32.50	43.75	35.00	35.00	22.50	26.25
SAR	5.58	2.90	9.73	9.30	10.5	8.44	5.18	5.25	10.5	12.0	12.0	16.6	19.3
SODIUM	29.4	31.4	52.2	75.3	57.9	48.7	59.2	63.5	59.6	7.87	80.5	73.1	82.2
MAGNESIUM	30.7	212.3	27.8	100.4	32.7	41.5	238	268	41.8	65.0	68.1	18.0	16.1
CALCIUM	25.0	21.9	29.8	30.5	27.6	25.1	23.4	24.4	22.4	20.5	21.5	20.8	20.1
% SAT	33.0	36.7	33.9	33.1	34.1	42.2	39.3	41.4	39.3	36.5	37.5	46.4	45.9
EC MMHO/CM	4,96	8,56	6.23	9.07	6.56	6.11	10.8	11.3	6.81	8,48	8.45	7.22	7.90
PH UNITS	5,49	4.90	6.28	4.86	6.34	6.44	7.95	7.97	5.33	6.21	6.25	7.40	7.30
SAMPLE DEPTH	0-1	1-3	1-0	1-3	0-1 Dup	6-1	1.3	1-3 Dup	1-0	1-3	1-3	5-1	1-3
SAMPLE DATE	11/28/18	11/28/18	11/28/18	11/28/18	11/28/18	11/28/18	11/28/18	11/28/18	11/28/18	11/28/18	11/28/18	11/28/18	11/28/18
LOCATION	4436	4436	4435	4435	4435	4447	4447	4447	4446	4446	4446	4457	4457
GAL#	1811-257-01	1811-257-02	1811-257-03	1811-257-04	1811-257-05	811-257-06	811-257-07	1811-257-08	1811-257-09	811-257-10	1811-257-10R	1811-257-11	1811-257-12

2018-6

Sample Site ID as	Sample Site ID as		Year	Mitigation	
Shown on Map	Listed on Laboratory	Year	Reported to	Thickness**	Attachment Page for
2.2.1*	Data Sheet	Sampled	OSMRE	(feet)	Laboratory Data
1	2225 61RG	2012	2013	2	2012-1
8	2185 61RG	2012	2013	4	2012-1
9	2182 61RG	2012	2013	4	2012-1
10	2181 61RG	2012	2013	2	2012-1
2404*	61RG9	2010	2011	1	2010-1
2430	61RG15	2011	2012	1	2011-1
2431	2183 61RG	2012	2013	4	2012-1
2432	2184 61RG	2012	2013	1	2012-1
2434	61RG23	2011	2012	4	2011-1
2435	61RG22	2011	2012	4	2011-1
2458	2167	2014	2015	4	2014-3
2465	2190 60RG	2012	2013	4	2012-1
2468	J19 2468	2016	2017	2	2016-6
2469	2168 60RG	2012	2013	4	2012-1
2470	2166 60RG	2012	2013	2	2012-1
2471	2147 60RG	2012	2013	4	2012-1
2472	2146 60RG	2012	2013	2	2012-1
2480	2165	2014	2015	4	2014-3
2481	2164 61RG	2012	2013	2	2012-1
2672	J19 1964	2013	2014	4	2013-1
2675	J19 1982	2013	2014	1	2013-1
2690	1941	2014	2015	1	2014-1
2702	2017	2014	2015	1	2014-3
2711 2715	2036 2051	2014 2014	2015 2015	4 1	2014-3
2715	2051	2014 2014	2015	2	2014-3 2014-4
2710	2052	2014	2015	2	2014-4
2717	2055	2014	2015	4	2014-1
2720	2030	2014	2015	4	2014-3
2723	2072	2014	2015	1	2014-1
2724	2072	2014	2015	4	2014-1
2725	2073	2014	2015	+ 1	2014-4
2730	2091	2014	2015	4	2014-4
2734	2092	2014	2015	4	2014-3
2734	2109	2014	2015	<u>د</u> 1	2014-3
2737	2103	2014	2015	1	2014-1
2738	2110	2014	2015	1	2014-3
2741	2128	2014	2015	1	2014-3
2742	2129	2014	2015	, 1	2014-3
2743	2120	2014	2015	1	2014-3
2746	2148	2014	2015	1	2014-3
2747	2149	2014	2015	2	2014-3
2748	2150	2014	2015	2	2014-3
2749	1958	2014	2015	4	2014-3

Laboratory Data Used to Evaluate Spoil Suitability and Determine Mitigation Thickness Values for the J19W Coal Resource Area (June 2020)

Sample Site ID as	Sample Site ID as		Year	Mitigation	
Shown on Map	Listed on Laboratory	Year	Reported to	-	Attachment Page for
2.2.1*	Data Sheet	Sampled	OSMRE	(feet)	Laboratory Data
2750	1959	2014	2015	3	2014-1
2751	1960	2014	2015	4	2014-1
2752	1961	2014	2015	1	2014-3
2753	1962	2014	2015	1	2014-1
4225	J19 4225	2016	2017	1	2016-6
4226	J19 4226	2016	2017	2	2016-6
4227	J19 4227	2016	2017	4	2016-6
4228	J19 4228	2016	2017	4	2016-6
4230	J19 4230	2016	2017	1	2016-6
4231	J19 4231	2016	2017	2	2016-6
4232	J19 4232	2016	2017	1	2016-6
4233	J19 4233	2016	2017	2	2016-6
4234	J19 4234	2016	2017	2	2016-6
4235	J19 4235	2016	2017	2	2016-6
4238	J19 4238	2016	2017	1	2016-6
4239	J19 4239	2016	2017	2	2016-6
4240	J19 4240	2016	2017	3	2016-6
4244	J19 4244	2016	2017	1	2016-6
4245	J19 4245	2016	2017	3	2016-6
4246	J19 4246	2016	2017	2	2016-6
4252	J19 4252	2016	2017	2	2016-6
4253	J19 4253	2016	2017	2	2016-6
4254	J19 4254	2016	2017	1	2016-6
4260	J19 4260	2016	2017	3	2016-6
4261	J19 4261	2016	2017	4	2016-6
4262	J19 4262	2016	2017	1	2016-6
4269	J19 4269	2016	2017	2	2016-6
4270	J19 4270	2016	2017	1	2016-6
4274	58-1963	2015	2016	1	2015-2
4275	J19 4275	2016	2017	1	2016-6
4276	J19 4276	2016	2017	2	2016-6
4277	J19 4277	2016	2017	1	2016-6
4435	4435	2018	2019	1	2018-6
4436	4436	2018	2019	1	2018-6
4446	4446	2018	2019	2	2018-6
4447	4447	2018	2019	1	2018-6
4448	J19 4448	2016	2017	1	2016-6
4457	4457	2018	2019	1	2018-6

* Sites denoted with an asterisk (*) have not been topsoiled nor has suitable spoil or red rock been applied. ** Per the Sampling Results and Redistribution section of the annual reports (1999, 2002-2006, 2010-2018), suitable plant growth material (weathered overburden, residual soils, and spoil) was used as subsoil and substratum to bury unsuitable spoil prior to topsoil replacement and for areas requiring erosion resistant material.

Sample Site ID as	Sample Site ID as		Year	Mitigation	
Shown on Map	Listed on Laboratory	Year	Reported to	Thickness**	Attachment Page for
2.2.1*	Data Sheet	Sampled	OSMRE	(feet)	Laboratory Data
922	58RG24	1999	2000) 1 1999-1	
1674	45RG26	2002	2003	1	2002-1
1816	46RG33	2003	2004	4	2003-1
1818	46RG35	2003	2004	4	2003-1
1891	43RG13	2004	2005	2	2004-1
2175	41RG14	2005	2006	1	2005-1
2177	41RG17	2005	2006	4	2005-1
2178	45RG33	2005	2006	1	2005-1
2179	45RG32	2005	2006	1	2005-1
2180	45RG34	2005	2006	1	2005-1
2181	45RG36	2005	2006	1	2005-1
2182	45RG35	2005	2006	1	2005-1
2205	41RG18	2005	2006	1	2005-2
2527	41RG21	2006	2007	1	2006-1
2528	41RG20	2006	2007	1	2006-1
2529	41RG19	2006	2007	1	2006-1
2771*	200	2014	2015	1	2014-3
2780*	298	2014	2015	2	2014-1
2781*	299	2014	2015	2	2014-1
2782*	438	2014	2015	1	2014-1
2783*	2081	2014	2015	1	2014-1
2784	580	2014	2015	2	2014-3
2814*	56-123	2014	2015	1	2014-6
2816*	56-125	2014	2015	1	2014-6
2818*	56-128	2014	2015	2	2014-6
2820*	56-2820	2016	2017	1	2016-1
2829*	56-2829	2016	2017	1	2016-1
2832*	2832	2017	2018	1	2017-5
2833	2833	2017	2018	1	2017-3
2834	2834	2017	2018	1	2017-3
2837	2837	2017	2018	1	2017-3
2838*	2838	2017	2018	1	2017-5
2844*	56-2844	2015 2015	2016 2016	4	2015-5
2855	46-221			1	2015-3
2856* 2862*	2856	2017	2018	1	2017-5
2862*	57-2862	2016	2017	1	2016-1
2864* 2865*	57-2864	2016 2016	2017 2017	4 3	2016-1
2865*	57-2865 57-297	2016	2017 2016	3 4	2016-1 2015-2
2867*		2015	2016	4 1	2015-2 2016-1
2867*	57-2867	2016	2017 2016	1	2016-1 2015-2
2868***********************************	57-303 56-2876	2015 2016	2016 2017	1	2015-2 2016-2
		2016 2017	2017 2018	4	2016-2 2017-3
2902	2902			1	
2904	2904	2017	2018	4	2017-3

Sample Site ID as	Sample Site ID as		Year	Mitigation	
Shown on Map	Listed on Laboratory	Year	Reported to	Thickness**	Attachment Page for
2.2.1*	Data Sheet	Sampled	OSMRE	(feet)	Laboratory Data
2905	2905	2017	2018	2	2017-3
2907	2907	2017	2018	3	2017-3
2908	2908	2017	2018	2	2017-3
2910	2910	2017	2018	4	2017-3
2913*	56-354	2014	2015	1	2014-6
2914*	56-355	2014	2015	1	2014-6
2917*	56-358	2014	2015	2	2014-6
2918*	56-2918	2016	2017	1	2016-1
2923*	56-364	2014	2015	1	2014-6
2925*	56-366	2014	2015	1	2014-6
2927*	56-368	2014	2015	1	2014-6
2936	2936	2017	2018	1	2017-3
2938	2938	2017	2018	1	2017-3
2940	46-381	2017	2016	1	2017-3
2945*	2945	2013	2010	3	2018-1
2945	62-2950	2018	2019	1	2016-1
2950	62-393	2010	2017	2	2015-2
2951 2994*	57-2994	2015	2018	2	2015-2
2994 2995*			2017	2	
	57-437	2015			2015-2
2996*	57-2996	2016	2017	1	2016-1
2997*	57-440	2015	2016	1	2015-2
3022	3022	2017	2018	4	2017-3
3023	3023	2017	2018	4	2017-3
3026	3026	2017	2018	1	2017-3
3040	J19 3040	2017	2018	1	2017-1
3048	J19 3048	2017	2018	2	2017-1
3049	J19 3049	2017	2018	4	2017-1
3050	3050	2017	2018	2	2017-3
3051	3051	2017	2018	2	2017-3
3052	3052	2017	2018	4	2017-4
3053	3053	2017	2018	1	2017-4
3054	3054	2017	2018	1	2017-3
3058	3058	2016	2017	1	2016-3
3059	J19 3059	2017	2018	1	2017-1
3060*	J19 3060	2017	2018	3	2017-1
3061	J19 3061	2017	2018	1	2017-1
3062	J19 3062	2017	2018	4	2017-1
3063	J19 3063	2017	2018	3	2017-1
3064	J19 3064	2017	2018	1	2017-1
3066	J19 3066	2017	2018	1	2017-1
3068	3068	2017	2018	1	2017-4
3069	3069	2017	2018	1	2017-4
3070	3070	2017	2018	1	2017-4
3075	3075	2016	2017	1	2016-3
3076	3076	2016	2017	1	2016-3

Laboratory Data Used to Evaluate Spoil Suitability and Determine Mitigation Thickness Values for the J19 Coal Resource Area (June 2020)

Sample Site ID as	Sample Site ID as		Year	Mitigation	
Shown on Map	Listed on Laboratory	Year	Reported to	Thickness**	Attachment Page for
2.2.1*	Data Sheet	Sampled	OSMRE	(feet)	Laboratory Data
3077	J19 3077	2017	2018	3	2017-1
3162	J19 3162	2017	2018	1	2017-1
3163	J19 3163	2017	2018	1	2017-1
3164	J19 3164	2017	2018	1	2017-1
3165	J19 3165	2017	2018	1	2017-1
3166	J19 3166	2017	2018	1	2017-2
3167	J19 3167	2017	2018	1	2017-2
3168	41-619	2014	2015	2	2014-8
3169	41-620	2014	2015	1	2014-8
3170	43-621	2014	2015	1	2014-8
3171	43-622	2014	2015	1	2014-8
3173	3173	2017	2018	1	2017-4
3185	3185	2017	2018	1	2017-4
3186*	3186	2017	2018	1	2017-4
3187*	3187	2017	2018	1	2017-4
3188*	3188	2017	2018	1	2017-4
3189*	3189	2017	2018	1	2017-4
4241*	57-2100	2015	2016	1	2015-2
4242*	57-2101	2015	2016	1	2015-2
4248	62-2119	2015	2016	1	2015-2
4249*	62-2120	2015	2016	1	2015-2
4250*	62-2121	2015	2016	1	2015-2
4256*	4256	2018	2019	1	2018-1
4257	62-2138	2015	2016	1	2015-2
4258*	62-2139	2015	2016	2	2015-2

* Sites denoted with an asterisk (*) have not been topsoiled nor has suitable spoil or red rock been applied. ** Per the Sampling Results and Redistribution section of the annual reports (1999, 2002-2006, 2010-2018), suitable plant growth material (weathered overburden, residual soils, and spoil) was used as subsoil and substratum to bury unsuitable spoil prior to topsoil replacement and for areas requiring erosion resistant material.

Sample Site ID as	Sample Site ID as		Year	Mitigation	
Shown on Map	Listed on Laboratory	Year	Reported to	Thickness**	Attachment Page for
2.2.2*	Data Sheet	Sampled	OSMRE	(feet)	Laboratory Data
2493	3123-N9	2012	2013	4	2012-2
2494	3127-N9	2012	2013	1	2012-2
2495	3331-N9	2012	2013	2	2012-2
2658	N9-3120	2013	2014	1	2013-1
2659	N9-3121	2013	2014	4	2013-1
2660	N9-3126	2013	2014	2	2013-1
2661	N9-3330	2013	2014	1	2013-1
2680	3015	2014	2015	1	2014-2
2681	2965	2014	2015	4	2014-2
2682	2991	2014	2015	4	2014-2
2683	2911	2014	2015	1	2014-2
2684	2881	2014	2015	1	2014-2
2685	2910	2014	2015	4	2014-2
2686	2990	2014	2015	1	2014-2
2687	2937	2014	2015	1	2014-2
2688 2792	2992 2909	2014 2014	2015 2015	2 4	2014-2 2014-5
2792 2793	2909 2935	2014	2015	4 2	2014-5 2014-5
2793	2935	2014	2015	2	2014-5
2795	2938	2014	2015	1	2014-5
2796	2963	2014	2015	4	2014-5
2797	2964	2014	2015	1	2014-5
2798	2988	2014	2015	2	2014-5
2799	2989	2014	2015	1	2014-5
3493	24-3493	2016	2017	3	2016-2
3494	24-3494	2016	2017	3	2016-2
4286	24-4286	2016	2017	1	2016-2
4287	24-4287	2016	2017	4	2016-2
4321	24-4321	2016	2017	1	2016-2
4322	24-4322	2016	2017	1	2016-2
4323	24-4323	2016	2017	4	2016-2
4342	25-4342	2016	2017	4	2016-2
4343	25-2332	2015	2016	1	2015-1
4344*	25-2333	2015	2016	3	2015-1
4345	25-2334	2015	2016	1	2015-1
4346	25-2335	2015	2016	1	2015-1
4375*	25-4375	2016	2017	2	2016-2
4376*	25-2365	2015	2016	2	2015-1
4377*	25-2366	2015	2016	4	2015-1
4378*	25-2367	2015	2016	1	2015-1
4493	4493	2018	2019	1	2018-1
4494	4494	2018	2019	4	2018-1
4495	4495	2018	2019	1	2018-2
4496	4496	2018	2019	3	2018-2

Sample Site ID as	Sample Site ID as		Year	Mitigation	
Shown on Map	Listed on Laboratory	Year	Reported to	Thickness**	Attachment Page for
2.2.2*	Data Sheet	Sampled	OSMRE	(feet)	Laboratory Data
4531	4531	2017	2018	4	2017-7
4532	4532	2017	2018	4	2017-6
4533	4533	2016	2017	3	2016-3
4534	4534	2018	2019	1	2018-2
4535	25-4535	2016	2017	1	2016-2
4536	N9 4536	2016	2017	1	2016-4
4569	N9 4569	2016	2017	4	2016-4
4570	4570	2016	2017	1	2016-3
4571	4571	2018	2019	1	2018-2
4572	26-2516	2015	2016	2	2015-4
4573	26-2517	2015	2016	3	2015-4
4574	25-2518	2015	2016	4	2015-4
4575	25-2519	2015	2016	1	2015-4
4605	4605	2016	2017	4	2016-3
4606	4606	2016	2017	4	2016-3
4607	26-2551	2015	2016	1	2015-4
4608	26-2552	2015	2016	1	2015-4
4609	4609	2016	2017	1	2016-3
4610	26-2554	2015	2016	1	2015-4
4611	26-2555	2015	2016	1	2015-4
4612	26-2556	2015	2016	1	2015-4
4613	25-2557	2015	2016	1	2015-4
4614	N9 4614	2016	2017	1	2016-4
4643*	4643	2016	2017	1	2016-3
4644*	4644	2018	2019	4	2018-4
4645	26-2589	2015	2016	1	2015-4
4646	26-2590	2015	2016	3	2015-4
4647	26-2591	2015	2016	3	2015-4
4648	26-2592	2015	2016	1	2015-4
4649	26-2593	2015	2016	4	2015-4
4650	26-2594	2015	2016	1	2015-4
4651	4651	2013	2018	1	2017-6
4681*	26-4681	2017	2016	3	2017-0
4682	4682	2013	2018	4	2013-3
4683	4683	2017	2018	1	2017-7
4684	26-2628	2017	2016	1	2015-4
4685	26-2629	2015	2016	1	2015-4
4686	26-2629	2015	2016	1	2015-4
4687	26-2630	2015	2016	3	2015-4
4688	4688	2013	2018	1	2013-4
4000	26-4715	2017	2018	4	2017-0
4715	4716	2015	2018	4	2013-5
4716 4717	4716	2017 2017	2018	4	2017-6
4717 4718	4717	2017 2017	2018	3	2017-6
				3 1	
4719*	N9 4719	2016	2017	I	2016-5

Sample Site ID as	Sample Site ID as		Year	Mitigation	
Shown on Map	Listed on Laboratory	Year	Reported to	Thickness**	Attachment Page for
2.2.2*	Data Sheet	Sampled	OSMRE	(feet)	Laboratory Data
4720*	26-2664	2015	2016	3	2015-4
4721	4721	2017	2018	1	2017-6
4722	4722	2017	2018	3	2017-6
4748	4748	2017	2018	1	2017-7
4749	4749	2017	2018	1	2017-7
4750*	4750	2017	2018	1	2017-7
4752	4752	2017	2018	1	2017-7
4753	4753	2017	2018	1	2017-6
4776*	26-2720	2015	2016	2	2015-1
4902	25-4902	2016	2017	1	2016-2
4903	25-2847	2015	2016	3	2015-1
4904	25-2848	2015	2016	1	2015-1
4905	25-2849	2015	2016	1	2015-1
4906	25-2850	2014	2015	2	2014-7
4907	25-2851	2014	2015	1	2014-7
4932	25-4932	2016	2017	1	2016-2
4933	25-2877	2015	2016	1	2015-1
4934	25-2878	2015	2016	1	2015-1
4935	25-2879	2015	2016	1	2015-1
4936	25-2880	2014	2015	2	2014-7
4960	N9 4960	2016	2017	1	2016-5
4961	25-2906	2015	2016	1	2015-1
4962	25-2907	2015	2016	1	2015-1
4963	25-2908	2015	2016	1	2015-1
4988	N9 4988	2016	2017	1	2016-5
4989	24-4989	2016	2017	1	2016-2
4990	24-4990	2016	2017	1	2016-2
5016	N9 5016	2016	2017	1	2016-5
5017	24-5017	2016	2017	2	2016-2
5018	24-5018	2016	2017	1	2016-2
5019	24-2962	2015	2016	3	2015-1
5020*	5020	2017	2018	4	2017-5
5021*	5021	2017	2018	1	2017-5
5044	24-5044	2016	2017	1	2016-2
5045*	5045	2017	2018	2	2017-5
5046*	5046	2018	2019	1	2018-5
5064*	5064	2017	2018	1	2017-7
5065*	5065	2017	2018	1	2017-7
5066*	5066	2017	2018	1	2017-7
5067	24-3016	2014	2015	1	2014-7
5068	5068	2017	2018	1	2017-5
5069*	5069	2017	2018	4	2017-5
5070*	5070	2018	2019	1	2018-5
5071*	5071	2018	2019	1	2018-5
5087*	5087	2018	2019	1	2018-3

Sample Site ID as	Sample Site ID as		Year	Mitigation	
Shown on Map	Listed on Laboratory	Year	Reported to	Thickness**	Attachment Page for
2.2.2*	Data Sheet	Sampled	OSMRE	(feet)	Laboratory Data
5088*	5088	2018	2019	1	2018-5
5089*	5089	2018	2019	1	2018-5
5090*	5090	2018	2019	1	2018-5
5091*	5091	2018	2019	4	2018-5
5092*	5092	2018	2019	1	2018-2
5093*	5093	2018	2019	1	2018-2
5094*	5094	2018	2019	1	2018-5
5095*	N9 5095	2017	2018	3	2017-1
5110*	5110	2018	2019	1	2018-5
5111*	5111	2018	2019	1	2018-5
5112*	5112	2018	2019	1	2018-5
5113*	5113	2018	2019	1	2018-5
5114*	5114	2018	2019	2	2018-2
5115*	5115	2018	2019	1	2018-5
5126*	5126	2018	2019	3	2018-1
5127*	5127	2018	2019	1	2018-5
5129*	5129	2018	2019	2	2018-5
5130*	5130	2018	2019	3	2018-5
5131*	5131	2018	2019	3	2018-5
5132*	5132	2018	2019	1 4	2018-5
5142*	5142	2018	2019	4	2018-1
* Sites denoted wit	h an asterisk (*) have not	been topsoil	ed nor has suita	able spoil or red	d rock been applied. **
	g Results and Redistribution			•	••
	owth material (weathered				
	insuitable spoil prior to top				

KAYENTA MINE PHASE I BOND RELEASE WATERSHED & CHANNEL DESIGNS J19

TABLE J19-2020 Channel Design Summary

						C	Channel J19-	13W						
						Typical	Rip Rap Line	ed Channel						
				Ĩ			Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-13W	3.12	11.40	28	3	0.1	2.25	1	1.1	N/A	-	5.0	0.034	80	A
											1			

Design Flow: 10-year, 6-hour Storm

J19-13W WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033 1

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

	Siluciule Networking.											
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description						
Null	#1	==>	End	0.000	0.000	J19-13W WATERSHED						

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	5.000	5.000	3.12	0.14

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-13W WATERSHED

					<u> </u>	33			
Stru #	SWS #	SWS Area	Time of Conc	Musk K	Musk X	Curve	UHS	Peak Discharge	Runoff Volume
#	# # (ac) (hrs) (h	(hrs)		Number		(cfs)	(ac-ft)		
#1	1	5.000	0.034	0.000	0.000	80.000	М	3.12	0.139
	Σ	5.000						3.12	0.139

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	6. Grassed waterway	17.16	70.00	408.00	6.210	0.018
		8. Large gullies, diversions, and low flowing streams	11.44	70.00	612.00	10.140	0.016
#1	1	Time of Concentration:					0.034

J19-13W CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
28.00	3.0:1	3.0:1	11.4	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard		
Design Discharge:	3.12 cfs			
Depth:	0.05 ft	1.05 ft		
Top Width:	28.30 ft	34.30 ft		
Velocity:	2.25 fps			
X-Section Area:	1.39 sq ft			
Hydraulic Radius:	0.049 ft			
Froude Number:	1.79			

TABLE J19-2020 Channel Design Summary

						C	Channel J19-	14W						
	Typical Rip Rap Lined Channel													
				[Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-14W	8.58	7.10	12	3	0.2	3.98	1	1.2	N/A	GRAVEL	21.8	0.098	75	А

Design Flow: 10-year, 6-hour Storm

J19-14W WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

	Siluciule Networking.										
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description					
Null	#1	==>	End	0.000	0.000	J19-14W WATERSHED					

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	21.800	21.800	8.58	0.37

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-14W WATERSHED

					<u> </u>	33			
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	21.800	0.098	0.000	0.000	75.000	М	8.58	0.368
	Σ	21.800						8.58	0.368

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	6. Grassed waterway	8.83	106.00	1,200.00	4.450	0.074
		8. Large gullies, diversions, and low flowing streams	7.08	50.00	706.00	7.980	0.024
#1	1	Time of Concentration:					0.098

J19-14W CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
12.00	3.0:1	3.0:1	7.1	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard		
Design Discharge:	8.58 cfs			
Depth:	0.17 ft	1.17 ft		
Top Width:	13.03 ft	19.03 ft		
Velocity:	3.98 fps			
X-Section Area:	2.16 sq ft			
Hydraulic Radius:	0.165 ft			
Froude Number:	1.72			

TABLE J19-2020 Channel Design Summary

		Channel J19-15W												
Typical Rip Rap Lined Channel														
	Designe	d		As-Built										
m Side Slope Depth	Velocity Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design						
ft) H:1 (ft) Flow (ft	t) (fps) Board (f) Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number							
3 0.1	4.48 1	1.1	N/A	-	10.1	0.058	81	А						
	(ft) H:1 (ft) Flow (ft	om Side Slope Depth Velocity Free (ft) H:1 (ft) Flow (ft) (fps) Board (ft	(ft) H:1 (ft) Flow (ft) (fps) Board (ft) Depth (ft)	om Side Slope Depth Velocity Free Total Rip Rap (ft) H:1 (ft) Flow (ft) (fps) Board (ft) Depth (ft) (in)	om Side Slope Depth Velocity Free Total Rip Rap Rip Rap (ft) H:1 (ft) Flow (ft) (fps) Board (ft) Depth (ft) (in) (in)	om Side Slope Depth Velocity Free Total Rip Rap Rip Rap Watershed (ft) H:1 (ft) Flow (ft) (fps) Board (ft) Depth (ft) (in) (in) (acres)	om Side Slope Depth Velocity Free Total Rip Rap Rip Rap Watershed Time of (ft) H:1 (ft) Flow (ft) (fps) Board (ft) Depth (ft) (in) (in) (acres) Concentration (hr)	om Side Slope Depth Velocity Free Total Rip Rap Rip Rap Watershed Time of Curve (ft) H:1 (ft) Flow (ft) (fps) Board (ft) Depth (ft) (in) (in) (acres) Concentration (hr) Number						

Design Flow: 10-year, 6-hour Storm

J19-15W WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

	Siluciule Networking.											
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description						
Null	#1	==>	End	0.000	0.000	J19-15W WATERSHED						

#1 Null

Structure Networking:



	Immediate Contributing Area	Total Contributing Area	Peak Discharge (cfs)	Total Runoff Volume
	(ac)	(ac)	(0.0)	(ac-ft)
#1	10.100	10.100	6.81	0.31

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-15W WATERSHED

					J	55			
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Runoff Discharge Volume (cfs) (ac-ft)	
#1	1	10.100	0.058	0.000	0.000	81.000	М	6.81	0.308
	Σ	10.100						6.81	0.308

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	6. Grassed waterway	10.54	86.00	816.00	4.860	0.046
		8. Large gullies, diversions, and low flowing streams	16.78	95.00	566.00	12.290	0.012
#1	1	Time of Concentration:					0.058

J19-15W CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
14.00	3.0:1	3.0:1	16.8	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	6.81 cfs	
Depth:	0.11 ft	1.11 ft
Top Width:	14.64 ft	20.64 ft
Velocity:	4.48 fps	
X-Section Area:	1.52 sq ft	
Hydraulic Radius:	0.103 ft	
Froude Number:	2.45	

1

TABLE J19-2020 Channel Design Summary

	Channel J19-16W													
	Typical Rip Rap Lined Channel													
							Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-16W	13.15	13.10	14	3	0.2	5.36	1	1.2	GRAVEL	GRAVEL	19.5	0.073	81	В

Design Flow: 10-year, 6-hour Storm

J19-16W WATERSHED DESIGN (10Y-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description					
Null	#1 ==> E		End	0.000 0.000		J19-16W WATERSHED					

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	19.500	19.500	13.15	0.59

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-16W WATERSHED

					<u> </u>	33			
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	19.500	0.073	0.000	0.000	81.000	М	13.15	0.595
	Σ	19.500						13.15	0.595

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	6. Grassed waterway	5.87	45.00	766.00	3.630	0.058
		8. Large gullies, diversions, and low flowing streams	13.13	78.00	594.00	10.870	0.015
#1	1	Time of Concentration:					0.073

J19-16W GRAVEL CHANNEL DESIGN (13.1%)

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
14.00	3.0:1	3.0:1	13.1	0.0300	1.00			5.5

	w/o Freeboard	w/ Freeboard		
Design Discharge:	13.15 cfs			
Depth:	0.17 ft	1.17 ft		
Top Width:	15.01 ft	21.01 ft		
Velocity:	5.36 fps			
X-Section Area:	2.45 sq ft			
Hydraulic Radius:	0.163 ft			
Froude Number:	2.34			

TABLE J19-2020 Channel Design Summary

	Channel J19-9W													
	Typical Rip Rap Lined Channel													
					Designed As-Built									
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-9W	19.31	9.80	16	3	0.2	5.41	1	1.2	GRAVEL	3	33.6	0.090	79	В
											J			

Design Flow: 10-year, 6-hour Storm

J19-9W WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description					
Null	#1 ==>		End	0.000	0.000	J19-9W WATERSHED					

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)		Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	33.600	33.600	19.31	0.85

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-9W WATERSHED

					J	33			
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	33.600	0.090	0.000	0.000	79.000	М	19.31	0.853
	Σ	33.600						19.31	0.853

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	6. Grassed waterway	6.28	35.00	557.00	3.760	0.041
		8. Large gullies, diversions, and low flowing streams	9.81	165.00	1,682.00	9.390	0.049
#1	1	Time of Concentration:					0.090

J19-9W GRAVEL CHANNEL DESIGN (9.8%)

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
16.00	3.0:1	3.0:1	9.8	0.0300	1.00			5.5

	w/o Freeboard	w/ Freeboard
Design Discharge:	19.30 cfs	
Depth:	0.21 ft	1.21 ft
Top Width:	17.29 ft	23.29 ft
Velocity:	5.41 fps	
X-Section Area:	3.57 sq ft	
Hydraulic Radius:	0.205 ft	
Froude Number:	2.10	

TABLE J19-2020 Channel Design Summary

	Channel J19-11W													
	Typical Rip Rap Lined Channel													
				Ĩ			Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-11W	14.17	12.00	16	3	0.2	5.12	1	1.2	GRAVEL	3	21.0	0.051	81	В

Design Flow: 10-year, 6-hour Storm

J19-11W WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

Siluciule Networking.									
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description			
Null	#1	==>	End	0.000	0.000	J19-11W WATERSHED			

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	21.000	21.000	14.17	0.64

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-11W WATERSHED

					<u> </u>	35			
Stru #	SWS #	SWS Area	Time of Conc	Musk K	Musk X	Curve	UHS	Peak Discharge	Runoff Volume
"	"	(ac)	(hrs)	(hrs)		Number		(cfs)	(ac-ft)
#1	1	21.000	0.051	0.000	0.000	81.000	М	14.17	0.640
	Σ	21.000						14.17	0.640

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	6. Grassed waterway	6.17	10.00	162.00	3.720	0.012
		8. Large gullies, diversions, and low flowing streams	11.98	175.00	1,461.00	10.380	0.039
#1	1	Time of Concentration:					0.051

J19-11W GRAVEL CHANNEL DESIGN (12.0%)

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
16.00	3.0:1	3.0:1	12.0	0.0300	1.00			5.5

	w/o Freeboard	w/ Freeboard
Design Discharge:	14.17 cfs	
Depth:	0.17 ft	1.17 ft
Top Width:	17.01 ft	23.01 ft
Velocity:	5.12 fps	
X-Section Area:	2.77 sq ft	
Hydraulic Radius:	0.162 ft	
Froude Number:	2.24	

TABLE J19-2020

Channel	Design	Summary	
Charmon	Congri	Caninary	

						Cha	innel J19-2W	.1C.1D						
						Typical	Rip Rap Line	ed Channel						
				[Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-2W.1C.1D	8.67	2.40	35	3	0.1	1.93	1	1.1	N/A	GRAVEL	22.9	0.164	81	А

Design Flow: 10-year, 6-hour Storm

J19-2W.1C.1D WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

	Siluciule Networking.									
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description				
Null	#1	==>	End	0.000	0.000	J19-2W.1C.1D WATERSHED				

#1 Null

Structure Networking:



3

	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	22.900	22.900	8.67	0.57

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-2W.1C.1D WATERSHED

					J	33			
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	22.900	0.164	0.000	0.000	81.000	М	8.67	0.570
	Σ	22.900						8.67	0.570

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	6. Grassed waterway	1.01	5.00	494.00	1.500	0.091
		8. Large gullies, diversions, and low flowing streams	2.44	30.00	1,230.00	4.680	0.073
#1	1	Time of Concentration:					0.164

J19-2W.1C.1D CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
35.00	3.0:1	3.0:1	2.4	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	8.67 cfs	
Depth:	0.13 ft	1.13 ft
Top Width:	35.76 ft	41.76 ft
Velocity:	1.93 fps	
X-Section Area:	4.49 sq ft	
Hydraulic Radius:	0.126 ft	
Froude Number:	0.96	

TABLE J19-2020 Channel Design Summary

						Ch	annel J19-1(DW.1C						
						Typical	Rip Rap Line	ed Channel						
				[Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-10W.1C	9.04	7.00	20	3	0.1	3.36	1	1.1	N/A	3	27.0	0.233	81	А
i									I					
1														

Design Flow: 10-year, 6-hour Storm

J19-10W.1C WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II			
Design Storm:	10 yr - 6 hr			
Rainfall Depth:	1.600 inches			

	Siluciule Networking.										
Туре		Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description				
Null		#1	==>	End	0.000	0.000	J19-10W.1C WATERSHED				

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	27.000	27.000	9.04	0.67

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-10W.1C WATERSHED

					<u> </u>	33			
Stru #	SWS #	SWS Area	Time of Conc	Musk K	Musk X	Curve Musk X Number	UHS		Runoff Volume
"	"	(ac)	(hrs)	(hrs)				(cfs)	(ac-ft)
#1	1	27.000	0.233	0.000	0.000	81.000	М	9.04	0.666
	Σ	27.000						9.04	0.666

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	2.90	22.00	759.00	1.360	0.155
		6. Grassed waterway	9.20	110.00	1,196.00	4.540	0.073
		8. Large gullies, diversions, and low flowing streams	6.99	10.00	143.00	7.930	0.005
#1	1	Time of Concentration:					0.233

J19-10W.1C CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
20.00	3.0:1	3.0:1	7.0	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	9.04 cfs	
Depth:	0.13 ft	1.13 ft
Top Width:	20.79 ft	26.79 ft
Velocity:	3.36 fps	
X-Section Area:	2.69 sq ft	
Hydraulic Radius:	0.129 ft	
Froude Number:	1.64	

TABLE J19-2020 Channel Design Summary

						(Channel J19-	12W						
						Typical	Rip Rap Line	ed Channel						
				Ĩ			Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-12W	2.57	7.00	18	3	0.1	2.13	1	1.1	N/A	3	11.9	0.133	76	A
											_			

Design Flow: 10-year, 6-hour Storm

J19-12W WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

	Siluciule Networking.								
Ту	vpe	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description		
Nu	الد	#1	==>	End	0.000	0.000	J19-12W WATERSHED		

#1 Null

Structure Networking:



	Immediate Contributing Area	Total Contributing Area	Peak Discharge (cfs)	Total Runoff Volume
	(ac)	(ac)	(013)	(ac-ft)
#1	11.900	11.900	2.57	0.18

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-12W WATERSHED

					<u> </u>	55			
Stru #	SWS #	SWS Area (ac)	Time of Conc	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge	Runoff Volume
		(ac)	(hrs)	(1113)		Number		(cfs)	(ac-ft)
#1	1	11.900	0.133	0.000	0.000	76.000	М	2.57	0.183
	Σ	11.900						2.57	0.183

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	6.07	40.00	659.00	1.970	0.092
		6. Grassed waterway	6.80	10.00	147.00	3.910	0.010
		8. Large gullies, diversions, and low flowing streams	6.99	62.00	887.00	7.930	0.031
#1	1	Time of Concentration:					0.133

J19-12W CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
18.00	3.0:1	3.0:1	7.0	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	2.57 cfs	
Depth:	0.07 ft	1.07 ft
Top Width:	18.40 ft	24.40 ft
Velocity:	2.13 fps	
X-Section Area:	1.20 sq ft	
Hydraulic Radius:	0.065 ft	
Froude Number:	1.47	

TABLE J19-2020 Channel Design Summary

						Ch	annel J19-10)W.2C						
						Typical	Rip Rap Line	ed Channel						
				[Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-10W.2C	15.74	7.20	20	3	0.2	4.20	1	1.2	N/A	3	41.6	0.136	81	А
											l i			

Design Flow: 10-year, 6-hour Storm

J19-10W.2C WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II			
Design Storm:	10 yr - 6 hr			
Rainfall Depth:	1.600 inches			

	Siruciure Networking.									
Туре		Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description			
Null		#1	==>	End	0.000	0.000	J19-10W.2C WATERSHED			

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	41.600	41.600	15.74	1.04

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-10W.2C WATERSHED

					<u> </u>	33			
Stru #	SWS #	SWS Area	Time of Conc	Musk K	Musk X	Curve	UHS	Peak Discharge	Runoff Volume
"	"	(ac)	(hrs)	(hrs)		Number		(cfs)	(ac-ft)
#1	1	41.600	0.136	0.000	0.000	81.000	М	15.74	1.036
	Σ	41.600						15.74	1.036

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	6.34	35.00	552.00	2.010	0.076
		6. Grassed waterway	15.04	40.00	266.00	5.810	0.012
		8. Large gullies, diversions, and low flowing streams	7.24	102.00	1,408.00	8.070	0.048
#1	1	Time of Concentration:					0.136

J19-10W.2C CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
20.00	3.0:1	3.0:1	7.2	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	15.74 cfs	
Depth:	0.18 ft	1.18 ft
Top Width:	21.09 ft	27.09 ft
Velocity:	4.20 fps	
X-Section Area:	3.75 sq ft	
Hydraulic Radius:	0.177 ft	
Froude Number:	1.76	

TABLE J19-2020 Channel Design Summary

						Chai	nnel J19-22V	V.3C.3D						
						Typical	Rip Rap Line	ed Channel						
				Ī			Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-22W.3C.3D	5.07	6.20	40	3	0.1	1.97	1	1.1	N/A	-	10.0	0.251	86	Α
									_		J			

Design Flow: 10-year, 6-hour Storm

J19-22W.3C.3D WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

	Siluciule Networking.										
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description					
Null	#1	==>	End	0.000	0.000	J19-22W.3C.3D WATERSHED					

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	10.000	10.000	5.07	0.37

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-22W.3C.3D WATERSHED

						55			
Stru #	SWS #	SWS Area	Time of Conc	Musk K	Musk X	Curve	UHS	Peak Discharge	Runoff Volume
"	"	(ac)	(hrs)	(hrs)		Number		(cfs)	(ac-ft)
#1	1	10.000	0.251	0.000	0.000	86.000	М	5.07	0.374
	Σ	10.000						5.07	0.374

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	1.17	7.00	596.00	0.860	0.192
		6. Grassed waterway	6.02	15.00	249.00	3.680	0.018
		8. Large gullies, diversions, and low flowing streams	6.22	70.00	1,126.00	7.470	0.041
#1	1	Time of Concentration:					0.251

J19-22W.3C.3D CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
40.00	3.0:1	3.0:1	6.2	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	5.07 cfs	
Depth:	0.06 ft	1.06 ft
Top Width:	40.38 ft	46.38 ft
Velocity:	1.97 fps	
X-Section Area:	2.57 sq ft	
Hydraulic Radius:	0.064 ft	
Froude Number:	1.38	

TABLE J19-2020 Channel Design Summary

						Chai	nnel J19-22V	V.3C.2D						
	Typical Rip Rap Lined Channel													
							Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-22W.3C.2D	12.50	5.70	25	3	0.2	3.29	1	1.2	N/A	-	21.4	0.127	86	А
											J			

Design Flow: 10-year, 6-hour Storm

J19-22W.3C.2D WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

Siluciule Networking.									
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description			
Null	#1	==>	End	0.000	0.000	J19-22W.3C.2D WATERSHED			

#1 Null

Structure Networking:



Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-22W.3C.2D WATERSHED

					<u> </u>	33			
Stru #	SWS #	SWS Area	Time of Conc	Musk K	Musk X	Curve	UHS	Peak Discharge	Runoff Volume
"	"	(ac)	(hrs)	(hrs)		Number		(cfs)	(ac-ft)
#1	1	21.400	0.127	0.000	0.000	86.000	М	12.50	0.811
	Σ	21.400						12.50	0.811

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	6.10	15.00	246.00	1.970	0.034
		6. Grassed waterway	4.90	35.00	714.00	3.320	0.059
		8. Large gullies, diversions, and low flowing streams	5.70	50.00	877.00	7.160	0.034
#1	1	Time of Concentration:					0.127

J19-22W.3C.2D CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
25.00	3.0:1	3.0:1	5.7	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	12.50 cfs	
Depth:	0.15 ft	1.15 ft
Top Width:	25.90 ft	31.90 ft
Velocity:	3.29 fps	
X-Section Area:	3.80 sq ft	
Hydraulic Radius:	0.146 ft	
Froude Number:	1.52	

TABLE J19-2020 Channel Design Summary

Channel J19-22W.3C.4D															
	Typical Rip Rap Lined Channel														
				[Designed					As-Built	1				
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design	
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number		
J19-22W.3C.4D	9.44	4.30	22	3	0.2	2.84	1	1.2	N/A	-	9.9	0.087	86	А	
											J				

Design Flow: 10-year, 6-hour Storm

J19-22W.3C.4D WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

Туре	Str #	u (flows into)	Stru #	Musk. K (hrs)	Musk. X	Description					
Null	#	1 ==>	End	0.000	0.000	J19-22W.3C.4D WATERSHED					

#1 Null

Structure Networking:



3

	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	9.900	9.900	9.44	0.46

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-22W.3C.4D WATERSHED

					<u> </u>	35			
Stru #	SWS #	SWS Area	Time of Conc	Musk K	Musk X	Curve	UHS	Peak Discharge	Runoff Volume
#	#	(ac)	(hrs) ^(hrs)		Number		(cfs)	(ac-ft)	
#1	1	9.900	0.087	0.000	0.000	86.000	М	9.44	0.460
	Σ	9.900						9.44	0.460

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	6. Grassed waterway	2.17	10.00	461.00	2.200	0.058
		8. Large gullies, diversions, and low flowing streams	4.29	28.00	652.00	6.210	0.029
#1	1	Time of Concentration:					0.087

J19-22W.3C.4D CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
22.00	3.0:1	3.0:1	4.3	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	9.44 cfs	
Depth:	0.15 ft	1.15 ft
Top Width:	22.89 ft	28.89 ft
Velocity:	2.84 fps	
X-Section Area:	3.32 sq ft	
Hydraulic Radius:	0.145 ft	
Froude Number:	1.31	

TABLE J19-2020 Channel Design Summary

						Cha	nnel J19-24V	V.1C.1D						
	Typical Rip Rap Lined Channel													
]			Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-24W.1C.1D	10.00	1.80	11	3	0.3	2.82	1	1.3	N/A	-	24.5	0.176	82	А
											1			

Design Flow: 10-year, 6-hour Storm

J19-24W.1C.1D WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

Filename: J19-24W.1C.1D WATERSHED.sc4

Printed 06-12-2020

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description					
Null	#1	==>	End	0.000	0.000	J19-24W.1C.1D WATERSHED					

#1 Null

Structure Networking:



Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-24W.1C.1D WATERSHED

					J	55			
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	24.500	0.176	0.000	0.000	82.000	М	10.00	0.665
	Σ	24.500						10.00	0.665

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	6. Grassed waterway	9.45	95.00	1,005.00	4.610	0.060
		8. Large gullies, diversions, and low flowing streams	1.78	30.00	1,681.00	4.000	0.116
#1	1	Time of Concentration:					0.176

J19-24W.1C.1D CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
11.00	3.0:1	3.0:1	1.8	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	10.00 cfs	
Depth:	0.30 ft	1.30 ft
Top Width:	12.79 ft	18.79 ft
Velocity:	2.82 fps	
X-Section Area:	3.55 sq ft	
Hydraulic Radius:	0.275 ft	
Froude Number:	0.94	

TABLE J19-2020 Channel Design Summary

						Cha	nnel J19-23V	V.2C.3D						
	Typical Rip Rap Lined Channel													
							Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-23W.2C.3D	106.07	1.30	25	3	0.8	4.68	1	1.8	N/A	-	569.8	0.855	82	А
											l			

Design Flow: 10-year, 6-hour Storm

J19-23W.2C.3D WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

Filename: J19-23W.2C.3D WATERSHED.sc4

Printed 06-12-2020

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

	Siluciule Networking.												
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description							
Null	#1	==>	End	0.000	0.000	J19-23W.2C.3D WATERSHED							

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	569.800	569.800	106.07	15.19

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-23W.2C.3D WATERSHED

					9	05			
Stru #	SWS #	SWS Area (ac)	Time of Musk K Conc (hrs)		Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	569.800	0.855	0.000	0.000	82.000	М	106.07	15.188
	Σ	569.800						106.07	15.188

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	5.17	73.00	1,412.01	1.810	0.216
		6. Grassed waterway	2.61	95.00	3,642.07	2.420	0.418
		8. Large gullies, diversions, and low flowing streams	1.29	35.00	2,709.00	3.400	0.221
#1	1	Time of Concentration:					0.855

J19-23W.2C.3D CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
25.00	3.0:1	3.0:1	1.3	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	106.07 cfs	
Depth:	0.83 ft	1.83 ft
Top Width:	29.95 ft	35.95 ft
Velocity:	4.68 fps	
X-Section Area:	22.68 sq ft	
Hydraulic Radius:	0.750 ft	
Froude Number:	0.95	

TABLE J19-2020 Channel Design Summary

						Cha	nnel J19-23V	V.2C.4D						
	Typical Rip Rap Lined Channel													
				[Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-23W.2C.4D	14.35	1.30	23	3	0.3	2.28	1	1.3	N/A	-	43.0	0.235	81	А
											1			

Design Flow: 10-year, 6-hour Storm

J19-23W.2C.4D WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

	Siluciule Networking.										
Туре		Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description				
Null		#1	==>	End	0.000	0.000	J19-23W.2C.4D WATERSHED				

#1 Null

Structure Networking:



3

	Immediate Contributing Area	Total Contributing Area	Peak Discharge	Total Runoff Volume
	(ac)	(ac)	(cfs)	(ac-ft)
#1	43.000	43.000	14.35	1.06

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-23W.2C.4D WATERSHED

						05			
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	43.000	0.235	0.000	0.000	81.000	М	14.35	1.061
	Σ	43.000						14.35	1.061

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	3.35	19.00	567.01	1.460	0.107
		6. Grassed waterway	5.05	10.00	198.00	3.370	0.016
		8. Large gullies, diversions, and low flowing streams	7.73	62.00	802.00	8.340	0.026
		8. Large gullies, diversions, and low flowing streams	1.25	13.00	1,041.00	3.350	0.086
#1	1	Time of Concentration:					0.235

J19-23W.2C.4D CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
23.00	3.0:1	3.0:1	1.3	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	14.35 cfs	
Depth:	0.26 ft	1.26 ft
Top Width:	24.59 ft	30.59 ft
Velocity:	2.28 fps	
X-Section Area:	6.30 sq ft	
Hydraulic Radius:	0.255 ft	
Froude Number:	0.79	

TABLE J19-2020 Channel Design Summary

						Chai	nnel J19-23V	V.2C.5D						
						Typical	Rip Rap Line	ed Channel						
							Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
J19-23W.2C.5D	4.16	7.70	13	3	0.1	3.00	1	1.1	N/A	-	11.0	0.149	81	А
											J			

Design Flow: 10-year, 6-hour Storm

J19-23W.2C.5D WATERSHED DESIGN (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

	<i>στι αυται το τνετινοι</i> κπιχ.										
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description					
Null	#1	==>	End	0.000	0.000	J19-23W.2C.5D WATERSHED					

#1 Null

Structure Networking:



3

	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	11.000	11.000	4.16	0.27

Structure Summary:

Structure Detail:

Structure #1 (Null)

J19-23W.2C.5D WATERSHED

					<u> </u>	33			
Stru #	SWS #	SWS Area	Time of Conc	Musk K	Musk X	Curve	UHS	Peak Discharge	Runoff Volume
<i>π</i>	π	(ac)	(hrs)	(hrs)		Number		(cfs)	(ac-ft)
#1	1	11.000	0.149	0.000	0.000	81.000	М	4.16	0.274
	Σ	11.000						4.16	0.274

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	3.35	19.00	567.00	1.460	0.107
		6. Grassed waterway	5.05	10.00	198.00	3.370	0.016
		8. Large gullies, diversions, and low flowing streams	7.73	62.00	802.00	8.340	0.026
#1	1	Time of Concentration:					0.149

J19-23W.2C.5D CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
13.00	3.0:1	3.0:1	7.7	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	4.16 cfs	
Depth:	0.10 ft	1.10 ft
Top Width:	13.62 ft	19.62 ft
Velocity:	3.00 fps	
X-Section Area:	1.39 sq ft	
Hydraulic Radius:	0.101 ft	
Froude Number:	1.66	

SECTION 2

Phase I Bond Release Supporting Information

Introduction

The Phase I Bond Release information contained in this application for the J19, J19-West (J19W), and N9 Coal Resource Areas (CRAs) consists primarily of backfilling, grading, suitable plant growth material replacement, drainage channel as-builts, and slope analysis.

Backfilling and Grading

There are no permanent support facilities included in this J19, J19W, and N9 Phase I Bond Release Application. The permanent support facilities will be included in later bond release applications. Final grading of permanent program lands within the J19, J19W, and N9 areas occurred from 1999 to 2018. Final grading status for the release areas shown on Maps 1.1.1 and 1.1.2 were previously reported and submitted with supporting maps to the regulatory authority in the following annual monitoring reports.

Peabody Western Coal Company (PWCC). 2000-2019. 1999-2018 Minesoil Reconstruction and Revegetation Activities Reports, Black Mesa and Kayenta Mines, Flagstaff and Kayenta, Arizona. <u>Reports Prepared for</u>: The Office of Surface Mining Reclamation and Enforcement, Western Service Center, Denver, Colorado.

The pre-mining and post-mining topography consists of rolling hills dissected by ephemeral drainage channels. The regulations require the post-mining graded slopes must approximate the pre-mining natural slopes. Approximate original contour means that surface configuration is achieved by backfilling and grading of the mined area so that the reclaimed area resembles the general surface configuration of the surrounding terrain with all final highwall and spoil piles eliminated. In order to perform a realistic comparison of the pre-mining and post-mining slope measurements, PWCC utilized ESRI ArcGIS 10 Spatial Analyst software to generate slope measurement polygons within the entire J19, J19W, and N9 reclamation areas included in this submittal. The J19, J19W, and N9 release areas included with this Phase I bond release application are all Permanent Program Lands. The J19, J19W, and N9 reclamation areas were evaluated to compare the slope stability of the pre- and post-mining landforms and general surface configuration.

The slope polygons were grouped into slope measurement ranges based on the following six slope measurement classifications:

- 1. <9%
- 2. 9% to 13%
- 3. 13% to 18%
- 4. 18% to 25%
- 5. 25% to 33%
- 6. >33%

These slope measurement classifications are like the classifications utilized in the AZ-0001F Permit, Chapter 26, Surface Stabilization. The location of the area associated with each of the pre- and post-mine slope measurement classes for the J19, J19W, and N9 reclamation areas can be found on Maps 2.3.1 and 2.3.2 (Post-Mine) and Maps 2.4.1 and 2.4.2 (Pre-Mine). Tables 2.1.1, 2.1.2, and 2.1.3 provide a summary of the area in each slope measurement classification before mining and after mining for the N9, J19, and J19W release areas, respectively:

Table 2.1.1. Pre and Post-Mining Slope Analysis for N9 Permanent Program Reclaimed Areas.

RANGE	BEGINNING (%)	END (%)	AREA(Ac.)	PERCENT of TOTAL AREA	POST - MINING SLOPE AREA VS. PRE - MINING SLOPE AREA (%)
1	0	9	205.8	50.1	+12.4
2	9	13	85.7	20.9	-4.6
3	13	18	65.5	15.9	-4.6
4	18	25	42.0	10.2	-1.9
5	25	33	9.2	2.2	-1.5
б	33	+	2.5	0.6	0

POST - MINING SLOPE ANALYSIS:

PRE - MINING SLOPE ANALYSIS:

RANGE	BEGINNING (%)	END (%)	AREA(Ac.)	PERCENT of TOTAL AREA
1	0	9	154.8	37.7
2	9	13	104.5	25.5
3	13	18	84.1	20.5
4	18	25	49.6	12.1
5	25	33	15.1	3.7
6	33	+	2.5	0.6

					POST - MINING SLOPE AREA
		END		PERCENT	vs.
RANGE	BEGINNING (%)	(%)	AREA(Ac.)	of TOTAL AREA	PRE - MINING SLOPE AREA (%)
1	0	9	130.9	49.1	-20.3
2	9	13	45.1	16.9	-0.3
3	13	18	45.7	17.1	+9.5
4	18	25	37.5	14.1	+11.0
5	25	33	6.6	2.5	+1.3
6	33	+	0.8	0.3	-1.1

POST - MINING SLOPE ANALYSIS:

PRE - MINING SLOPE ANALYSIS:

RANGE	BEGINNING (%)	END (%)	AREA(Ac.)	PERCENT of TOTAL AREA
1	0	9	185.0	69.4
2	9	13	46.0	17.2
3	13	18	20.2	7.6
4	18	25	8.3	3.1
5	25	33	3.3	1.2
6	33	+	3.8	1.4

Table 2.1.3. Pre and Post-Mining Slope Analysis for J19W Permanent Program Reclaimed Areas.

					POST - MINING SLOPE AREA
		END		PERCENT	vs.
RANGE	BEGINNING (%)	(%)	AREA(Ac.)	of TOTAL AREA	PRE - MINING SLOPE AREA (%)
1	0	9	96.5	38.4	+18.0
2	9	13	40.0	15.9	-0.9
3	13	18	51.9	20.6	-2.7
4	18	25	43.7	17.4	-6.5
5	25	33	14.2	5.6	-5.6
6	33	+	4.9	1.9	-2.6

POST - MINING SLOPE ANALYSIS:

PRE - MINING SLOPE ANALYSIS:

RANGE	BEGINNING (%)	END (%)	AREA(Ac.)	PERCENT of TOTAL AREA
1	0	9	51.2	20.4
2	9	13	42.1	16.8
3	13	18	58.6	23.3
4	18	25	59.9	23.9
5	25	33	28.2	11.2
6	33	+	11.2	4.5

As illustrated above, the post-mine topography has very similar slope gradient percentages in each of the six range categories compared with the original pre-mine topography. Overall, post-mine topography has slightly less steep slopes than the pre-mine topography. The asbuilt post-mine surface was compared to the Estimated Post-mining Topographic (PMT), Drawing 85352, Sheets K6, K7, M9, and M10, Volume 29 of Permit AZ-0001F. The comparison did not reflect any areas outside the +/- 20 feet of the estimated post-mine contours as required in the permit.

Attachment 2.1 includes the as-built information for the J19, J19W, and N9 reclamation drainage channels shown on Map 2.5.1 (Sheets 1 to 3 of 3) and Map 2.5.2 (Sheets 1 to 2 of 2). This is similar to the map submitted previously in the Annual Surface Stabilization Reports. Based on the information in Attachment 2.1 and a field inspection of the J19, J19W, and N9 areas, PWCC has demonstrated the post-mining reclamation drainage structures are stable and can safely pass the design runoff. The locations of these drainage structures are shown on Map 2.5.1 (3 sheets) and Map 2.5.2 (2 sheets).

In conclusion, the J19, J19W, and N9 reclamation areas have been graded to very similar overall slopes compared to pre-mine topography. Grading was completed to eliminate final highwalls and spoil piles, to ensure stability, to reestablish a positive stable drainage network, and to facilitate the livestock grazing, wildlife habitat, and cultural plant postmining land uses. The J19, J19W, and N9 backfilling, grading, and drainage system construction was conducted in conformance with the applicable regulatory requirements and approved reclamation plans.

Surface Water Data

There have been very few NPDES discharges from Pond J16-L located in Reed Valley Wash and no NPDES discharges from Ponds J7-JR, J19-A, J19-B, J19-D, and J19-E located in tributaries of Red Peak Valley Wash down gradient from the J19 and J19W bond release watersheds. There have been no NPDES discharges from Ponds N9-A, N9-B, N9-C, N9-D, N9-E, N9-F, and N9-G located in tributaries of Yellow Water Canyon Wash down gradient from the N9 bond release watershed. Lagoon dewatering was conducted at Pond J16-L on August 24, 2007 and February through May 2011 to perform maintenance activities per MSHA regulations. Lagoon dewatering was also conducted at Pond J16-L during August 2008 to restore enough storage capacity. No applicable effluent limitations were exceeded for the duration of these lagoon dewatering activities. Eleven (11) water quality samples have been collected from two of these thirteen ponds during the past five (5) years per the approved monitoring schedule presented in Table 10, Chapter 16 of the Permit Application Package (PAP) for Permit AZ-0001F. Ten water quality samples (two per year) were collected from Pond J7-JR over the past five years and one sample from Pond J16-L in 2019. Laboratory data for all eleven samples met livestock water quality standards.

Spoil Sampling and Suitable Material Replacement

Final graded spoil for the J19, J19W, and N9 CRAs permanent program lands was sampled during fifteen (15) years from 1999 to 2018 (as documented in Attachments 2.3a, 2.3b, and 2.3c) to comprehensively evaluate suitability and determine suitable plant growth material replacement requirements per Chapter 22, Volume 11, Permit AZ-0001F. All spoil sampling and data evaluations were completed using procedures and suitability criteria presented in Chapter 22, Volume 11, Permit AZ-0001F. Spoil sampling results were previously reported and submitted with supporting maps to the regulatory authority in fifteen (15) annual monitoring reports as referenced below and documented in Attachments 2.3a, 2.3b, and 2.3c. Peabody Western Coal Company (PWCC). 2000, 2003-2007, 2011-2019. 1999, 2002-2006, 2010-2018 Minesoil Reconstruction and Revegetation Activities Reports, Black Mesa and Kayenta Mines, Flagstaff and Kayenta, Arizona. <u>Reports Prepared for</u>: The Office of Surface Mining Reclamation and Enforcement, Western Service Center, Denver, Colorado.

Spoil sample laboratory data from the reports listed above that is pertinent to the Phase I bond release area is included in Attachment 2.3a for the J19W CRA, Attachment 2.3b for the J19 CRA, and Attachment 2.3c for the N9 CRA. A total of 351 sites, 82 in J19W, 114 in J19, and 155 in N9 were located on final graded spoil slopes and sampled within the designated Phase I release areas. Two hundred seven (207) of the 351 sites sampled (59%) as listed in Attachments 2.3a, 2.3b, and 2.3c and shown on Maps 2.2.1 and 2.2.2 had suitable spoil characteristics from the surface to three (3) feet and required no additional suitable subsoil and substratum material to be replaced before applying one foot of suitable surface Topsoil, suitable residual soils, and weathered overburden derived from mostly soil. scoria, sandstone, and siltstone were used to bury unsuitable spoil at J19, J19W, and N9 when 2, 3, or 4 feet of suitable mitigation material was required as shown on Maps 2.2.1 and 2.2.2. Four feet of suitable residual soils and weathered overburden were used in six (6) cultural planting and two (2) steep slope areas that total 34.4 and 16.3 acres, respectively. Durable sandstone, siltstone, and scoria overburden were used to construct seventeen (17) rocked downdrains and drainages (2.7 acres). Occasionally, topsoil was used in J19, J19W, and N9 as mitigation material as observed by the field supervisors during reclamation work and as noted by the suitable plant growth material thickness survey. An average of 0.84 feet of mitigation material was required for the entire Phase I release

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area (929 acres) based on the comprehensive graded spoil sampling suitability analysis presented in Attachments 2.3a, 2.3b, and 2.3c. For areas that have had suitable plant growth material replaced (696 acres), an average of 0.88 feet of mitigation material was required based on the comprehensive graded spoil sampling suitability analysis presented in Attachments 2.3a, 2.3b, and 2.3c. As documented in the next section titled Suitable Plant Growth Material Thickness, the mean thickness of mitigation material replaced for this 696 acre area equaled 1.2 feet (excluding one (1) foot of topsoil, suitable residual soils, and weathered scoria overburden at the surface).

Suitable Plant Growth Material Thickness

Four feet of suitable plant growth material as defined in Chapter 22, Volume 11, Permit AZ-001F was replaced on final graded slopes of permanent program lands within the J19, J19W, and N9 CRAs from 1999 to 2019. Suitable plant growth material replacement status for most of the release areas shown on Maps 1.1.1 and 1.1.2 were previously reported to the regulatory authority on the Reclamation Status Map 2 (as of December 31, 2018) shown on the Southeast and Northwest Sheets contained in the 2018 Reclamation Status and Monitoring Report, Black Mesa and Kayenta Mines (submitted May 2019). Suitable plant growth material replacement areas for the 2019 calendar year will be submitted to the regulatory authority with the next annual report in August 2020. Soil was redistributed on final graded slopes from stockpiles or replaced directly from soil removal areas prior to ripping and contour discing. Pursuant to Chapter 22 of Permit AZ-0001F, the thickness of soil replaced shall exceed the minimum average of 1 foot.

Six (6) cultural planting and two (2) steep slope sites, totaling approximately 51 acres combined as shown on Maps 2.1.1 and 2.1.2, received four feet of suitable residual soils and weathered overburden. Seventeen (17) rocked downdrains and drainages, totaling about 2.7 acres as shown on Maps 2.2.1 and 2.2.2, received suitable overburden derived from predominantly scoria, sandstone, and siltstone. Topsoil was not replaced at these twentyfive (25) sites that totaled about 54 acres.

One suitable plant growth material thickness survey of the J19, J19W, and N9 reclaimed areas included with this Phase I bond release application was completed during May 2020 as shown on Maps 2.1.1 and 2.1.2. Personnel from Peabody Western Coal Company (PWCC) observed sites in the J19, J19W, and N9 reclaimed areas in order to verify the suitable plant growth material replacement thickness. A stratified grid sampling scheme using a random number generator program was used for the PWCC survey to locate 47 sites within the topsoiled,

2.6

cultural planting, and steep slope areas of J19 (162 acres), J19W (247 acres), and N9 (286 acres) prior to going into the field. Suitable plant growth material thickness verification sites were not placed within the rocked downdrain, large drainage areas, and areas that have not yet been topsoiled. A sampling density of about 1 site per 15 acres was used; a slightly higher density than those used and approved previously at Kayenta Mine for the N1/N2, N7/N8, N11, N14, J16, J19, and J21 soil thickness evaluations. A Tremble GeoXT survey grade GPS unit was used to navigate to each of the sites. At all sites, either a 3 ½-inch bucket auger or backhoe pit were used to verify the soil and mitigation material thickness by excavating to the contact with spoil. The results of the soil and mitigation material thickness verification survey are shown in Table 2.2 and Maps 2.1.1 and 2.1.2 show all sampled sites with corresponding thickness values.

Forty-seven (47) sample sites were randomly placed within the 696 acres of disturbed lands that received suitable plant growth material within the release area. Suitable plant growth material thickness was verified at all 47 sites. Suitable plant growth material thickness among the 47 profiles placed over the J19, J19W, and N9 release area ranged from 0.8 to 5.6 feet. The mean topsoil thickness value, excluding thickness attributed to suitable residual soils and suitable overburden derived from predominantly scoria and sandstone used in the cultural planting and steep slope areas noted in Table 2.2 was 1.9 feet over 45 sites. The mean soil and suitable material thickness of 1.9 feet exceeds the minimum 1-foot average topsoil thickness requirements presented in the approved reclamation plan in Chapter 22 of Permit AZ-0001F.

When the topsoiled reclamation areas (644 acres) are combined with the cultural planting, steep slope, and select mitigative areas (52 acres), the mean thickness of suitable plant growth material is 2.2 feet (Table 2.2). This mean thickness of 2.2 feet exceeds the average combined topsoil and mitigation material thickness of 1.9 feet as required by the spoil suitability mitigation requirements discussed in the previous section and shown on Maps 2.2.1 and 2.2.2. In conclusion, PWCC has satisfied topsoil and suitable plant growth material thickness replacement requirements in conformance with applicable regulatory requirements and as stipulated by the approved reclamation plan for the J19, J19W, and N9 Phase I release areas shown on Maps 1.1.1 and 1.1.2.

2.7

	Table 2.2. Suitable Plant Growth Material Thickness Verification Sites Sampled by PWCC at J19, J19W, and N9 During May 2020 (See Maps 2.1.1 and 2.1.2 for Site Locations).							
	Easting	Northing	Soil/Mitigation					
Site ID $^{(1)}$	(feet) ⁽²⁾	(feet) ⁽²⁾	Thickness (feet)	Coal Resource Area				
1	26612	10794	1.0	N9				
2	21549	5270	1.0	N9				
3	24986	6506	1.0	N9				
4	25951	7045	1.0	N9				
5	26979	9406	2.5	N9				
б	19996	2150	3.6	N9				
7	23727	7586	2.6	N9				
8	21301	5560	0.8	N9				
9	24911	6861	1.3	N9				
10	23572	7050	1.6/4.0(4)	N9				
11	26392	10541	2.0	N9				
12	21633	5646	2.0	N9				
13	22132	4398	2.3	N9				
14	22588	4702	2.6	N9				
15	25322	8912	4.5 ⁽³⁾	N9				
16	25789	8663	3.5 ⁽³⁾	N9				
17	48363	-35744	2.3	J19W				
18	48869	-37887	1.7	J19W				
19	49698	-34785	1.5	J19W				
20	50141	-35800	2.4	J19W				
21	48841	-36101	1.7/1.2(4)	J19W				
22	48186	-36179	2.4	J19W				
23	47995	-35556	2.2	J19W				
24	50158	-36254	3.1	J19W				
25	50061	-35615	0.9	J19W				
26	48209	-35115	2.8	J19W				
27	49626	-35443	0.9	J19W				
28	47533	-33981	2.2	J19W				
29	49415	-36426	2.1/2.9 ⁽⁴⁾	J19W				
30	47776	-35033	2.3	J19W				
31	48527	-37519	1.4	J19W				

Table 2.2. Continued.								
	Easting	Northing	Soil Thickness					
Site ID ⁽¹⁾	(feet) ⁽²⁾	(feet) ⁽²⁾	(feet)	Coal Resource Area				
32	49940	-35059	1.2	J19W				
33	47481	-33253	1.5	J19W				
34	47471	-34648	3.5	J19W				
35	48186	-34027	3.1	J19W				
36	49534	-34324	1.1	J19W				
37	49313	-36021	1.4/1.0(4)	J19W				
38	58959	-34045	4.2	J19				
39	58758	-40322	2.3	J19				
40	59490	-37362	2.4	J19				
41	58854	-32935	1.2	J19				
42	58670	-39493	1.3	J19				
43	59160	-40740	1.9	J19				
44	53043	-35847	1.3	J19				
45	58968	-41457	1.4	J19				
46	59586	-40740	1.5	J19				
47	55374	-29444	1.1	J19				
MEAN								
⁽¹⁾ For locat	⁽¹⁾ For location see Maps 2.1.1 and 2.1.2. ⁽²⁾ PWCC coordinate system. ⁽³⁾ Cultural planting							
area. ⁽⁴⁾ Suitable mitigation material replaced between topsoil and spoil. ⁽⁵⁾ Total thickness								
attributed	attributed to topsoil and suitable mitigative material.							

CERTIFICATION

PEABODY WESTERN COAL COMPANY KAYENTA MINE, J19, J19W, AND N9 COAL RESOURCE AREAS, PHASE I BOND RELEASE APPLICATION NAVAJO COUNTY, ARIZONA

I HEREBY CERTIFY that, to the best of my knowledge and belief, all applicable reclamation activities described in the attached Phase I Bond Release Application for the J19, J19 West (J19W), and N9 Coal Resource Areas dated June 17, 2020 have been accomplished in accordance with the reclamation requirements of the Act, the regulatory program, and the approved reclamation plan contained in the AZ-0001F Permit. The bond release parcel is free from enforcement actions.

Peabody Western Coal Company - Kayenta Mine

By:

Randy Lehn Director Operations Support - Kayenta Mine

STATE OF ARIZONA

- NAVAJO- COUNTY

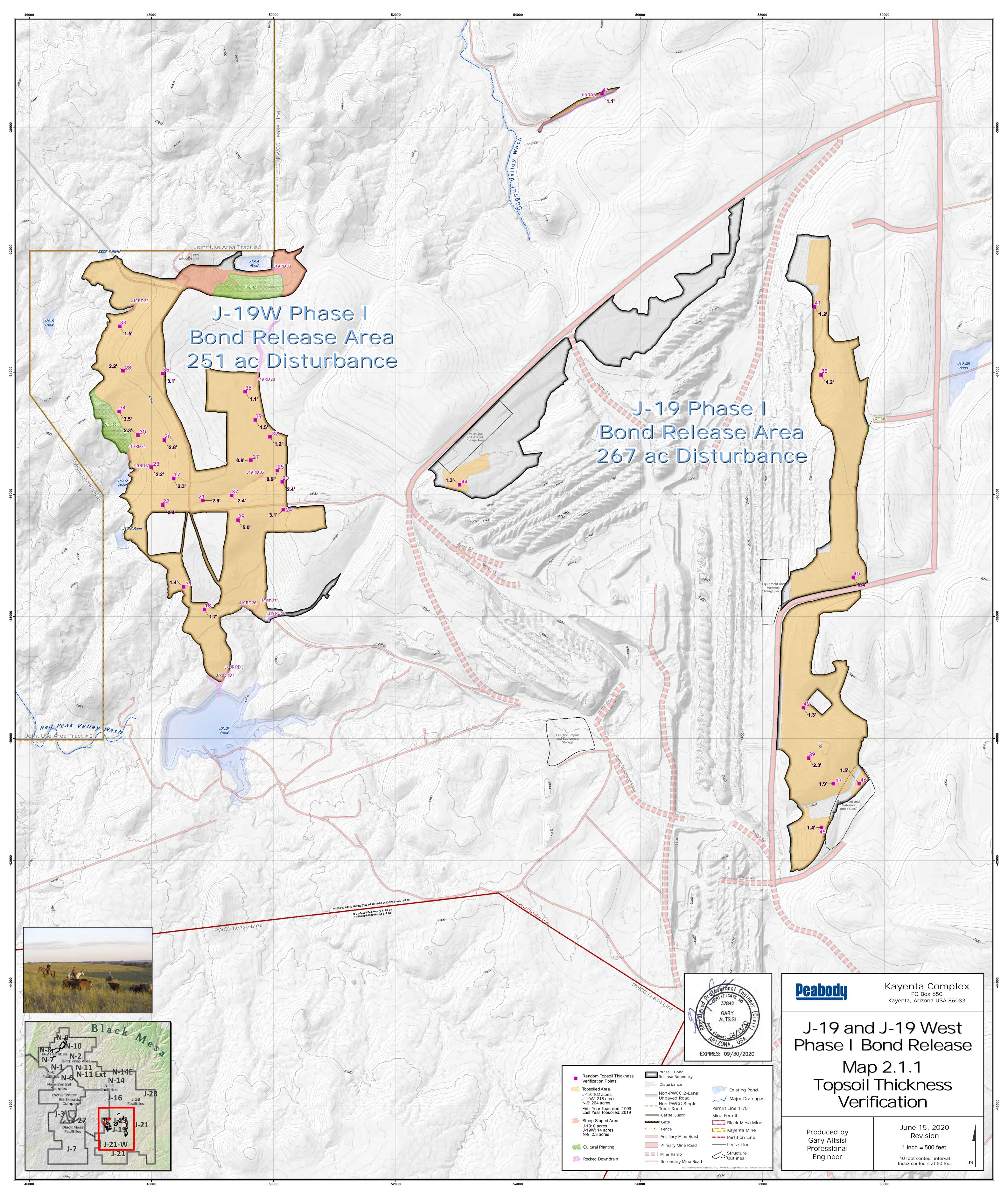
Signed or attested before me this <u>day</u> day of June 2020, by Randy Lehn, Director Operations Support of Kayenta Mine owned by Peabody Western Coal Company, a Delaware Corporation, on behalf of said Kayenta Mine.

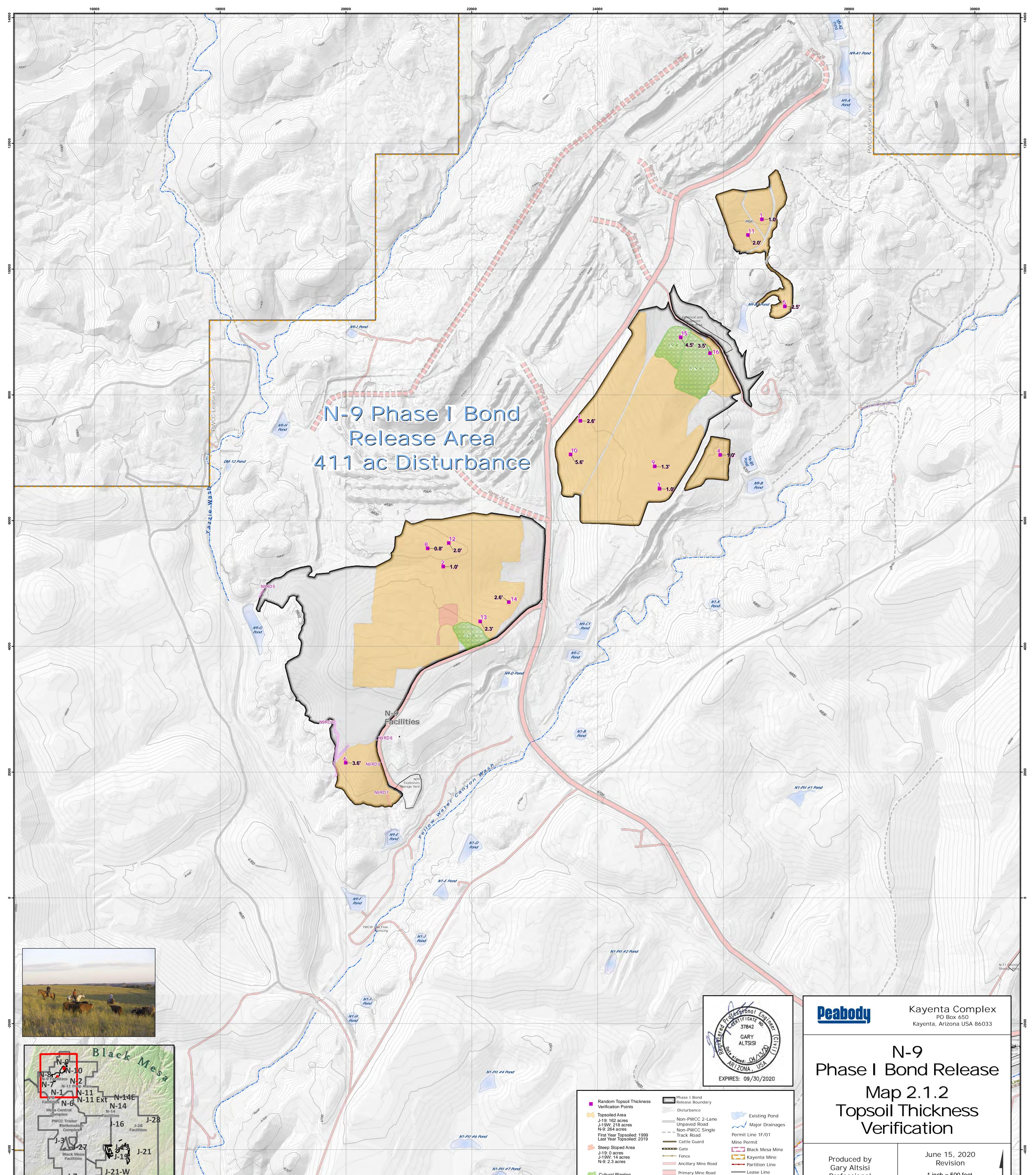
Notary Public



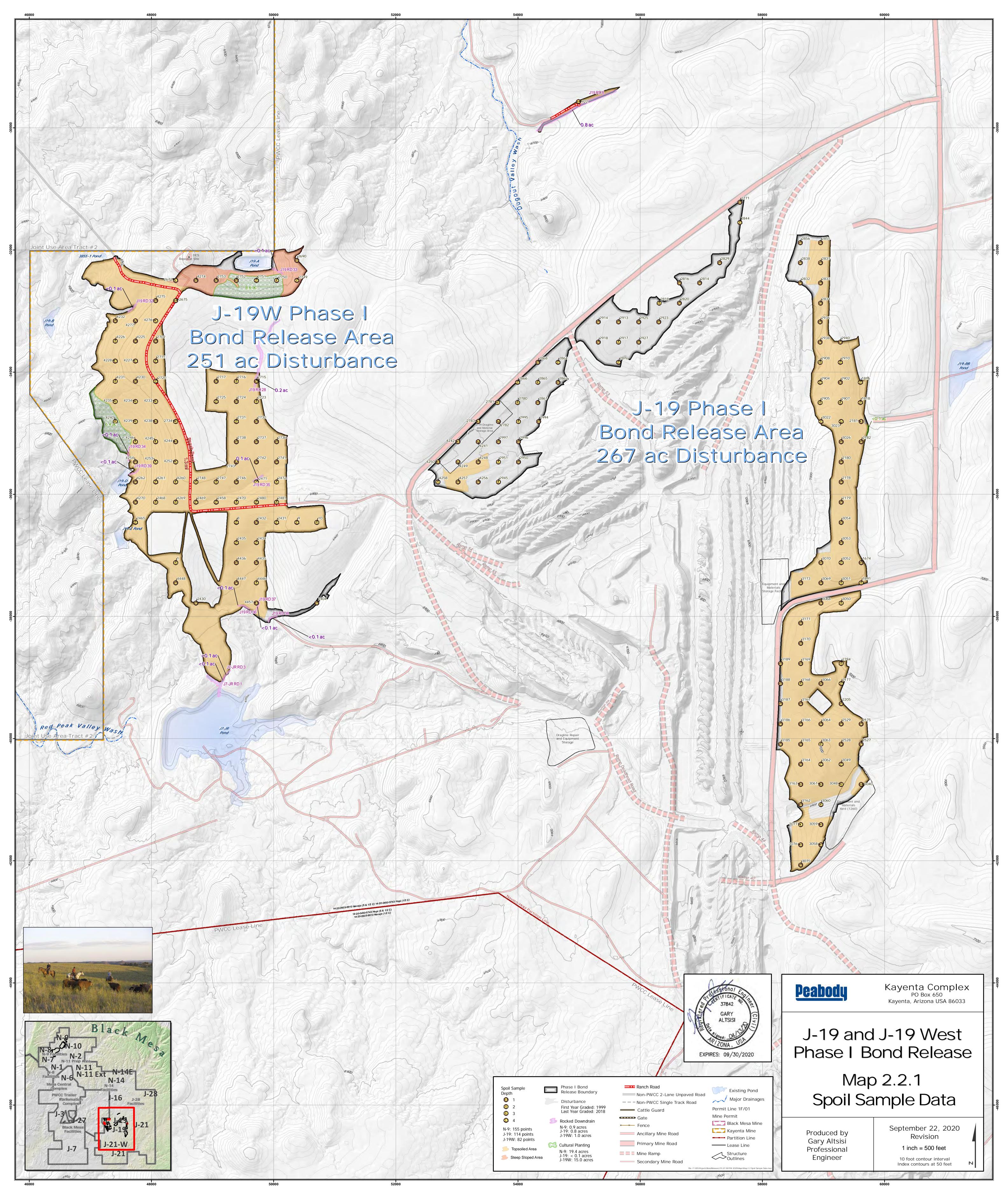
My commission expires:

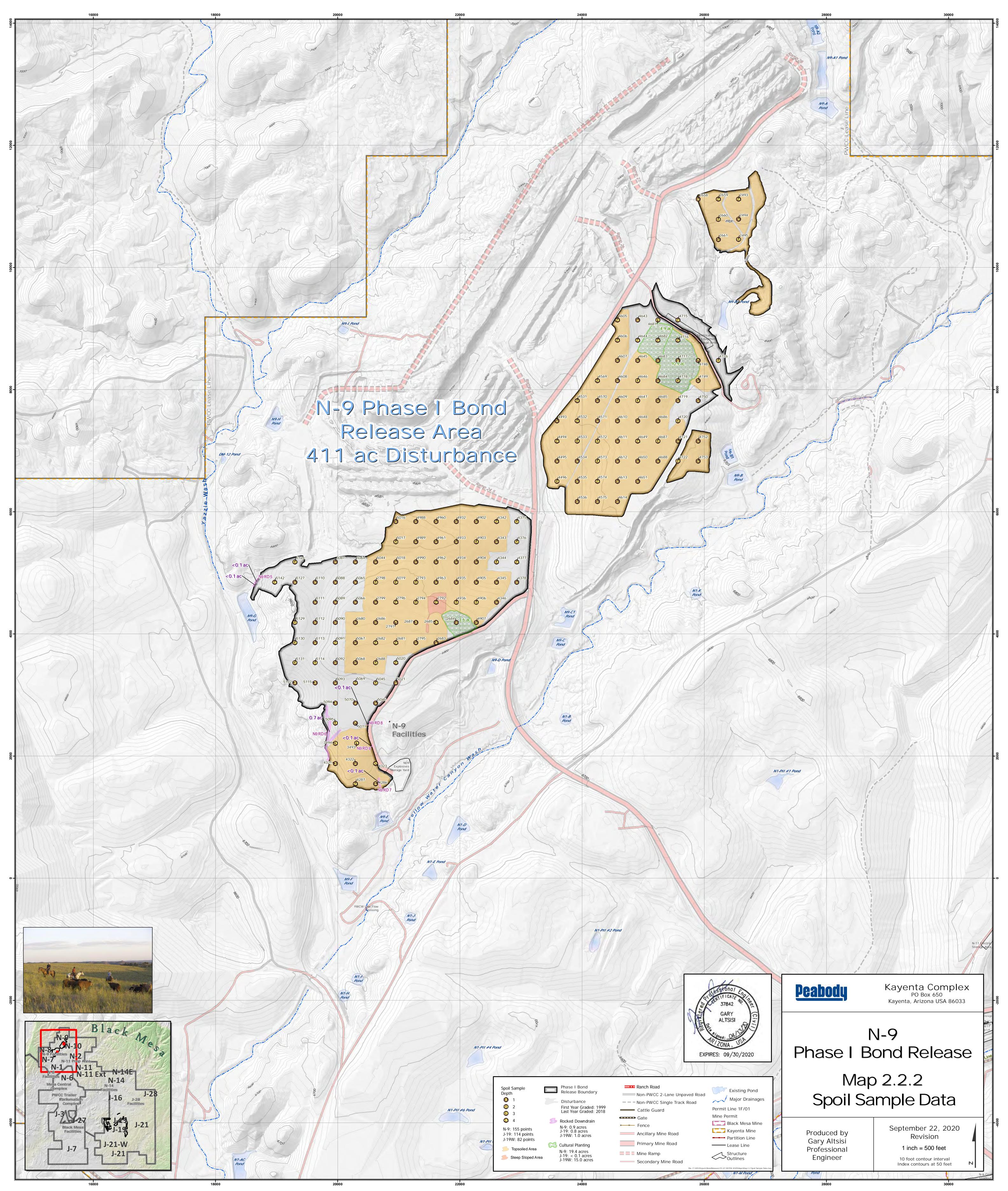
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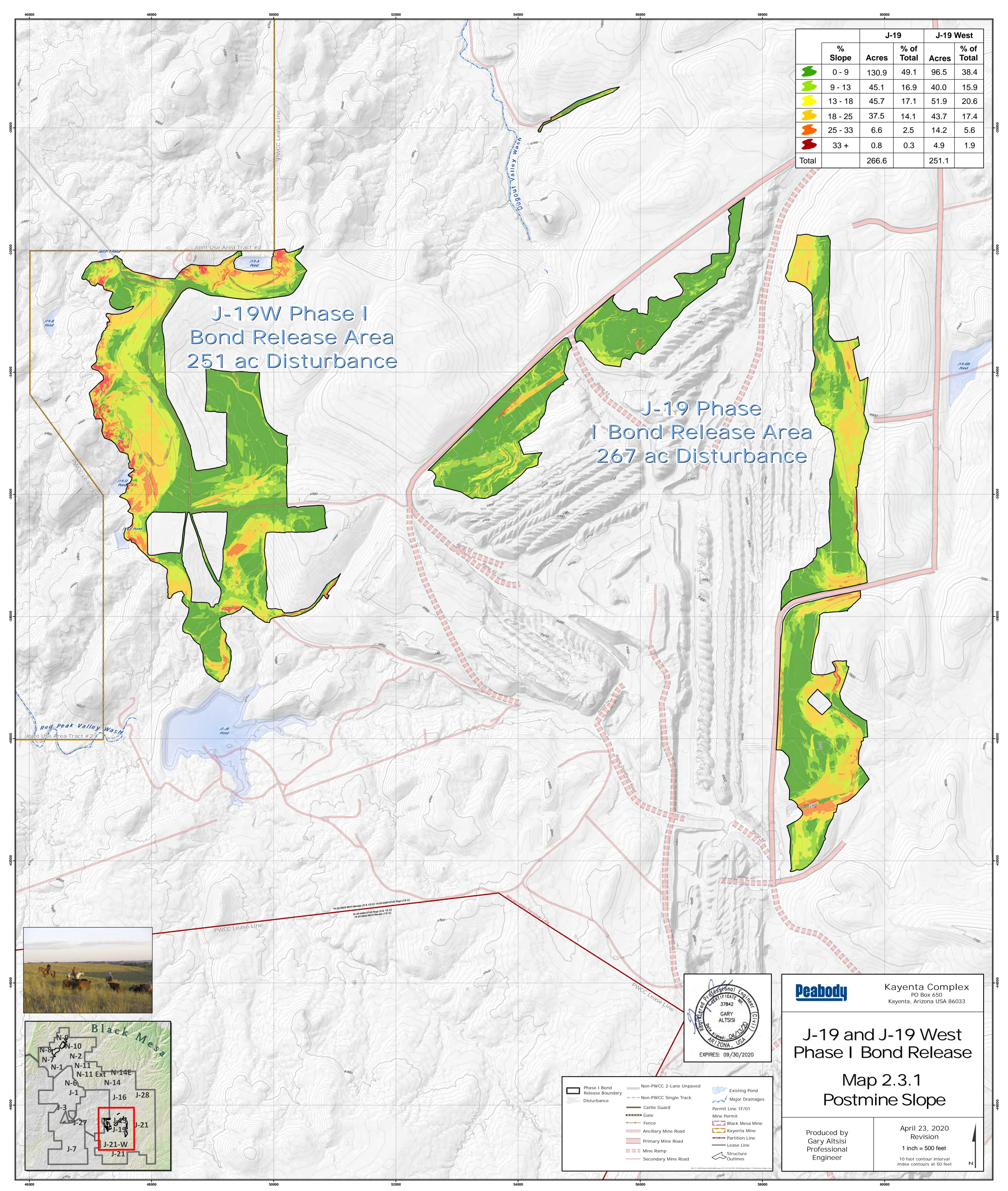


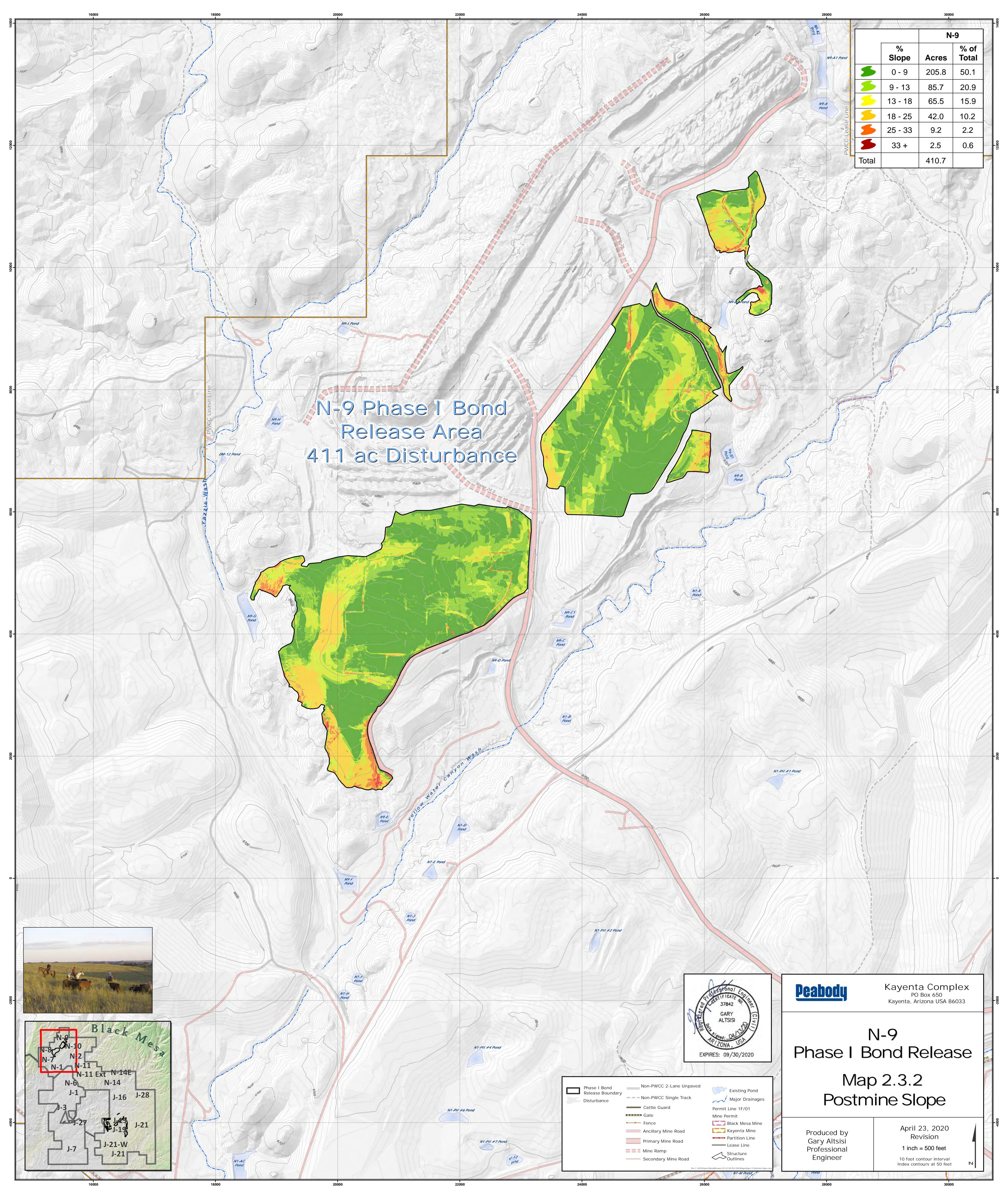


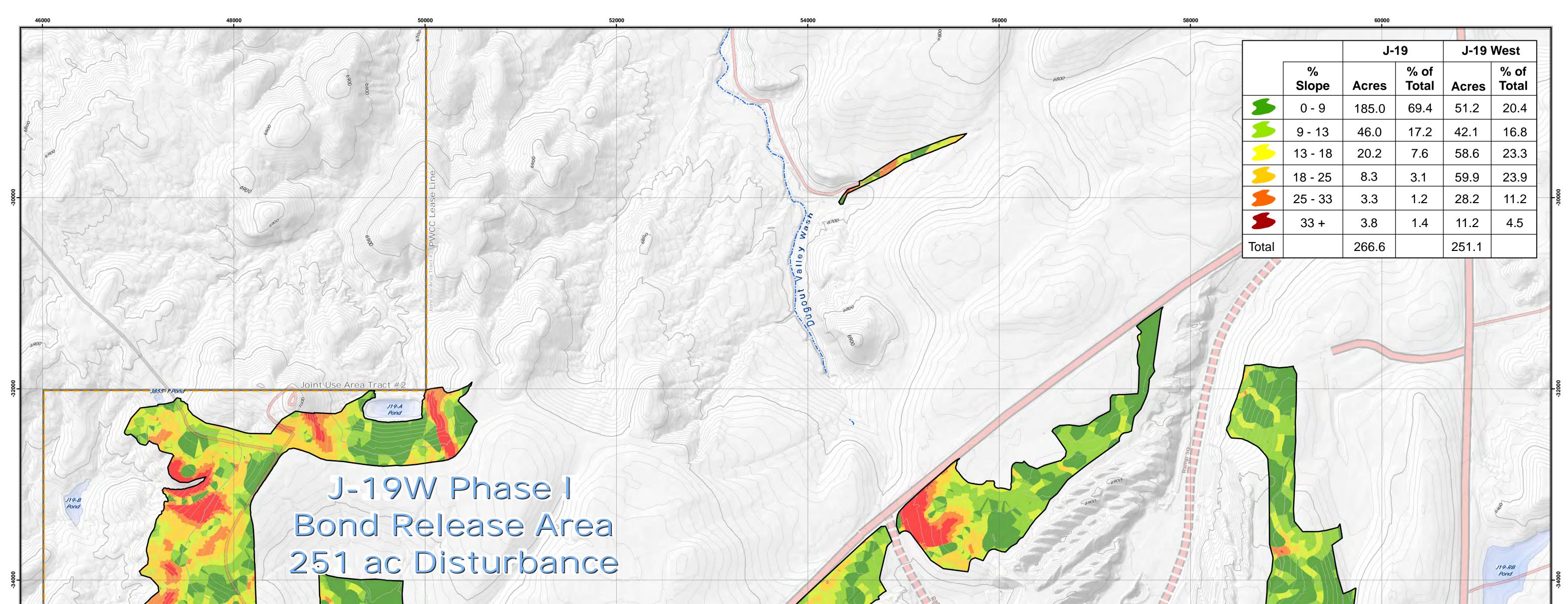




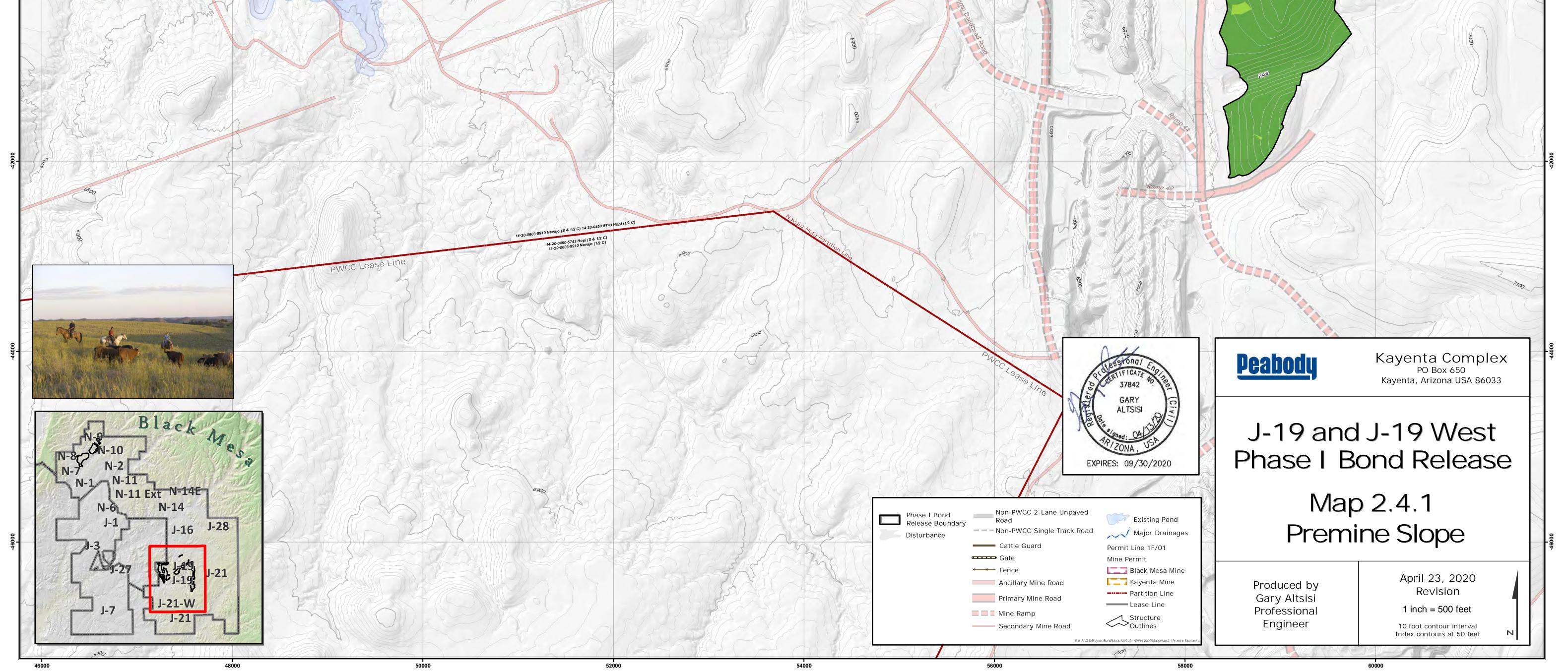


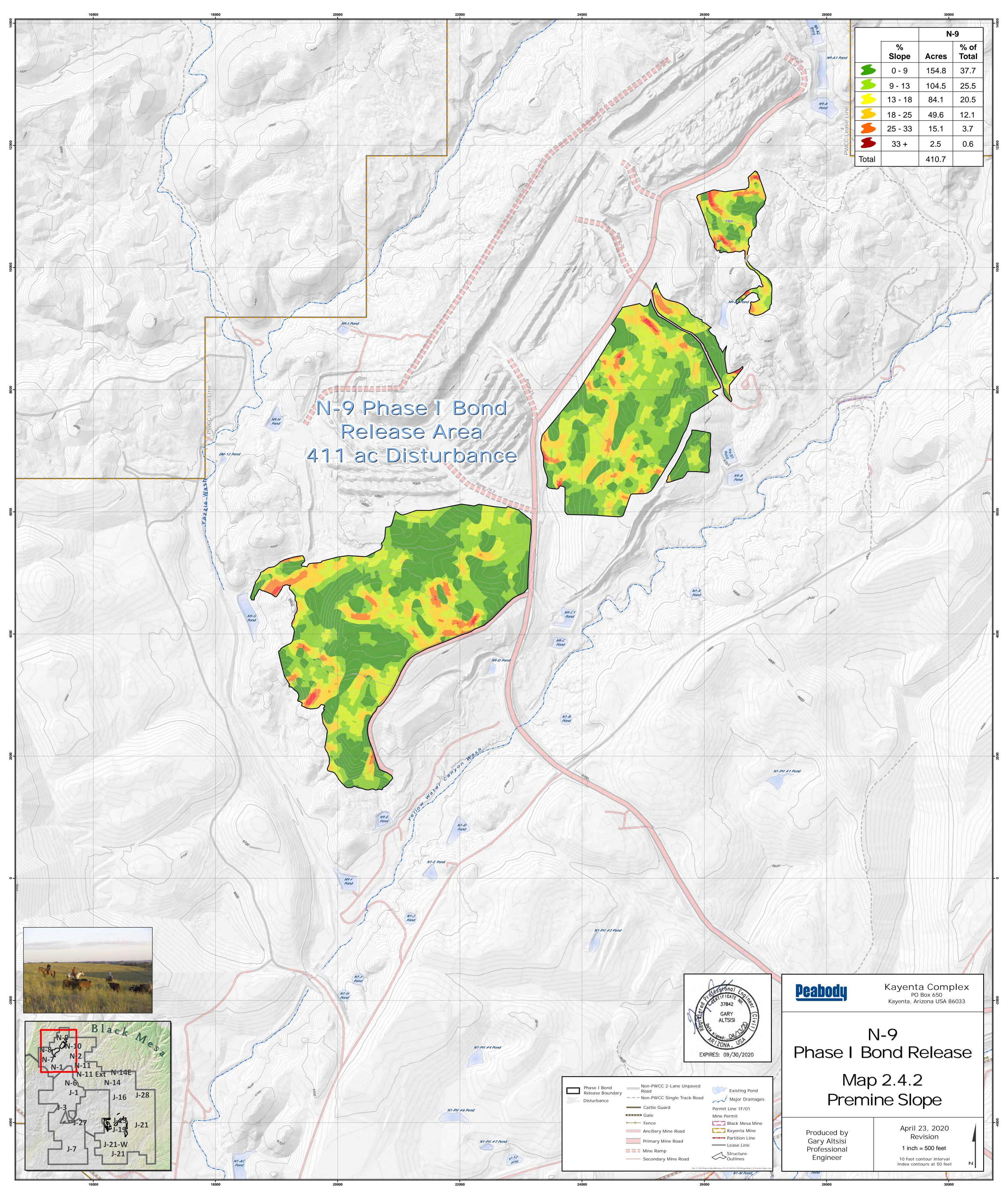






J-19 Phase Bond Release Area 267 ac Disturbance





KAYENTA MINE PHASE I BOND RELEASE WATERSHED & CHANNEL DESIGNS N9

TABLE N9-2020 Channel Design Summary

						Cha	annel N9-1W	.1C.1D						
						Typical	Rip Rap Line	ed Channel						
							Designed			As-Built				
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
N9-1W.1C.1D	14.27	5.30	25	3	0.2	3.39	1	1.2	N/A	-	42.2	0.227	81	A
									-					

Design Flow: 10-year, 6-hour Storm

<u>N9-1W.1C.1D WATERSHED DESIGN</u> (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

	Siluciule Networking.									
T	уре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description			
Ν	lull	#1	==>	End	0.000	0.000	N9-1W.1C.1D WATERSHED			

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
	· · /		14.07	. ,
#1	42.200	42.200	14.27	1.04

Structure Summary:

Structure Detail:

Structure #1 (Null)

N9-1W.1C.1D WATERSHED

					<u> </u>	33			
Stru #	SWS #	SWS Area (ac)	Time of Conc	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge	Runoff Volume
		(ac)	(hrs)	(113)		Number		(cfs)	(ac-ft)
#1	1	42.200	0.227	0.000	0.000	81.000	М	14.27	1.040
	Σ	42.200						14.27	1.040

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	3.24	22.00	678.00	1.440	0.130
		6. Grassed waterway	6.78	50.00	737.00	3.900	0.052
		8. Large gullies, diversions, and low flowing streams	5.30	60.00	1,133.00	6.900	0.045
#1	1	Time of Concentration:					0.227

N9-1W.1C.1D CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

N	Bottom Nidth (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
	25.00	3.0:1	3.0:1	5.3	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	14.27 cfs	
Depth:	0.17 ft	1.17 ft
Top Width:	25.99 ft	31.99 ft
Velocity:	3.39 fps	
X-Section Area:	4.21 sq ft	
Hydraulic Radius:	0.162 ft	
Froude Number:	1.49	

TABLE N9-2020 Channel Design Summary

						C	hannel N9-1\	W.2C						
						Typical	Rip Rap Line	ed Channel						
]			Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
N9-1W.2C	18.14	3.40	30	3	0.2	3.04	1	1.2	N/A	-	59.7	0.365	82	A

Design Flow: 10-year, 6-hour Storm

<u>N9-1W.2C WATERSHED DESIGN (10YR-</u> <u>6HR)</u>

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

	Siluciule Networking.										
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description					
Null	#1	==>	End	0.000	0.000	N9-1W.2C WATERSHED					

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
	(ac)	(ac)		(ac-it)
#1	59.700	59.700	18.14	1.60

Structure Summary:

Structure Detail:

Structure #1 (Null)

N9-1W.2C WATERSHED

					<u> </u>	33			
Stru #	SWS #	SWS Area	Time of Conc	Musk K	Musk X	Curve Number	UHS	Peak Discharge	Runoff Volume
		(ac)	(hrs)	(hrs)		Number		(cfs)	(ac-ft)
#1	1	59.700	0.365	0.000	0.000	82.000	М	18.14	1.595
	Σ	59.700						18.14	1.595

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	2.10	20.00	951.00	1.160	0.227
		6. Grassed waterway	6.52	80.00	1,227.00	3.830	0.088
		8. Large gullies, diversions, and low flowing streams	3.79	40.00	1,056.00	5.830	0.050
#1	1	Time of Concentration:					0.365

N9-1W.2C CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
30.00	3.0:1	3.0:1	3.4	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	18.14 cfs	
Depth:	0.20 ft	1.20 ft
Top Width:	31.17 ft	37.17 ft
Velocity:	3.04 fps	
X-Section Area:	5.97 sq ft	
Hydraulic Radius:	0.191 ft	
Froude Number:	1.22	

TABLE N9-2020 Channel Design Summary

						Cha	annel N9-2W	.1C.1D						
	Typical Rip Rap Lined Channel													
				[Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
N9-2W.1C.1D	12.41	11.80	15	3	0.2	4.95	1	1.2	N/A	-	18.4	0.084	81	А
											1			
1														

Design Flow: 10-year, 6-hour Storm

<u>N9-2W.1C.1D WATERSHED DESIGN</u> (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II		
Design Storm:	10 yr - 6 hr		
Rainfall Depth:	1.600 inches		

	Structure Networking.								
Туре		Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description		
Null		#1	==>	End	0.000	0.000	N9-2W.1C.1D WATERSHED		

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	18.400	18.400	12.41	0.56

Structure Summary:

Structure Detail:

Structure #1 (Null)

N9-2W.1C.1D WATERSHED

						55			
Stru #	SWS #	SWS Area	Time of Conc	Musk K	Musk X	Curve	UHS	Peak Discharge	Runoff Volume
"	"	(ac)	(hrs)	(hrs)		Number		(cfs)	(ac-ft)
#1	1	18.400	0.084	0.000	0.000	81.000	М	12.41	0.561
	Σ	18.400						12.41	0.561

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	7.03	18.00	256.00	2.120	0.033
		6. Grassed waterway	8.28	40.00	483.00	4.310	0.031
		8. Large gullies, diversions, and low flowing streams	11.83	90.00	761.00	10.310	0.020
#1	1	Time of Concentration:					0.084

N9-2W.1C.1D CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
15.00	3.0:1	3.0:1	11.8	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	12.41 cfs	
Depth:	0.16 ft	1.16 ft
Top Width:	15.97 ft	21.97 ft
Velocity:	4.95 fps	
X-Section Area:	2.51 sq ft	
Hydraulic Radius:	0.156 ft	
Froude Number:	2.20	

TABLE N9-2020 Channel Design Summary

	Channel N9-2W.1C.3D													
	Typical Rip Rap Lined Channel													
				ſ			Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	-
N9-2W.1C.3D	12.94	4.30	20	3	0.2	3.33	1	1.2	N/A	-	17.8	0.094	82	А
									l					

Design Flow: 10-year, 6-hour Storm

<u>N9-2W.1C.3D WATERSHED DESIGN</u> (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II			
Design Storm:	10 yr - 6 hr			
Rainfall Depth:	1.600 inches			

	Siluciule Networking.										
Туре		Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description				
Null		#1	==>	End	0.000	0.000	N9-2W.1C.3D WATERSHED				

#1 Null

Structure Networking:



	Immediate Contributing Area	Total Contributing Area	Peak Discharge (cfs)	Total Runoff Volume
	(ac)	(ac)	(013)	(ac-ft)
#1	17.800	17.800	12.94	0.59

Structure Summary:

Structure Detail:

Structure #1 (Null)

N9-2W.1C.3D WATERSHED

					<u> </u>	33			
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	17.800	0.094	0.000	0.000	82.000	М	12.94	0.593
	Σ	17.800						12.94	0.593

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	6. Grassed waterway	7.46	59.00	791.00	4.090	0.053
		8. Large gullies, diversions, and low flowing streams	4.29	40.00	932.00	6.210	0.041
#1	1	Time of Concentration:					0.094

N9-2W.1C.3D CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
20.00	3.0:1	3.0:1	4.3	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	12.94 cfs	
Depth:	0.19 ft	1.19 ft
Top Width:	21.13 ft	27.13 ft
Velocity:	3.33 fps	
X-Section Area:	3.89 sq ft	
Hydraulic Radius:	0.184 ft	
Froude Number:	1.37	

TABLE N9-2020 Channel Design Summary

					C	hannel N9-6\	W.1C						
Typical Rip Rap Lined Channel													
			[Designed			As-Built				
Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
20.12	6.00	26	3	0.2	3.97	1	1.2	N/A	9	81.7	0.537	82	А
	(cfs)	(cfs) (%)	(cfs) (%) Width (ft)	(cfs) (%) Width (ft) H:1 (ft)	(cfs) (%) Width (ft) H:1 (ft) Flow (ft)	Flow (Q) Slope Bottom Side Slope Depth Velocity (cfs) (%) Width (ft) H:1 (ft) Flow (ft) (fps)	Typical Rip Rap Line Designed Flow (Q) Slope Bottom Side Slope Depth Velocity Free (cfs) (%) Width (ft) H:1 (ft) Flow (ft) (fps) Board (ft)	Designed Flow (Q) Slope Bottom Side Slope Depth Velocity Free Total (cfs) (%) Width (ft) H:1 (ft) Flow (ft) (fps) Board (ft) Depth (ft)	Typical Rip Rap Lined Channel Designed Flow (Q) Slope Bottom Side Slope Depth Velocity Free Total Rip Rap (cfs) (%) Width (ft) H:1 (ft) Flow (ft) (fps) Board (ft) Depth (ft) (in)	Typical Rip Rap Lined Channel Designed As-Built Flow (Q) Slope Bottom Side Slope Depth Velocity Free Total Rip Rap Rip Rap (cfs) (%) Width (ft) H:1 (ft) Flow (ft) (fps) Board (ft) Depth (ft) (in) (in)	Typical Rip Rap Lined Channel Designed As-Built Flow (Q) Slope Bottom Side Slope Depth Velocity Free Total Rip Rap Rip Rap Watershed (cfs) (%) Width (ft) H:1 (ft) Flow (ft) (fps) Board (ft) Depth (ft) (in) (in) (acres)	Typical Rip Rap Lined Channel Designed As-Built Flow (Q) Side Slope Depth Velocity Free Total Rip Rap Watershed Time of (%) Width (ft) H:1 (ft) Flow (ft) Openth (ft) Designed As-Built Flow (Q) Side Slope Depth Velocity Free Total Rip Rap Watershed Time of (cfs) (%) Width (ft) H:1 (ft) Flow (ft) (fps) Board (ft) Depth (ft) (in) (in) (acres) Concentration (hr) (hr)	Typical Rip Rap Lined Channel Designed As-Built Flow (Q) Slope Bottom Side Slope Depth Velocity Free Total Rip Rap Rip Rap Rip Rap Watershed Time of Curve (cfs) (%) Width (ft) H:1 (ft) Flow (ft) (fps) Board (ft) Depth (ft) (in) (in) (acres) Concentration (hr) Number

Design Flow: 10-year, 6-hour Storm

<u>N9-6W.1C WATERSHED DESIGN (10YR-6HR)</u>

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II			
Design Storm:	10 yr - 6 hr			
Rainfall Depth:	1.600 inches			

	Siluciule Networking.										
Туре		Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description				
Null		#1	==>	End	0.000	0.000	N9-6W.1C WATERSHED				

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	81.700	81.700	20.12	2.18

Structure Summary:

Structure Detail:

Structure #1 (Null)

N9-6W.1C WATERSHED

						0,5			
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	81.700	0.537	0.000	0.000	82.000	М	20.12	2.179
	Σ	81.700						20.12	2.179

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	3.32	55.00	1,659.00	1.450	0.317
		6. Grassed waterway	2.34	10.00	427.00	2.290	0.051
		8. Large gullies, diversions, and low flowing streams	4.12	40.00	971.00	6.080	0.044
		8. Large gullies, diversions, and low flowing streams	0.65	5.00	771.00	2.410	0.088
		8. Large gullies, diversions, and low flowing streams	6.02	60.00	996.00	7.360	0.037
#1	1	Time of Concentration:					0.537

N9-6W.1C CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
26.00	3.0:1	3.0:1	6.0	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	20.12 cfs	
Depth:	0.19 ft	1.19 ft
Top Width:	27.14 ft	33.14 ft
Velocity:	3.97 fps	
X-Section Area:	5.07 sq ft	
Hydraulic Radius:	0.186 ft	
Froude Number:	1.62	

TABLE N9-2020 Channel Design Summary

						Cha	annel N9-6W	.1C.1D						
						Typical	Rip Rap Line	ed Channel						
]			Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
N9-6W.1C.1D	8.64	4.12	30	3	0.1	2.41	1	1.1	N/A	-	30.2	0.412	82	А
											J			

Design Flow: 10-year, 6-hour Storm

<u>N9-6W.1C.1D WATERSHED DESIGN</u> (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II		
Design Storm:	10 yr - 6 hr		
Rainfall Depth:	1.600 inches		

	Siluciule Networking.							
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description		
Null	#1	==>	End	0.000	0.000	N9-6W.1C.1D WATERSHED		

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
	(ac)	(ac)		(ac-it)
#1	30.200	30.200	8.64	0.81

Structure Summary:

Structure Detail:

Structure #1 (Null)

N9-6W.1C.1D WATERSHED

					<u> </u>	33			
Stru #	SWS #	SWS Area	Time of Conc	Musk K	Musk X	Curve	UHS	Peak Discharge	Runoff Volume
"	"	(ac)	(hrs)	(hrs)		Number		(cfs)	(ac-ft)
#1	1	30.200	0.412	0.000	0.000	82.000	М	8.64	0.808
	Σ	30.200						8.64	0.808

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	3.32	55.00	1,659.00	1.450	0.317
		6. Grassed waterway	2.34	10.00	427.00	2.290	0.051
		8. Large gullies, diversions, and low flowing streams	4.12	40.00	971.00	6.080	0.044
#1	1	Time of Concentration:					0.412

N9-6W.1C.1D CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom 'idth (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
30.00	3.0:1	3.0:1	4.1	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	8.64 cfs	
Depth:	0.12 ft	1.12 ft
Top Width:	30.71 ft	36.71 ft
Velocity:	2.41 fps	
X-Section Area:	3.59 sq ft	
Hydraulic Radius:	0.117 ft	
Froude Number:	1.24	

TABLE N9-2020

Channel Design Summary	y	
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	Channel N9-6W.1C.2D													
	Typical Rip Rap Lined Channel													
]	Designed					As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
N9-6W.1C.2D	12.50	2.60	35	3	0.2	2.28	1	1.2	N/A	-	21.4	0.126	86	A
											4			

Design Flow: 10-year, 6-hour Storm

<u>N9-6W.1C.2D WATERSHED DESIGN</u> (10YR-6HR)

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033 1

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description				
Null	#1	==>	End	0.000	0.000	N9-6W.1C.2D WATERSHED				

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	21.400	21.400	12.50	0.81

Structure Summary:

Structure Detail:

Structure #1 (Null)

N9-6W.1C.2D WATERSHED

					<u> </u>	33			
Stru #	SWS #	SWS Area	Time of Conc	Musk K	Musk X			Peak Discharge	Runoff Volume
"	"	(ac)	(hrs) ^(hrs)	(nrs)		Number		(cfs)	(ac-ft)
#1	1	21.400	0.126	0.000	0.000	86.000	М	12.50	0.811
	Σ	21.400						12.50	0.811

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	4.08	12.00	294.00	1.610	0.050
		6. Grassed waterway	15.66	70.00	447.00	5.930	0.020
		8. Large gullies, diversions, and low flowing streams	2.56	25.00	976.00	4.800	0.056
#1	1	Time of Concentration:					0.126

N9-6W.1C.2D CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom /idth (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
35.00	3.0:1	3.0:1	2.6	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	12.50 cfs	
Depth:	0.15 ft	1.15 ft
Top Width:	35.93 ft	41.93 ft
Velocity:	2.28 fps	
X-Section Area:	5.48 sq ft	
Hydraulic Radius:	0.152 ft	
Froude Number:	1.03	

TABLE N9-2020 Channel Design Summary

	Channel N9-8W.1C													
	Typical Rip Rap Lined Channel													
				Ĩ			Designed			As-Built				
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
N9-8W.1C	7.70	11.50	25	3	0.1	3.37	1	1.1	N/A	9	9.2	0.097	84	A

Design Flow: 10-year, 6-hour Storm

<u>N9-8W.1C WATERSHED DESIGN (10YR-</u> <u>6HR)</u>

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

Туре		Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description				
Null		#1	==>	End	0.000	0.000	N9-8W.1C WATERSHED				

#1 Null

Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	9.200	9.200	7.70	0.36

Structure Summary:

Structure Detail:

Structure #1 (Null)

N9-8W.1C WATERSHED

					<u> </u>	35			
Stru #	SWS #	SWS Area	Time of Conc	Musk K	Musk X	Curve	UHS	Peak Discharge	Runoff Volume
#	#	(ac)	(hrs)	hrs) (hrs)		Number		(cfs)	(ac-ft)
#1	1	9.200	0.097	0.000	0.000	84.000	М	7.70	0.363
	Σ	9.200						7.70	0.363

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	1.93	5.00	259.00	1.110	0.064
		6. Grassed waterway	9.36	25.00	267.00	4.580	0.016
		8. Large gullies, diversions, and low flowing streams	11.47	75.00	654.00	10.150	0.017
#1	1	Time of Concentration:					0.097

N9-8W.1C CHANNEL DESIGN

Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
25.00	3.0:1	3.0:1	11.5	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	7.70 cfs	
Depth:	0.09 ft	1.09 ft
Top Width:	25.54 ft	31.54 ft
Velocity:	3.37 fps	
X-Section Area:	2.29 sq ft	
Hydraulic Radius:	0.089 ft	
Froude Number:	1.98	

TABLE N9-2020 Channel Design Summary

	Channel N9-9W.1C													
	Typical Rip Rap Lined Channel													
							Designed			As-Built	1			
Channel	Flow (Q)	Slope	Bottom	Side Slope	Depth	Velocity	Free	Total	Rip Rap	Rip Rap	Watershed	Time of	Curve	Design
	(cfs)	(%)	Width (ft)	H:1 (ft)	Flow (ft)	(fps)	Board (ft)	Depth (ft)	(in)	(in)	(acres)	Concentration (hr)	Number	
N9-9W.1C	13.06	12.00	23	3	0.1	4.34	1	1.1	N/A	9	33.1	0.248	83	С
											l			
														_

Design Flow: 10-year, 6-hour Storm

<u>N9-9W.1C WATERSHED DESIGN (10YR-</u> <u>6HR)</u>

Kurtis Silversmith

Peabody Western Coal Co. P.O. Box 650 Kayenta, AZ 86033

General Information

Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 6 hr
Rainfall Depth:	1.600 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description		
Null	#1	==>	End	0.000	0.000	N9-9W.1C WATERSHED		

#1 Null

Structure Networking:

	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	33.100	33.100	13.06	0.97

Structure Summary:

Structure Detail:

Structure #1 (Null)

N9-9W.1C WATERSHED

					<u> </u>	0,0			
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	33.100	0.248	0.000	0.000	83.000	М	13.06	0.970
	Σ	33.100						13.06	0.970

Subwatershed Hydrology Detail:

Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	4.72	35.00	741.00	1.730	0.118
		6. Grassed waterway	4.42	50.00	1,132.00	3.150	0.099
		8. Large gullies, diversions, and low flowing streams	11.99	142.00	1,184.00	10.380	0.031
#1	1	Time of Concentration:					0.248

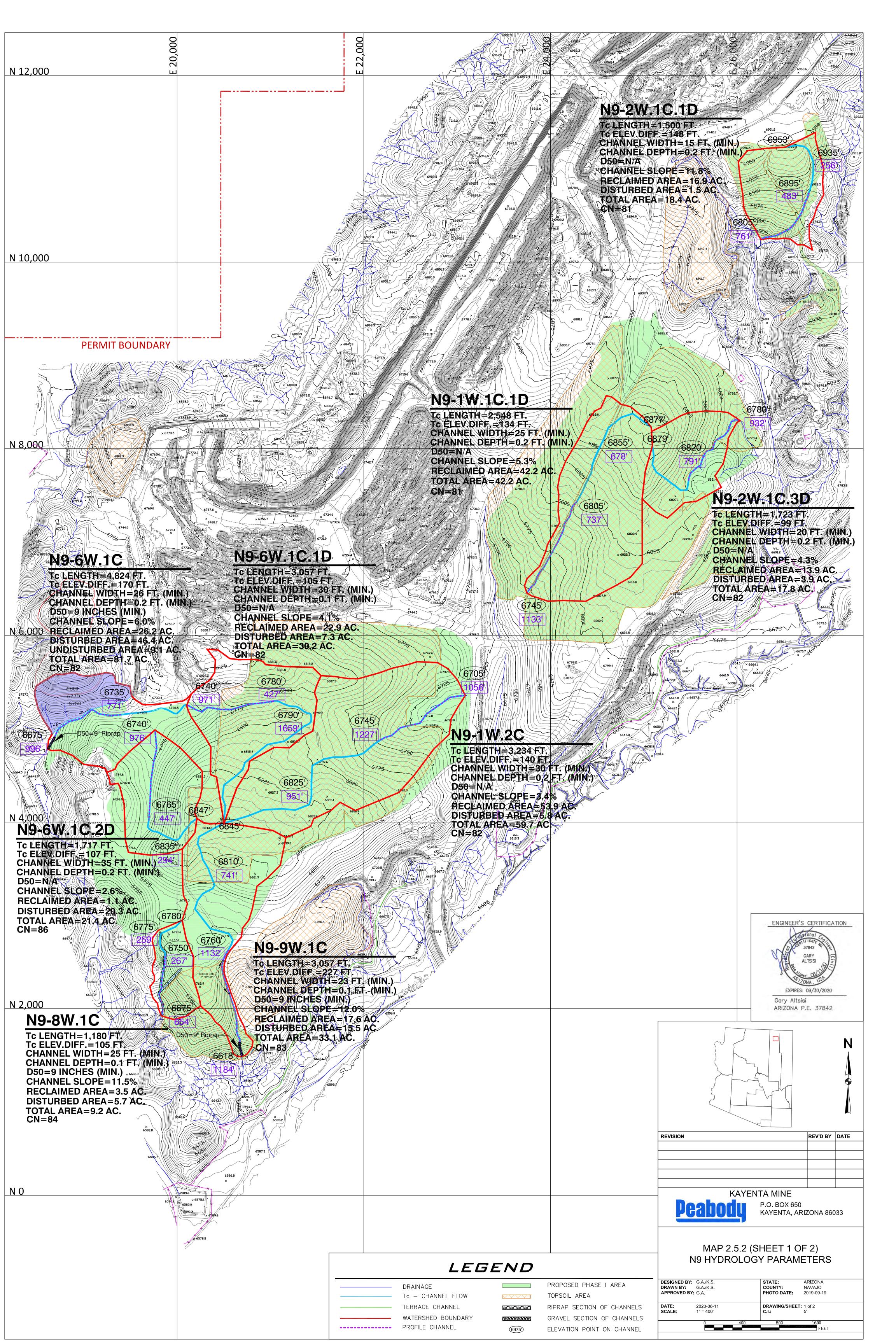
N9-9W.1C CHANNEL DESIGN

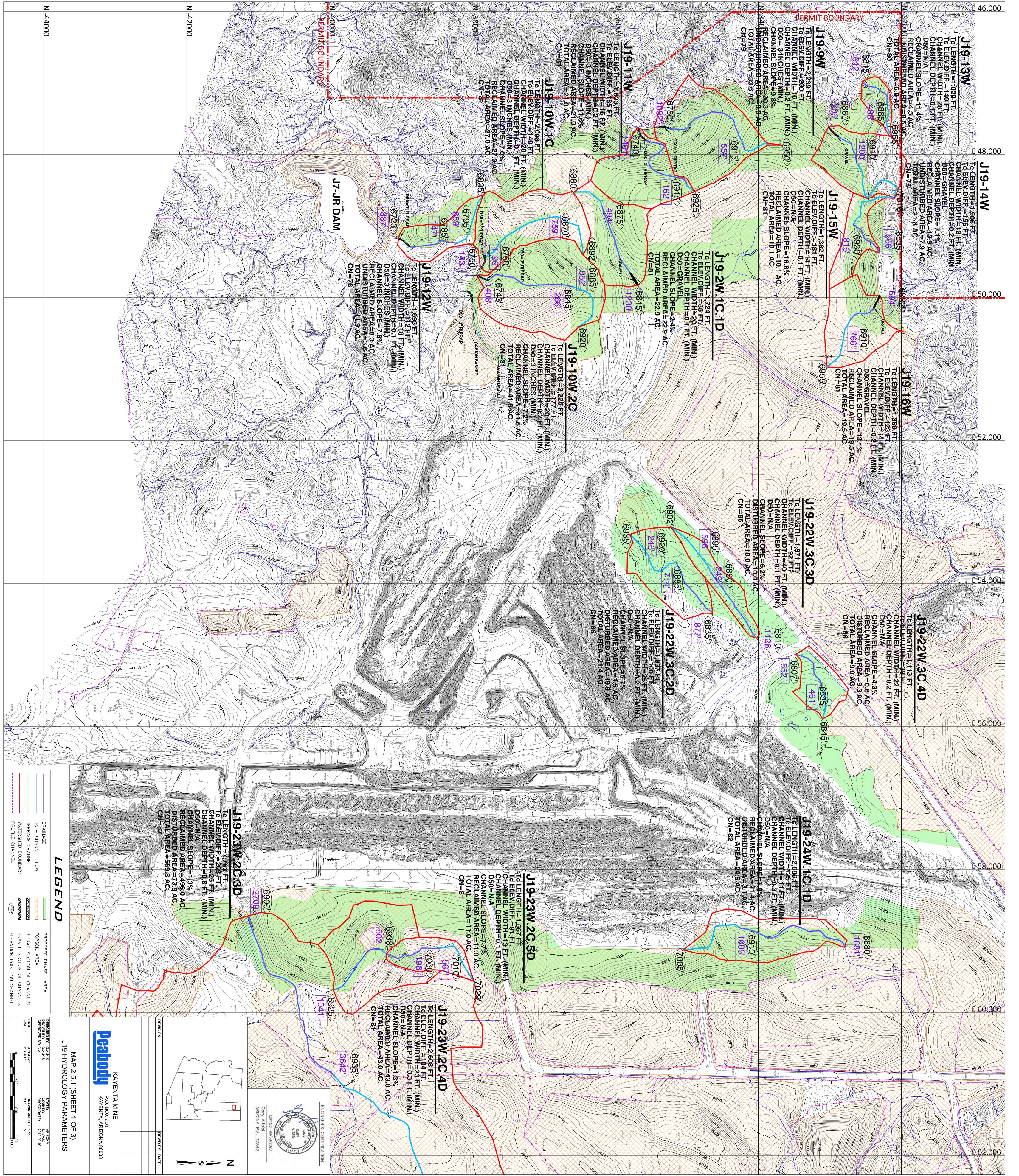
Material: Graded Spoil

Trapezoidal Channel

Bottom Width (ft)	Left Sideslope Ratio	Right Sideslope Ratio	Slope (%)	Manning's n	Freeboard Depth (ft)	Freeboard % of Depth	Freeboard Mult. x (VxD)	Limiting Velocity (fps)
23.00	3.0:1	3.0:1	12.0	0.0300	1.00			5.0

	w/o Freeboard	w/ Freeboard
Design Discharge:	13.06 cfs	
Depth:	0.13 ft	1.13 ft
Top Width:	23.77 ft	29.77 ft
Velocity:	4.34 fps	
X-Section Area:	3.01 sq ft	
Hydraulic Radius:	0.126 ft	
Froude Number:	2.15	



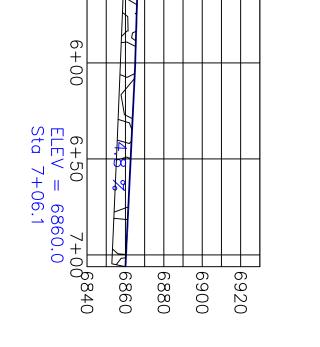


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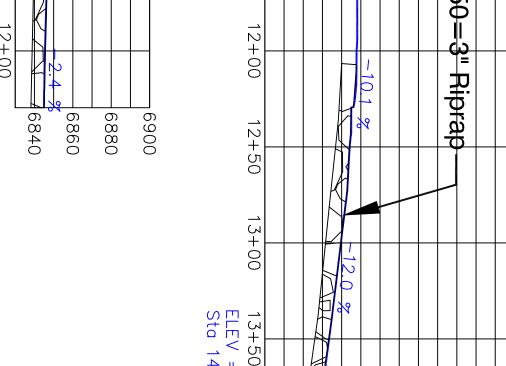


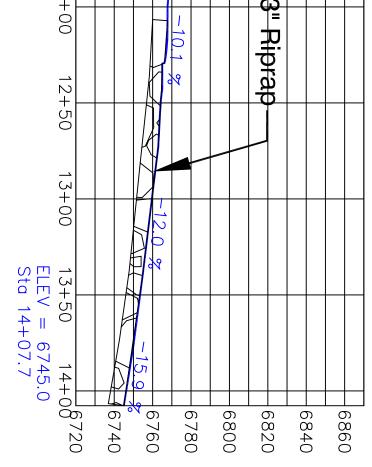


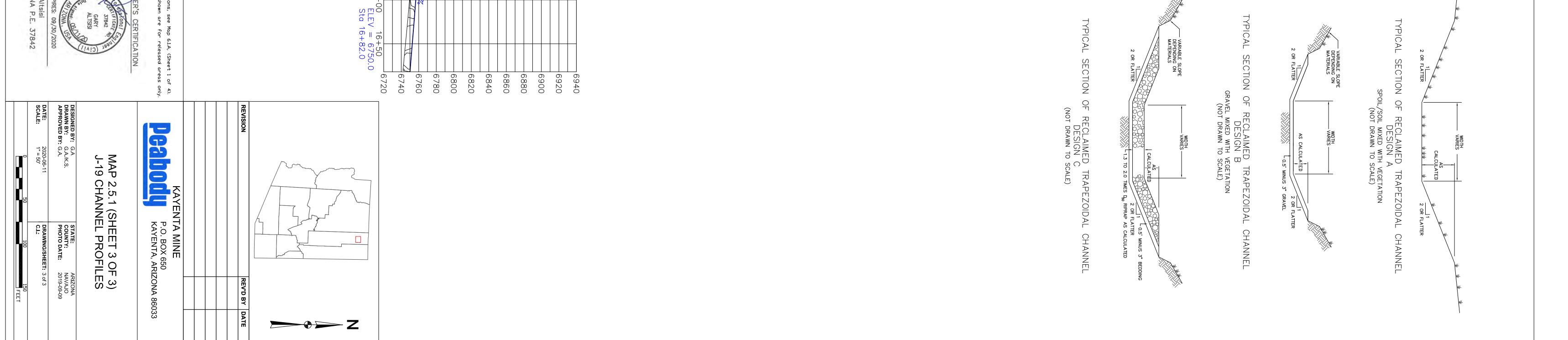
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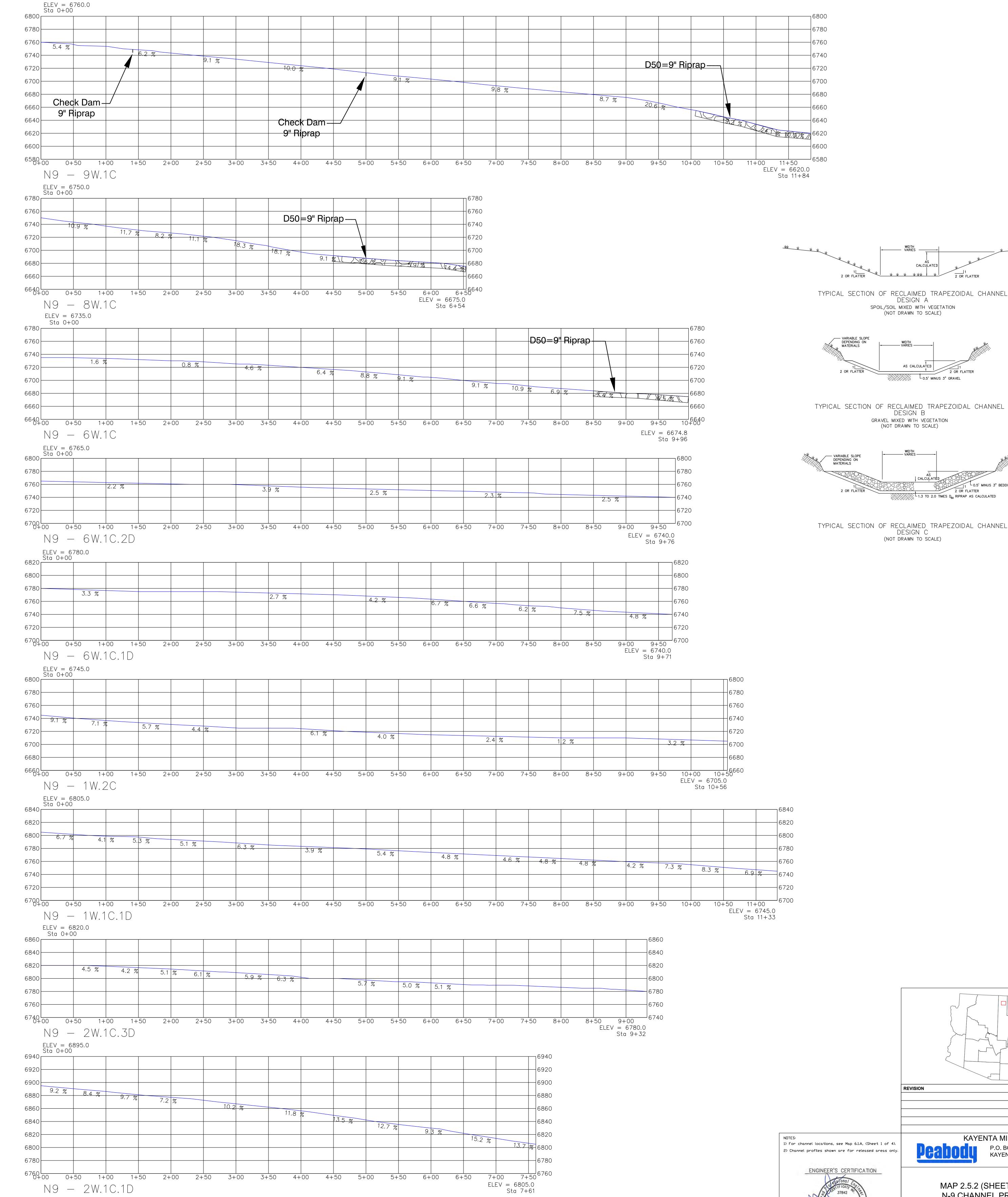












TYPICAL SECTION OF RECLAIMED TRAPEZOIDAL CHANNEL DESIGN C (NOT DRAWN TO SCALE)

* * * *

2 OR FLATTER

2 OR FLATTER

L 0.5' MINUS 3" BEDDING

2 OR FLATTER

